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ENERGETICS AND MECHANICS OF RUNNING:

*Metabolic and mechanical changes in ultra-endurance running races
and the effects of a specific training on energy cost of running*

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ABSTRACT

The present thesis is divided into two parts.

Part I: The objectives of the first part were to examine the factors affecting the ultra-endurance performance and in particular which aspects influence the cost of running (Cr). Consequently, we defined how the Cr and running mechanics changed during different types (i.e. level and uphill) of ultra-endurance races. Finally, we proposed a specific training protocol for improving the Cr in high-level ultra-marathoners.

We assessed the Cr by measuring the oxygen consumption at one (or more) fixed speeds using a metabolic unit. Further, for the running mechanics measurement and the spring-mass model parameters computation we used video analysis. Other parameters such as maximal muscle power of the lower limbs (MMP), morphological properties of the gastrocnemius medialis and Achilles tendon stiffness were also measured.

Our studies showed that the maximal oxygen uptake, the fraction of it maintained throughout the race and the Cr are the main physiological parameters affecting the ultra-endurance performance, both in level and uphill competitions. Moreover, low Cr values were related to high MMP, vertical stiffness (k_{vert}), low foot print index (FPI), Achilles tendon stiffness and external work. These results indicate that MMP, k_{vert} and FPI are important factors in determining ultra-endurance performance. Also, our studies reported that during ultra-endurance competitions athletes tend to change their running mechanics after a certain time (~4 hours) rather than after a certain distance covered. Then, by adding strength, explosive and power training to the usual endurance training it is possible to lower the cost of running leading to a better performance.

From these conclusions we suggest new training protocol for the ultra-marathoners including strength, explosive and power training which maintain a correct and less expensive running technique during ultra-endurance events.

Part II: The aim of the second part was to develop and validate a customized thermoplastic polyurethane insole shoe sensor for collecting data about the ground reaction forces (GRF), contact and aerial times. This prototype allowed us to collect vertical GRF and contact time by using piezoresistive force sensors (RFS). Our final model was composed by a rubber insole, five RFSs, an s-beam load cell, an acquisition device (NI myRIO) and a battery case. By using this device we can collect data on field, avoiding the restrictions imposed by the laboratory environment.

LIST OF PUBLICATIONS

- I. Lazzer S, Taboga P, Salvadego D, Rejc E, Simunic B, Narici MV, Buglione A, **Giovanelli N**, Antonutto G, Grassi B, Pisot R, di Prampero PE. Factors affecting metabolic cost of transport during a multi-stage running race. *J Exp Biol.* 2014;217(Pt 5):787-95. doi: 10.1242/jeb.091645. PubMed PMID: 24265425.
- II. Lazzer S, Salvadego D, Taboga P, Rejc E, **Giovanelli N**, di Prampero PE. Effects of the Etna uphill ultramarathon on energy cost and mechanics of running. *Int J Sports Physiol Perform.* 2015;10(2):238-47. doi: 10.1123/ijsp.2014-0057. PubMed PMID: 25117400.
- III. **Giovanelli N**, Taboga P, Rejc E, Simunic B, Antonutto G, Lazzer S. Effects of an Uphill Marathon on Running Mechanics and Lower Limb Muscles Fatigue. *Int J Sports Physiol Perform.* 2015. doi: 10.1123/ijsp.2014-0602. PubMed PMID: 26390075.
- IV. **Giovanelli N**, Ortiz ALR, Henninger K, Kram R. Energetics of vertical kilometer foot races; is steeper cheaper? *J Appl Physiol (1985).* 2016 Feb 1;120(3):370-5. doi: 10.1152/jap.00546.2015. Epub 2015 Nov 25.

LIST OF UNDER REVISION PAPERS

- V. **Giovanelli N**, Taboga P, Rejc E, Lazzer S. Effects of a strength, explosive and plyometric training protocol on ultra-endurance athletes' cost of running. Under revision *Eur J Appl Physiol*
- VI. **Giovanelli N**, Taboga P, Lazzer S. Changes in running mechanics during a six hours running race. Under revision *Int J Sports Physiol Perform*

OTHER RELATED PUBLICATIONS AND UNPUBLISHED PAPERS

- VII. Da Ponte A, **Giovanelli N**, Nigris D, Lazzer S. Effects of hydrogen rich alkaline water on prolonged intermittent exercise. Under revision *J Int Soc Sport Nutr.*
- VIII. Da Ponte A, Antonutto G, **Giovanelli N**, Curcio F, Cortese P, Lazzer S. Effects of an uphill only running marathon on biomarkers of cardiac and muscle damage . In Prep.

CONFERENCE PROCEEDINGS

- I. **Giovanelli N**, Taboga P, Rejc E, Simunic B, Antonutto G, Lazzer S. Changes in spring.-mass model parameters and lower limb muscle fatigue during an uphill ultra-marathon. Presentation at the 2015 Rocky Mountain Regional American Society of Biomechanics Meeting. April 17th-18th, 2015. Estes Park, USA.
- II. Giovanelli D, **Giovanelli N**, Taboga P, Shojaei Bariuei E, Boscariol P, Vidoni R, Gasparetto A, Lazzer S. A mechatronic system mounted on insole for analyzing human gait. International Conference on Robotiscs and Mechatronics. October 15th-17th, 2014. Tehran, Iran.
- III. Lazzer S, Taboga P, Salvadego D, Rejc E, Simunic B, Narici MV, Buglione A, **Giovanelli N**, Antonutto G, Grassi B, Pisot R, di Prampero PE. Factors affecting energy cost of running during an ultra-endurance race. Med Sci Sports Exerc. 2014; 46(5):S733

AWARDS

- I. Boscariol P, Gasparetto A, **Giovanelli N**, Lazzer S, Taboga P, Shojaei Barjuei E. Best application “Advanced research” – Forum Tecnologico NIDays 2015. March 12th Milan, Italy

LIST OF ABBREVIATIONS

ΔL	Leg length variation during the stance phase
Δz	Vertical displacement of the center of mass during the stance phase
BW	Body weight
CG	Control group
CoM	Centre of mass
CoT	Cost of transport
Cr	Cost of running
Cr_{vert}	Vertical cost of running
Cw	Cost of walking
Cw_{vert}	Vertical cost of walking
E_{es}	Elastic energy
EG	Experimental group
E_{kf}	Forward kinetic energy
E_{p}	Potential energy
FPI	Foot print index
GM	Gastrocnemius medialis
GRF	Ground reaction force
HS	Heel strike
K_{leg}	Leg stiffness
K_{tendon}	Stiffness of the Achilles' tendon
K_{vert}	Vertical stiffness
LT	Lactate threshold
MMP	Maximal muscle power
MS	Mid-stance
MTS	Muscle tendon stiffness
MUM	Mountain ultra-marathon
RE	Running Economy
RFD	Rate of force development
SEP	Strength, endurance and plyometric
S_m	Optimal metabolic transition speed
SMM	Spring-mass model
S_s	Spontaneous transition speed
Ta	Aerial time
Tc	Contact time
TMG	Tensyomyography
TO	Toe off

$\dot{V}CO_2$	Carbon dioxide production
VK	Vertical kilometer
$\dot{V}O_2$	Oxygen consumption
$\dot{V}O_{2max}$	Maximal oxygen uptake
W _{ext}	External work
W _{int}	Internal work

CHAPTER I

GENERAL INTRODUCTION

Ultra-endurance: from the origins to the present days

The term *ultra-endurance* identifies efforts greater than four (Hawley and Hopkins 1995; Laursen and Rhodes 2001) or six hours (Zaryski and Smith 2005). Several multi-stage cycling events (Tour de France, Giro d'Italia) that took place at the beginning of last century presented stages longer than 300-400 km. However, one of the oldest "official" ultra-endurance competition is the Comrades Marathon (www.comrades.com), which take place in South Africa. It is a point-to-point 90-km running race and the first edition took place in 1921. The racecourse direction is alternated each year between the cities of Durban and Pietermaritzburg. The course record was set in the 2007 edition by the Russian Leonid Shvetsov in 5 hours 20 minutes and 49 seconds.

Ultra-endurance performance is usually achieved by swimming, cycling or running (or the combination of these three specialty, e.g. the Ironman). Our field of interest is the running competition (i.e. ultra-marathons) and we will refer to this type of race throughout the text.

Endurance running is defined as running many kilometers over extended time periods using aerobic metabolism (Bramble and Lieberman 2004). It is a type of locomotion typical of the humans that influenced human evolution. Indeed, humans are the only primates capable of endurance running. Apes and other primates can sprint rapidly, but they do so only for short distances (Bramble and Lieberman 2004). Millions people all over the world regularly jog or run several kilometers a day. Amateur runners can regularly run up to 10 km or even longer distances such as marathons. Recent trends show how races longer than a marathon have become more popular among the running community lately.

Ultra-marathons are footraces longer than the traditional marathon distance (>42.195 km) and they can be divided into two types: those that cover a specified distance (i.e. 50-100 km, in which the ranking depends on the time spent to cover that distance) and those that take place during specified time (i.e. 6-12-24 h, in which the ranking depends on the distance covered). Further, some races are performed on a 200-m (indoor) or 400-m (outdoor) track loop, others are on pavement road and others are on trail or technical terrain (e.g. mountain path). The number of participants in these types of race is rapidly increasing and many "classical" marathoners are eager to race in longer distances. For these reasons, over the last few years the interest of different research groups has been directed to better understand the factors that affect the ultra-

endurance performance (Gimenez et al. 2013; Hoffman 2014; Lazzer et al. 2012; Martin et al. 2010; Millet 2011; Millet et al. 2011a; Morin et al. 2011a; Rejc et al. 2010; Schena et al. 2014; Vernillo et al. 2015a).

Factors affecting ultra-endurance performance

Lazzer et al. (2012) reported that the main physiological factors determining the ultra-endurance performance during a multi-stage running race were the maximal oxygen uptake ($\dot{V}O_2\text{max}$), the fraction of it sustained throughout the race (F) and the cost of running (Cr) (Fig. 1.1).

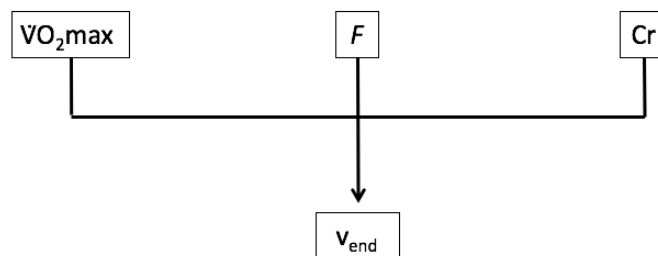


Fig. 1.1 – Factors related to distance running performance. $\dot{V}O_2\text{max}$: maximal oxygen uptake; F : % of $\dot{V}O_2\text{max}$ maintained during the race; Cr : cost of running; v_{end} : speed in endurance running.

Specifically, the combination of these three components explains 87% of the total competition time variance. As described previously (di Prampero et al. 1986) the maximal theoretical speed in endurance running (v_{end}) can be predicted by the equation

$$v_{\text{end}} = \dot{V}O_2\text{max} \cdot F \cdot Cr^{-1} \quad (1)$$

Consequently, if athletes want to improve their performance they should focus the training on improving one or more of these parameters. $\dot{V}O_2\text{max}$ and F can be enhanced by specific running or cycling training (Laursen et al. 2002; Midgley et al. 2006), whereas the Cr can be improved by including various forms of training (Billat et al. 1999; Enoksen et al. 2011; Hoff et al. 2002; Hoff et al. 1999; Ronnestad et al. 2012; Ronnestad and Mujika 2014; Spurrs et al. 2003; Storen et al. 2008; Turner et al. 2003).

Maximal oxygen uptake

Maximal oxygen uptake is defined as the highest rate at which oxygen can be taken up and utilized by the body during severe exercise (Bassett and Howley 2000). Potential factors limiting $\dot{V}O_2\text{max}$ operate along the route from the air to the mitochondria, where the oxygen is used. They include the pulmonary diffusion capacity, the maximal cardiac output, the blood capacity to transport oxygen and/or the muscle's capacity to consume oxygen (Bassett and Howley 2000) (Fig. 1.2).

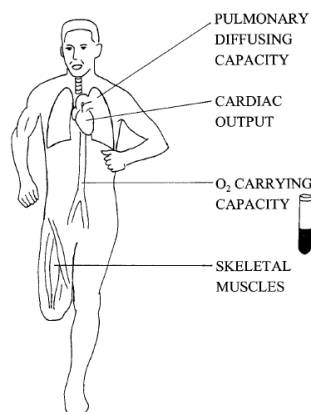


Fig. 1.2 – Physiological factors limiting $\dot{V}O_2\text{max}$ during exercise in human. From Bassett and Howley (2000)

The *maximal cardiac output* is considered the main limiting factor, affecting the $\dot{V}O_2\text{max}$ by 70-85%. Since during maximum exercise almost all the available O_2 is extracted from the red blood cells as they perfuse the active muscles, it follows that the mechanism for the increase in $\dot{V}O_2\text{max}$ is by increasing the blood flow (and O_2 delivery) (Bassett and Howley 2000).

The *oxygen carrying capacity* can be enhanced by increasing the hemoglobin content of the blood (Ekblom et al. 1976). It can be induced by specific training (i.e. training in altitude) or as a consequence of unethical and illegal doping activity. Indeed, reinfusion of 900-1,350 mL blood leads to an increase in $\dot{V}O_2\text{max}$ by 4-9% (Gledhill 1982; Gledhill 1985).

The *pulmonary system* may limit $\dot{V}O_2\text{max}$ under certain circumstances, but in “normal” conditions (e.g. sea level, healthy subjects...) it is not the most important factor in determining the $\dot{V}O_2\text{max}$. Authors (Dempsey et al. 1984) demonstrated that elite athletes with high maximal cardiac output (~40 L/min) can be penalized by the lower

transit time of the red blood cell in the pulmonary capillary. This leads to a lower time to saturate the blood with O₂ before it exits the pulmonary capillary net.

Other limitations can be detected in the *skeletal muscles*. Peripheral diffusion gradients, mitochondrial enzyme levels and capillary density have a role in limiting the $\dot{V}O_2\text{max}$. However, when limiting factors for $\dot{V}O_2\text{max}$ are discussed, there is agreement in saying that it is mainly the ability of the cardiorespiratory system (i.e. heart, lungs and blood) to transport O₂ to the muscles, not the ability of muscle mitochondria to consume O₂ that limits $\dot{V}O_2\text{max}$ (Bassett and Howley 2000).

The fraction of maximum oxygen uptake

Another important factor in determining the performance in ultra-endurance race is the fraction of $\dot{V}O_2\text{max}$ maintained during the competition. It decreases with increasing the exercise duration and it is strongly dependent from the training status of the athlete. Subjects are able to sustain the 100% of $\dot{V}O_2\text{max}$ for ~6 minutes (Billat et al. 1994; Renoux et al. 2000) while it is much lower when they perform a longer exercise. Indeed, ultra-marathoners may be able to sustain a running intensity of 88% of $\dot{V}O_2\text{max}$ for 1 hour, 66% $\dot{V}O_2\text{max}$ for 8 hours and 39 – 47% for 24 hours (Davies and Thompson 1979; Gimenez et al. 2013; Millet et al. 2011a). Conversely to $\dot{V}O_2\text{max}$, which increases during the first 2 months of training and then it stabilizes, F continues to change over time (Bassett and Howley 2000).

The energy cost of walking and running

The cost of transport (CoT) is determined by measuring the steady-state oxygen consumption ($\dot{V}O_2$, in ml/kg m⁻¹) and the respiratory exchange ratio (RER) at a fixed speed or power. CoT can be expressed as joule or kilojoule per distance covered, or in mlO₂ used per unit distance and it is lower in trained athletes. Moreover, many studies used the term running economy (RE) as synonymous with oxygen cost of running (Lacour and Bourdin 2015). It can be applied to different actions (cycling, swimming, rowing, walking, running, etc.). However, we will focus on the cost of walking (C_w) and running (C_r).

It has been reported that the importance of C_r is higher in determining the performance when athletes with similar $\dot{V}O_2\text{max}$ are compared and its relevance increases in longer

aces (Horowitz et al. 1994). The Cr is affected by several factors (Fig. 1.3), nonetheless in the present thesis we will discuss only few of them.

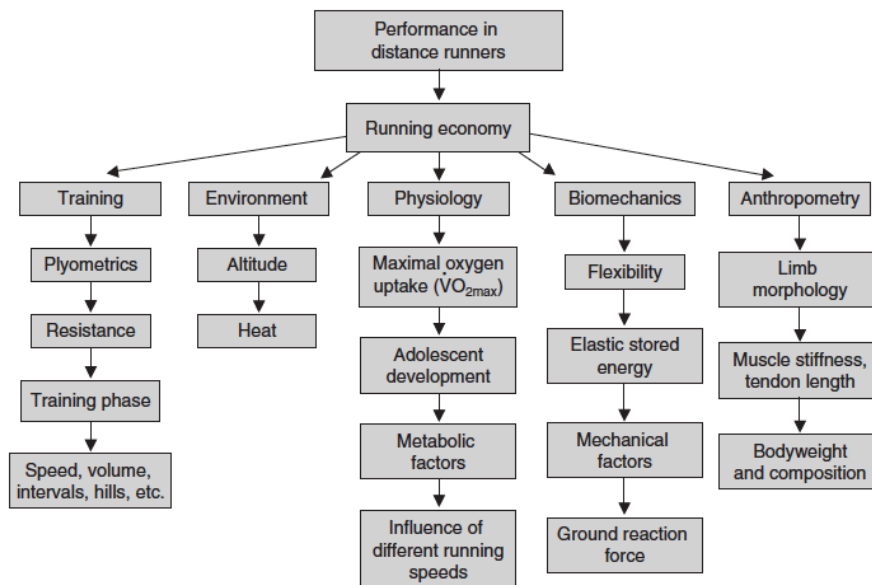


Fig. 1.3 – Factors affecting running economy. From Saunders et al. (2004)

The metabolic cost of walking for humans, like that of other mammals, is a “U”-shaped curve, in which optimal speed is $\sim 1.3 \text{ m} \cdot \text{s}^{-1}$ (Abe et al. 2015; Minetti et al. 1994b). On level ground or treadmills, at speeds slower than $\sim 2 \text{ m} \cdot \text{s}^{-1}$, walking requires less metabolic energy than running (di Prampero 1986; Minetti et al. 1994b). From $\sim 2 \text{ m} \cdot \text{s}^{-1}$ running is the preferred gait. However, the speed at which subjects decide to switch from walking to running (preferred transition speed) does not always correspond with the optimal metabolic transition speed (Mercier et al. 1994) (Fig. 1.4).

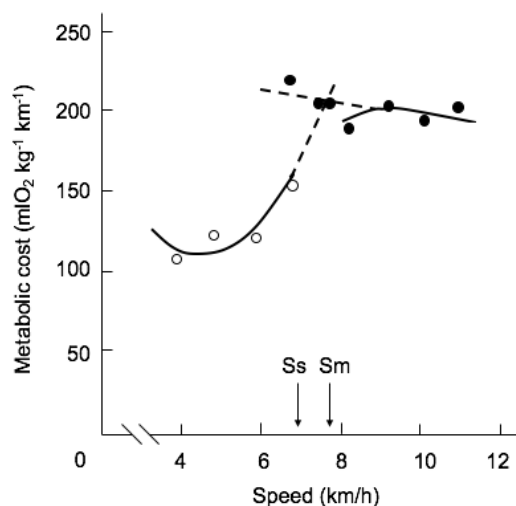


Fig. 1.4 – The optimal metabolic transition speeds (S_m) and spontaneous transition speed (S_s) do not always overlap. Adapted from Minetti et al. (1994b).

The difference between cost of walking and running is generally attributed to the more effective inverted pendulum-like exchange of mechanical energy at slower walking speeds and the superior elastic energy storage and recovery of running at faster speeds (see the “Walking and running mechanics” paragraph) (Farley and Ferris 1998) (Fig. 1.5). Indeed, at higher speeds running is less costly than walking because the exchange of kinetics and potential energy is in phase and a spring-mass mechanism is involved. Tendons and ligaments in the leg store elastic strain energy during the initial, braking part of the support phase, and then release the energy during the subsequent propulsive phase (Cavagna et al. 1976).

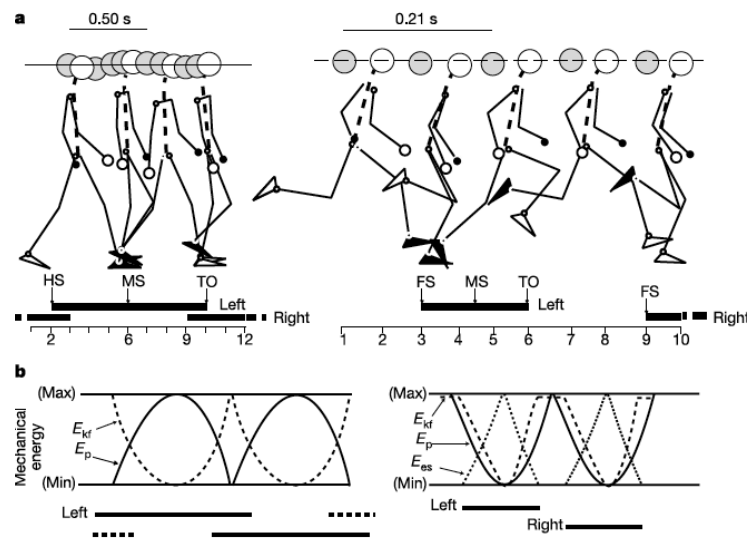


Fig. 1.5 – Comparison of walking and running. **a**, kinematics of walking (left) and running (right). **b**, biomechanical contrasts between human gaits. HS: heel strike; TO: toe off; MS: mid-stance; E_{kf} : forward kinetic energy; E_p : potential energy; E_{es} : elastic energy. Adapted from Bramble and Lieberman (2004).

Conversely to walking, it is widely accepted that the metabolic rate during running increases linearly as a function of the speed. Thus, it has been proposed that C_r is independent from the running speed (di Prampero et al. 1986; di Prampero et al. 2009; Margaria et al. 1963) (Fig. 1.6).

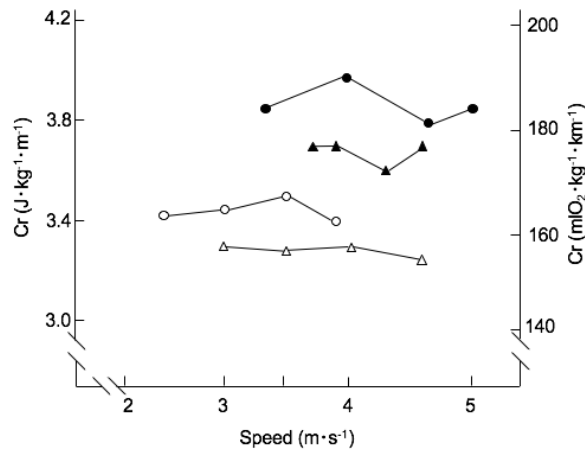


Fig. 1.6 - Energy cost of running as a function of treadmill speed in four subjects. Adapted from di Prampero et al. (1986).

Indeed, researchers have suggested that the amount of energy used to run a given distance is (nearly) the same, independently from the speed (Kram and Taylor 1990; Margaria et al. 1963). Conversely, more recently some authors have sustained that there is an optimal running speed (Stuedel-Numbers and Wall-Scheffler 2009) which can derive from an evolutionary selection (Fig. 1.7).

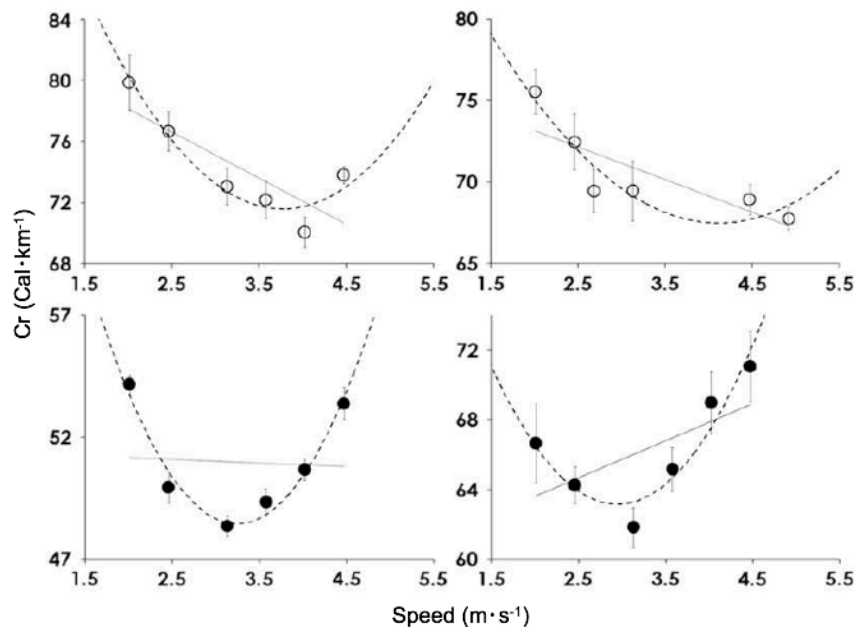


Fig. 1.7 - Individual's Cr with both a linear and curvilinear line fit. Open circles are males, closed circles are females. Error bars are the standard error of mean values averaged over the trials at each speed.

Adapted from Stuedel-Numbers and Wall-Scheffler (2009).

Cost of running and ultra-endurance

It is reported that during a marathon race the Cr at a fixed speed increases by ~5% (Brueckner et al. 1991). During ultra-marathons different results are reported. Most of authors showed that Cr increases with the distance covered in ultra-endurance performance (Gimenez et al. 2013; Lazzer et al. 2012; Millet et al. 2009). Gimenez et al. (2013) reported that Cr increases after 8 hours of treadmill run compared with the PRE and this increment may be explained by peripheral muscular alterations. In particular, authors (Fernstrom et al. 2007) demonstrated that the reduction of mitochondrial efficiency might explain the increased oxygen cost. Also, changes in muscle activation, or changes in running mechanics pattern could affect the Cr (Morin et al. 2011b). Moreover, Lazzer et al. (2012) showed increased Cr during a multi-day competition by ~18% after the third day of race suggesting that Cr, along with $\dot{V}O_2\text{max}$ and F , explains 87% of the variance in the total race time. Conversely to previous works, Vernillo et al. (Vernillo et al. 2015b; Vernillo et al. 2014) showed lower Cr after mountain ultra-marathons. These authors reported unchanged or lower uphill Cr after 65-km and 330-km trail running competitions. Also, Cr on level did not change in both races. Authors explain the unchanged Cr by a greater eccentric contribution during level as compared with uphill running. They hypothesize that the return of elastic energy in the concentric phase of the stretch-shortening cycle may have compensated for any deficit in the force-generating capacity after the race and resulted in unchanged level-running steps mechanics that probably did not affect the level Cr (Vernillo et al. 2015b).

How can the cost of running be improved?

Several authors reported that different types of training can positively affect the Cr (Barnes and Kilding 2015) (Fig. 1.8) but most studies deal with different approaches to resistance training.

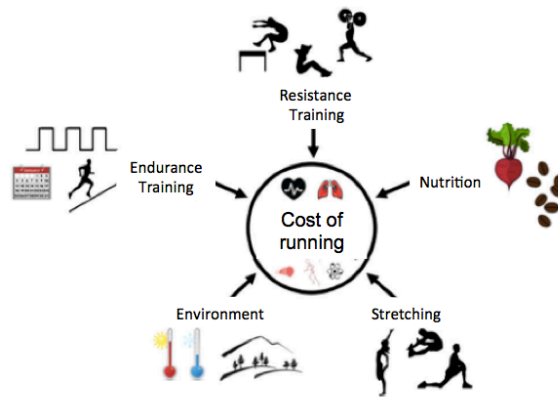


Fig. 1.8 – Schematic of strategies to improve running economy. Adapted from Barnes and Kilding (2015).

Indeed, strength, explosive and plyometric (SEP) training positively affect short (<15 minutes) and long (>15 minutes) endurance performance in different types of subjects and sport situations (Aagaard et al. 2011; Hakkinen et al. 2003; Hoff et al. 2002; Hoff et al. 1999; Millet et al. 2002; Paavolainen et al. 1999; Ronnestad et al. 2012; Ronnestad and Mujika 2014; Spurrs et al. 2003; Storen et al. 2008; Sunde et al. 2010; Turner et al. 2003). Moreover, lower values of Cr in trained runners were related with higher values of MMP and vertical stiffness supporting previous studies that underlined the role of muscle-tendon complex stiffness (MTS) in storing and releasing elastic energy and the importance of a good ankle stability (Spurrs et al. 2003). SEP training affects the performance without affecting $\dot{V}O_2\max$, lactate threshold and body weight (Hoff et al. 1999; Millet et al. 2002; Spurrs et al. 2003; Storen et al. 2008; Turner et al. 2003). Indeed, adding strength training to an athlete's usual endurance training may improve endurance performance by acting on exercise economy, anaerobic capacity, maximal speed and reducing the fatigue effects (Ronnestad and Mujika 2014). Mechanisms involved in improving performance consequently of concurrent strength and endurance training include an increased proportion of more fatigue-resistant type IIA fibers and reduced proportion of type IIX fibers (Aagaard et al. 2011). This adaptation results in an increased maximal muscle strength and RFD without any change in body mass nor in muscle fiber size (Aagaard et al. 2011). Also, in activity where the stretch-shortening cycle is involved and the storage and return of elastic energy plays an important role such as running, explosive strength training (Spurrs et al. 2003) and heavy strength training (Millet et al. 2002) added to normal endurance training can increase the MTS, which may improve the storage and release of elastic energy (Spurrs et al. 2003).

Walking and running mechanics

The gait cycle

The gait cycle begins when one foot touch the ground and ends when the same foot contacts the ground again. These moments are referred to as initial contact (or heel strike, HS). Stance ends when the foot is no longer in contact with the ground. Toe off (TO) marks the beginning of the swing phase of the gait cycle. The stance phase in walking is longer than 50%. This part of the gait cycle is referred as duty factor (i.e. the percent of the total cycle which a given foot is on the ground). In walking there are two periods of double support whilst in running *usually* there are no periods when both feet are in contact with the ground (Novacheck 1998) (Fig. 1.5). However, distinguish walking and running just from the presence or not of the aerial phase is not always correct. Indeed, more appropriate is to differentiate running from walking by analyzing the center of mass (CoM) trajectory.

The CoM trajectory and the spring-mass model

In walking, the CoM reaches its lowest point near toe-off and highest at mid-stance (MS) where the leg is relatively straight. During running, the CoM reaches its highest point during the aerial phase and lowest at MS, when the hip, knee and ankle are flexed (Bramble and Lieberman 2004). This latest definition is true also when humans run without an aerial phase. Indeed, McMahon first defined this running pattern as “Groucho running” (McMahon et al. 1987) whereas Rubenson et al. (2004) named it “grounded running”. Groucho (or grounded) running requires increased knee flexion. In this posture, contact time increases until the aerial phase disappears entirely. However, with this running pattern, CoM continues to reach its lowest height near MS and the bouncing gait is present, as is the case with “normal” running.

Video analysis and force plate can be used to investigate walking and running mechanics. Indeed, with these devices is possible to compute the total work done during gait. In pioneering age (Fenn 1930) studied first a model in which the total work (W_{tot}) done to move the body during walking and running is the sum of the external work, done to accelerate and lift the CoM (W_{ext}), and the internal work, done to accelerate the limbs relatively to the CoM (W_{int}). The positive work done by the muscles derives from the chemical energy transformed by their contractile machinery and the

mechanical energy stored in the muscles and tendons complex. The ratio of the positive work done by the muscles to the chemical energy used (e.g. efficiency) gives an indication of the role of the elastic energy returned during locomotion. Indeed, values greater than 0.25 (which is the efficiency of the concentric contraction) indicate that part of the positive work is “free of cost” and it is permitted by elastic elements stretched by some external force during a preceding phase of negative work. Cavagna and Kaneko (1977) reported that the efficiency during walking is always lower than during running and it reaches a maximum (0.35-0.40) at intermediate speeds. Conversely, during running it increases linearly with speed, attaining values of ~0.50.

The different efficiency between walking and running can be explained by the different mechanism involved in the two gaits. The difference in phase of potential and kinetic energy in walking (Fig. 1.5) suggests that the mechanism of walking is similar to that of a “rolling egg” or a pendulum (Cavagna et al. 1976). Indeed, during walking an inverted pendulum mechanism exchanges forward kinetic energy (E_{kf}) for gravitational potential energy (E_p) between heelstrike (HS) and MS; the exchange is reversed between MS and TO. Conversely, in running, the potential and kinetic energy are in phase, as in a “bouncing ball”. Leg tendons and ligaments partially store the elastic strain energy (E_{es}) derived from the decrease of E_p and E_{kf} during the first half of the stance, which is subsequently returned between MS and TO (Bramble and Lieberman 2004). The bouncing ball model was proposed by Cavagna et al. (1964) and more recently it was developed by McMahon and Cheng (1990) into the spring-mass model. In this model the legs can be described as springs loaded by the runner’s body mass (Blickhan 1989). The main mechanical parameter studied when using the spring-mass model is the stiffness of the leg spring (k_{leg}), which is defined as the ratio of the maximal force and the leg deformation (ΔL) at the middle of the stance phase. Also, the vertical stiffness (k_{vert}) is calculated by the ratio of the maximal force and the displacement of CoM (Δz) at the middle of the stance phase (Farley and Gonzalez 1996; McMahon and Cheng 1990). Measurement of the maximal ground reaction forces (F_{max}) and Δz during running required expensive equipment (i.e. force plate, video-motion analysis). However, Morin et al. (2005) validated a method for assessing leg and vertical stiffness during running. Given athlete’s leg length (L , in m), body mass (BM, in kg), contact and aerial time (t_c and t_a , in s) and running velocity (v , $m \cdot s^{-1}$) k_{vert} (in $kN \cdot m^{-1}$) can be calculated as follows:

$$k_{vert} = \frac{F_{max}}{\Delta z} \quad (2)$$

with

$$F_{max} = BMg \frac{\pi}{2} \left(\frac{t_a}{t_c} + 1 \right) \quad (3)$$

and

$$\Delta z = -\frac{F_{max}}{m} \frac{t_c^2}{\pi^2} + g \frac{t_c^2}{8} \quad (4)$$

then, k_{leg} (in $\text{kN} \cdot \text{m}^{-1}$) can be calculated as:

$$k_{leg} = \frac{F_{max}}{\Delta L} \quad (5)$$

with

$$\Delta L = L - \sqrt{L^2 - \left(\frac{vt_c}{2} \right)^2} + \Delta z \quad (6)$$

Ground reaction forces

Ground reaction forces (GRF) are used to quantify impacts, understand propulsion and braking, compute muscle forces, and calculate mechanical energy fluctuations (Gottschall and Kram 2005). These forces are dependent from the running speed, running pattern, characteristics and inclination of the terrain. For instance, during uphill and downhill running GRF behaves in different way compared to level running (see “*Uphill and downhill running*” paragraph).

GRF have three components: vertical, horizontal and mediolateral. The vertical component presents two peaks in rear-foot strikers while in mid-foot and fore-foot strikers there is only an active peak. At a moderate pace of $3 \text{ m} \cdot \text{s}^{-1}$, for runners who land on their rear-foot, the vertical component of the GRF quickly rises and falls, forming the impact peak (~ 1.6 body weight). The vertical component then more slowly increases to a second peak at mid-stance, termed the active peak (~ 2.5 BW), before decreasing prior to toe-off. The horizontal component is negative at foot strike, since a braking force is applied reaching a minimum (~ 0.3 BW) at about one-quarter of stance time before decreasing in magnitude and becoming positive during the propulsion phase prior to toe-off (Fig. 1.9)

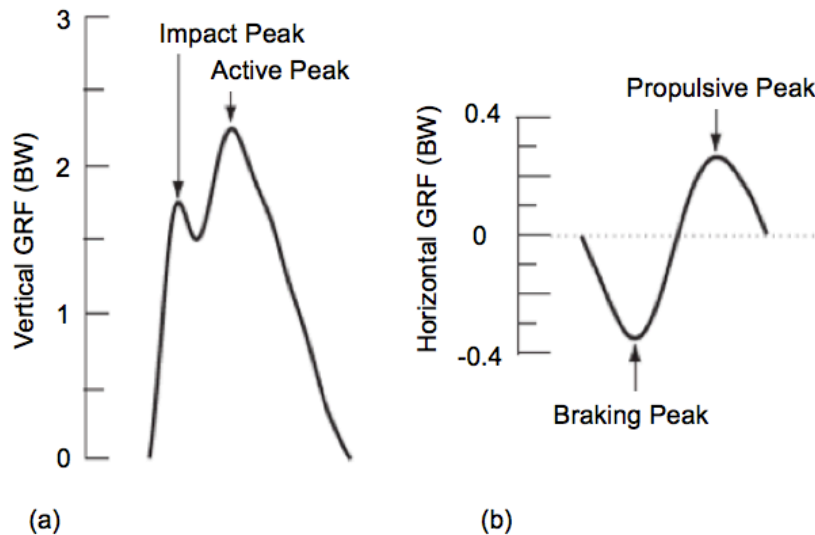


Fig. 1.9 - Typical traces of the vertical (a) and horizontal (b) GRF during level running at 3 m·s⁻¹. Adapted from Gottschall and Kram (2005).

The mediolateral component is usually small compared to the vertical and anteroposterior components. Indeed, it equals to 9% of the peak vertical component and 26% of the horizontal component (Cavanagh and Lafortune 1980).

Running mechanics in ultra-endurance events: does it change?

In the latest years many researchers attempted to clarify how the running biomechanics change during long-lasting events. Few years ago authors (Millet et al. 2009) examined the physiological and biomechanical changes occurring in a subject after running 8,500 km in 161 days. They reported that contact time (t_c) did not change but there was a tendency toward a “smoother” running pattern with higher step frequency (SF) and duty factor (DF) with lower aerial time (t_a), maximal vertical GRF (F_{max}) and loading rate at impact. In the following years different groups have studied the ultra-endurance performance in different situations. All studies agree that F_{max} decreases with the distance covered but there is not agreement about other biomechanical parameters' behavior. Indeed, some authors (Degache et al. 2013; Morin et al. 2011a) reported similar changes both after a 5-hour hilly running and 24-hour treadmill running. Indeed, they showed an increase in SF caused by a decrease in t_c with constant t_a . Further, spring-mass parameters (Δz and ΔL) decreased significantly. Consequently, vertical and leg stiffness increased. After a 160 km mountain ultra marathon (MUM) authors reported a similar trend but in this event t_a decreased (Morin et al. 2011b). Also, Vernillo et al. (2014) studied the world's most challenging MUM (Tor des Geants: 330

km, 24,000 m elevation gain) on energetics and mechanics of running in two conditions (level running at 9 km/h and uphill running at 6 km/h with an inclination of 15%). No differences were reported during the level-running condition while in uphill running t_c and DF increased. Similar results were reported after a 65 km MUM with higher t_c , DF and SF and shorter stride length (SL) (Vernillo et al. 2015b).

Differences among these studies may be in part explained by the different experimental design (treadmill vs. overground running) and different racecourses (distance, flat or with elevation gain/loss).

Relationships between Cr and mechanical parameters

Stride frequency and stride length

As speed is the product of SF and SL, a wide range combinations is possible for a given speed. Usually runners adopt a SF which is very close to the energetically optimal SF (i.e. less expensive) (Cavanagh and Williams 1982), which is between 85 and 90 strides $\cdot \text{min}^{-1}$ for a range of speeds below $6 \text{ m} \cdot \text{s}^{-1}$ (Cavanagh and Kram 1989; Cavanagh and Williams 1982). Cavanagh and Kram (1989) reported that as speed increased in the range of $3.15\text{-}4.12 \text{ m} \cdot \text{s}^{-1}$, SF remained nearly constant (+4%) while SL increased by 28%. Runners adjust their SL in order to minimize the metabolic Cr when running speed changes.

Vertical stiffness

Authors (Heise and Martin 1998) found inverse relationships between vertical stiffness (k_{vert}) and the Cr, suggesting that higher stiffness led to lower Cr. Thus, changes in stiffness with fatigue may help to explain increased metabolic cost in endurance and ultra-endurance running. Stiffness coefficients play a role in determining the final performance in running. Indeed, it is reported that higher k_{vert} corresponds to lower Cr (Dalleau et al. 1998). Thus, greater plantar flexor muscle strength and greater tendon-aponeurosis stiffness in the triceps surae lead to lower Cr (Arampatzis et al. 2006).

Muscle tendon stiffness

Also, authors underlined the role of muscle-tendon complex stiffness (MTS) in storing and releasing elastic energy and the importance of a good ankle stability (Spurrs et al. 2003). Indeed, in activities where the stretch-shortening cycle is involved and the storage and return of elastic energy plays an important role such as running, a high MTS may improve the storage and release of elastic energy. Higher MTS can be attained by adding explosive strength training (Spurrs et al. 2003) and heavy strength training (Millet et al. 2002) to normal endurance training.

Uphill and downhill running

Uphill running was studied first by Margaria (1938) and in more recent years authors studied different gradients/gaits combinations (Minetti et al. 1994a; Minetti et al. 2002). The increase number of uphill competitions stimulated this exploration. Indeed, there are uphill running races of various distance and inclination. Uphill running requires higher cost of running (Margaria 1938; Minetti et al. 1994a; Minetti et al. 2002), and lower vertical GRF (Gottschall and Kram 2005). During uphill running the energy demand increases linearly up to +0.45. At this steep gradient, it is ~5 fold higher than on level ground. Conversely, the energy cost of running decreases in downhill and reaches a minimum at approximately -20% (Minetti et al. 2002) (Fig. 1.10).

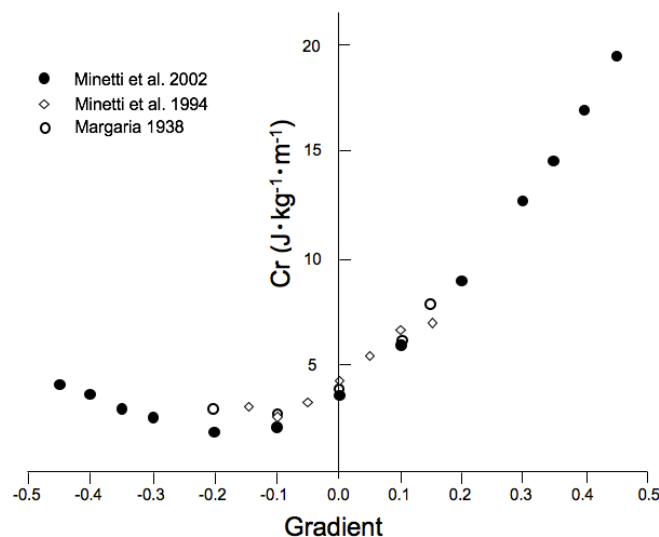


Fig. 1.10 - Metabolic energy cost of running as a function of the gradient from the works of Margaria (1938), Minetti et al. (1994a) and Minetti et al. (2002). Adapted from Minetti et al. (2002) .

Also the GRF are dependent on the gradient. Indeed, Gottschall and Kram (2005) reported that in downhill running the impact peaks were dramatically larger compared to level running and they were smaller in uphill running (Fig. 1.11). Particularly, compared to level running, at -9° the normal impact peak of the vertical GRF increased by 54%. The horizontal braking force peaks were larger for downhill running and smaller for uphill running. Running at -9° the parallel braking force peaks increased by 73% and during uphill running at 9° it decreased by 54%.

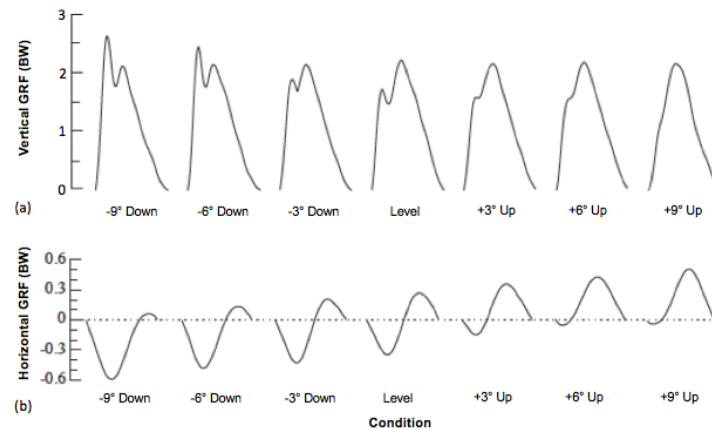


Fig. 1.11 - Vertical (a) and horizontal (b) ground reaction forces versus time traces for a 73-kg subject running at $3 \text{ m} \cdot \text{s}^{-1}$. Adapted from Gottschall and Kram (2005).

In level running, gravitational potential energy and kinetic energy of the CoM fluctuations are symmetrical and in-phase (Fig. 1.5). Part of this energy is stored elastically in the tendons and subsequently recovered (Cavagna et al. 1977). Conversely, in downhill and uphill running, some net mechanical energy dissipation and generation is required. Minetti et al. (1994a) reported that positive external work per unit distance decreased linearly with slope during downhill running and increased linearly with slope during uphill running. At angles steeper than $\pm 17\%$, exclusively negative and positive work is performed. Further, other authors (Snyder et al. 2012) reported that at -9° mechanical energy must no longer be generated while when running uphill additional energy must be generated to offset reduced elastic energy storage and return.

Conclusions of the general introduction

In this introduction we presented the physiological and mechanical determinants of endurance and ultra-endurance running. $\dot{V}O_{2\max}$, F and Cr are all factors that can be improved by specific training. Consequently, endurance and ultra-endurance performance can be enhanced. Further, in the latest years the interest for studying the running mechanics changes during ultra-endurance event has grown up.

Ultra-endurance running is a relatively new field of study that can provide new insight of the human behavior in extreme fatigue conditions. For this reason we designed a study to investigate the human reaction from a physiological and mechanical point of view. In the next part I will present the aims of this thesis and the works generated throughout the last three years.

AIMS OF THE THESIS

This thesis is divided into two parts. The first part elucidates the energetics and mechanics of ultra-endurance running whereas the second part describes the development of a device for the gait mechanical analysis.

Part I: The objectives of the first part were to examine the factors affecting the ultra-endurance performance and in particular which aspects influence the cost of running (Cr). Consequently, we defined how the Cr and running mechanics changed during different types (i.e. level and uphill) of ultra-endurance races. Finally, we proposed a specific training protocol for improving the Cr in high-level ultra-marathoners.

Part II: The aim of the second part was to develop and validate an insole shoe sensor to collect data about the ground reaction forces, contact and aerial times. I will present the different prototypes we developed and the one we used for the validation. This device should be flexible, comfortable and low cost. Moreover it should allow to collect data in the field without the use of force plate nor video analysis.

CHAPTER 2

PART I

MECHANICAL CHANGES DURING ULTRA-
ENDURANCE EVENTS AND THE EFFECTS OF A
SPECIFIC TRAINING ON THE COST OF
RUNNING

Introduction

As described in the previous chapters several factors affect the endurance and ultra-endurance performance. Physiological, mechanical, environmental, psychological and nutritional aspects influence the final results.

We confirmed that in ultra-endurance events the most important physiological factors determining the final performance are $\dot{V}O_2\text{max}$, F and Cr (Lazzer et al. 2014). Also, we reported that the mean velocity in this type of race can be predicted by the equation 1) previously proposed by other authors (di Prampero 2003; di Prampero et al. 1986).

In particular, we focused our efforts in studying the Cr under different conditions. In the first project (Lazzer et al. 2014) we analyzed the energetics and mechanics of running before and after a trail-running *flat* race (www.magraid.it). We reported that low Cr values before the race were related to high MMP and k_{vert} , and low foot print index (i.e. the mediolateral displacement of the foot during the stance phase, FPI) and W_{ext} (Lazzer et al. 2014). These results are important in suggesting that MMP , k_{vert} and FPI are relevant for the final performance. Thus, athletes may improve their results by acting on these parameters with specific training programs.

Since more recently uphill running races have become more popular among the athletic population, in another work (Lazzer et al. 2015) we studied the effects of an uphill-only race on the running mechanics and the Cr . We analyzed the changes occurred after the “Supermaratona dell’Etna”, (www.supermaratonadelletna.it), an uphill-only marathon from sea level to the top of Monte Etna, Sicily, Italy (43 km with 3000 m of elevation gain). In this study we compared pre- and post-race MMP , Cr and running mechanics. We concluded that there is a direct relationship between Cr measured before the race and performance time. Further, in agreement with other studies (Brueckner et al. 1991; Lazzer et al. 2014) the Cr increased with the distance covered by ~9%. This increase was associated with changes in running mechanics, particularly with a decrease in k_{vert} and k_{leg} . We hypothesized that the decrease of k_{vert} and k_{leg} due to fatigue, induced the runner to lower the CoM during contact, increasing t_c and Δz . Furthermore, the decreased stride frequency likely led runners to a less efficient elastic energy utilization (Snyder and Farley 2011). In this study an important role in determining the final performance was played by the MMP , which was related with ΔCr (i.e. the increase of the Cr during the race). Indeed, athletes with higher MMP showed a lower ΔCr , suggesting that MMP may limit the variation of the Cr .

In previous works (Lazzer et al. 2015; Lazzer et al. 2014) our group reported that ultra-endurance races induce changes both in running mechanics and energetics. However, in these studies we were not able to define at which point of the race such changes happen.

Thus, in another work (Giovanelli et al. 2015b) we investigated when (and at which point of the race) the running mechanics change during the Supermaratona dell'Etna. Studying the running mechanics at four different points of the race (at km 3, 14, 30 and immediately after the finish line) we could define when athletes changed their running pattern. Further, we evaluated the effect of race-induced fatigue on muscle contractile properties by using tensiomyography (TMG). Finally, we compared the fastest runners with the slowest ones to determine if the running mechanics changed in a different way between the two groups. The results of this work underlined once again the role of the MMP and k_{vert} in defining the performance. Moreover, we reported that the fastest athletes did not change their running mechanics throughout the race while it changed from the 30th km onward in the slowest runners suggesting that the spring-mass parameters change after a certain time of exercise performed (~4 hours) rather than after a certain amount of distance covered. Further, in this study we analyzed the muscle response to an electrical stimulus by using TMG. Our results showed a decrement in muscle stiffness and higher sensibility of the muscle to the electrical stimulus, suggesting that the potentiation of fast twitch fibers and the fatigue of the slow twitch fibers are two parallel mechanism involved in this type of race.

When considering uphill running performance, particular attention deserves the vertical kilometer (VK) foot races in which athletes have to cover 1000 m of elevation gain in less than 5 km. The mean slope in this competition can exceed 30° and athletes can choose running, walking and the combination of the two gaits. To the best of our knowledge, there were no prior scientific studies of human walking or running at the steep angles that are encountered in the fastest VK races. To date, the only study in which authors analyzed steep slopes was by Minetti et al. (2002). Authors measured the metabolic cost of walking (C_w) and running (C_r) on a range of slopes up to 24.2°. A new experimental design (Giovanelli et al. 2015a) explored steeper slopes than Minetti et al. by quantifying the metabolic costs of walking and running across a wide range of inclines up to and beyond those used in VK races. We also analyzed the mechanics of walking vs. running on steep inclines. We found that there is a range of

angles for which energy expenditure is minimized (between 20° and 35°). Further, at the vertical velocity tested ($0.35 \text{ m} \cdot \text{s}^{-1}$), on inclines steeper than 15.8°, athletes can reduce their energy expenditure by walking rather than running.

We reported (Giovanelli et al. 2015b; Lazzer et al. 2015; Lazzer et al. 2014) that in uphill-only race the running mechanics change after a certain time of exercise performed rather than a certain distance covered. Our next goal was to define if this happens also in *flat* races. In the race “6 ore città di Buttrio” athletes were required to run as many 874 m loops as possible in six hours. In this context we analyzed the running mechanics evolution every ~30 minutes of race to define whether and when any change occurs. The measurements performed and results obtained are explained in the following manuscript, which is currently in revision in the Int J Sports Physiol Perf.

Changes in running mechanics during a six hours running race

To date, different types of ultra-endurance race have been analyzed and from previous work it seems that the running mechanics change after a certain time of exercise performed rather than a certain distance covered (Giovanelli et al. 2015b). The aim of this study was to analyze continuous changes in running mechanics during a six hours running competition on an 874 m flat loop. We hypothesized an increase in t_c and a decrease in t_a and k_{vert} between the third and fourth hour of the race. Also, we hypothesized that during a flat running race the changes in biomechanical parameters were smaller when comparing with an uphill-only race of similar duration.

Materials and Methods

Participants

Nineteen healthy Italian male runners (age: 41.9 ± 5.8 years; body mass index: 22.3 ± 2.1 $\text{kg} \cdot \text{m}^{-2}$, Table 2.1) were enrolled in this study as participants in the “6 ore Città di Buttrio”. The experimental protocol was conducted according to the Declaration of Helsinki and it was approved by the Ethics Committee of the University of Udine. Before the study began, the purpose and objectives were carefully explained to each participant and written informed consent was obtained from all of them. The participants were recruited among experienced ultra-endurance runners (12.4 ± 8.5 years of training history in running and 6.5 ± 3.5 years of ultra-endurance running race experience; they reported to run on average 73.3 ± 19.5 km every week). Athletes were asked to fill out a questionnaire on physical exercise activity, demographics, medical history and lifestyle (Craig et al. 2003). All the nineteen athletes who were eligible for the study began the race but only 12 completed the entire competition. The athletes dropped out because of gastrointestinal problems ($n=4$) and muscular cramps ($n=3$). Therefore, only the runners who concluded the race ($n=12$) were taken into account for the data analysis.

Age (years)	41.9 ± 5.8	[33.0 - 56.0]
Body mass (kg)	68.3 ± 12.6	[51.0 - 86.0]
Stature (m)	1.72 ± 0.09	[1.62 - 1.90]
Body mass index ($\text{kg} \cdot \text{m}^{-2}$)	22.3 ± 2.1	[19.4 - 25.6]
L (m)	0.91 ± 0.05	[0.83 - 0.99]
$\dot{V}\text{O}_2\text{max}$ ($\text{mL} \cdot \text{kg}^{-1} \cdot \text{min}^{-1}$)	52.7 ± 5.0	[45.0 - 60.0]
Race distance (km)	62.9 ± 7.9	[47.4 - 79.5]

TABLE 2.1. Physical characteristics of participants measured before the race in the athletes who concluded the race (n: 12). All values are mean \pm standard deviation (SD). Range in square brackets. L: lower limb length; $\dot{V}O_2\text{max}$: maximal oxygen uptake.

Experimental design

The athletes were required to run as many 874 m flat loops as possible in six hours. In the week preceding the race, the participants were asked to come to the laboratory to perform a graded exercise test on a treadmill to evaluate their maximal oxygen uptake ($\dot{V}O_2\text{max}$). Athletes were also asked to refrain from performing any vigorous physical activity during the day preceding the test and during the preliminary testing session they performed to familiarize with the equipment. During the race, running mechanics in the first lap and every 30 minutes thereafter (± 2 minutes, depending on the athlete's position along the circuit) were evaluated. Athletes were free to choose their own running velocity during the race to achieve their best performance (i.e. the highest distance covered).

Physiological measurements before the race

Body mass (BM) was measured by a manual weighing scale (Seca 709, Hamburg, Germany) and stature by standardized wall-mounted height board. Then, body mass index (BMI) was calculated as $\text{BM (kg)} \cdot \text{stature}^{-2}$ (m). $\dot{V}O_2\text{max}$ ($\text{mL} \cdot \text{kg}^{-1} \cdot \text{min}^{-1}$) was measured by means of a graded exercise test on a treadmill (Saturn, HP Cosmos, Germany) as previously described elsewhere (Lazzer et al. 2015; Lazzer et al. 2014).

Mechanical measurements during the race

A digital camera with a sample frequency of 400 Hz (Nikon J1, Japan) has been used to record participants during the race. The camera was placed perpendicular to the running direction of the athletes in a flat section of the loop. Running velocity was measured by means of two photocells placed 20 m apart (Fig. 2.1). Five subsequent steps were analyzed in order to measure t_c (s) and t_a (s) (Giovanelli et al. 2015b; Morin et al. 2011b). Afterwards, step frequency (f , $\text{step} \cdot \text{s}^{-1}$) was calculated as $f = 1 / (t_c + t_a)$. Finally, the spring-mass model parameters (F_{max} , Δz , ΔL , k_{vert} , k_{leg}) were calculated using the method proposed by Morin et al. (2005).

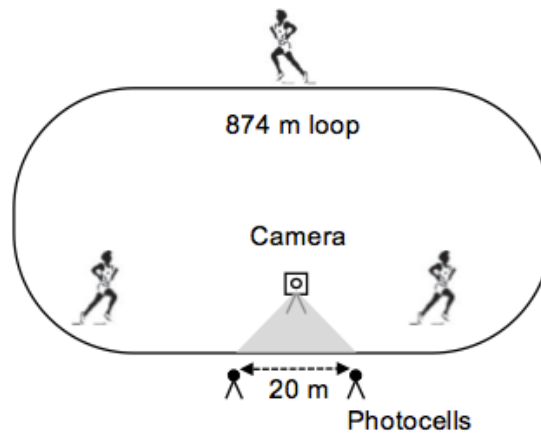


Fig. 2.1 – The experimental setup

Statistical analyses

Statistical analyses were performed using PASW Statistic 18 (SPSS Inc., IL, USA) with significance set at $p < 0.05$. All results are expressed as means and standard deviation (SD).

Normal distribution of the data was tested using the Kolmogorov-Smirnov test. Changes of speed and mechanical parameters during the race were studied with the General Linear Model repeated measures. When significant differences were found, a Bonferroni post-hoc test was run to determine the exact location of the difference. The magnitude of the changes was assessed using effect size (ES) statistic and percentage change. The interpretation of effect size was as follows: < 0.2 = trivial, $0.2-0.49$ = small, $0.5-0.79$ = medium, > 0.80 = large (Cohen 1992).

Results

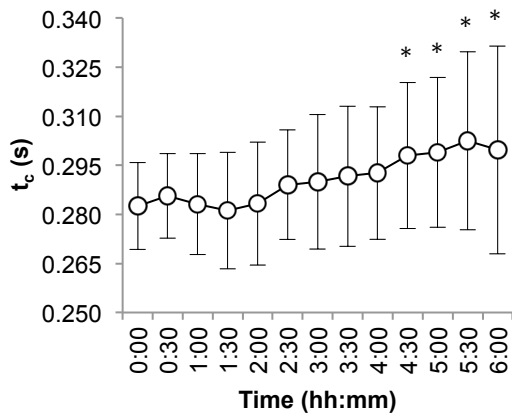
The physical characteristics of the participants measured before the race are reported in Table 1, together with the distance covered. The average running velocity during the race was $2.91 \pm 0.37 \text{ m} \cdot \text{s}^{-1}$.

Running velocity decreased significantly starting from 4h30' onward, compared to the running velocity measured at the first check point (first lap) (mean: $-5.6 \pm 0.3\%$; $p < 0.05$, $ES = 0.64$, medium).

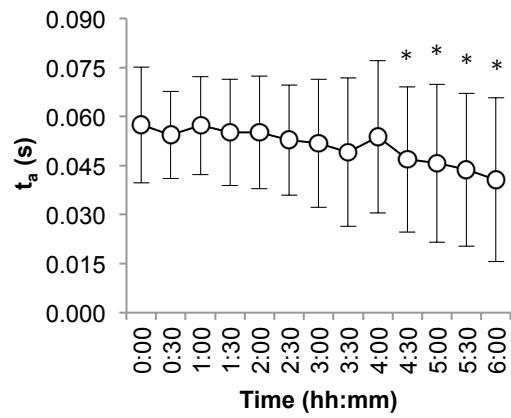
Figure 2.2 shows the trends of mechanical parameters during the race. All the changes are related to the first check point. Contact time (Fig. 2.2(a)) increased significantly from

4h30' onward, reaching the maximum difference at 5h30, (+6.1%, $p=0.015$, $ES=0.97$, large). Aerial time (Fig. 2.2(b)) and F_{max} (Fig. 2.2(c)) decreased significantly from 4h30' throughout the end of the race (mean: -29.2% and -5.1%, $p<0.05$ and $p<0.05$; $ES=0.55$ and $ES=0.72$, medium; respectively). Also, Δz (Fig. 2.2(d)) decreased only in the last check point (-6.5%, $p=0.02$; $ES=0.64$, medium). Consequently, k_{vert} (Fig. 2.2(e)) decreased significantly after 4h00' reaching the lowest value after 5h30' (-6.5%, $p=0.008$; $ES=0.33$, small). Finally, SL (Fig. 2.2(f)) decreased significantly from 5h00' throughout the end of the race (mean: -5.1%, $p=0.010$; $ES=0.41$, small).

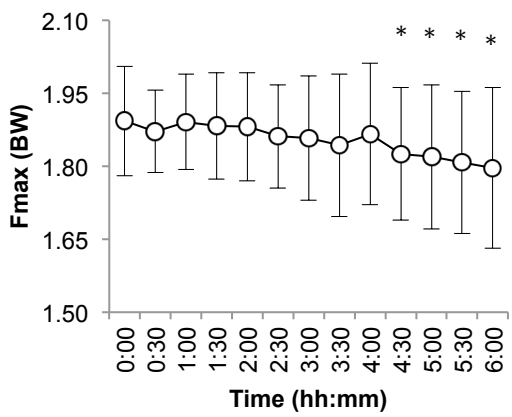
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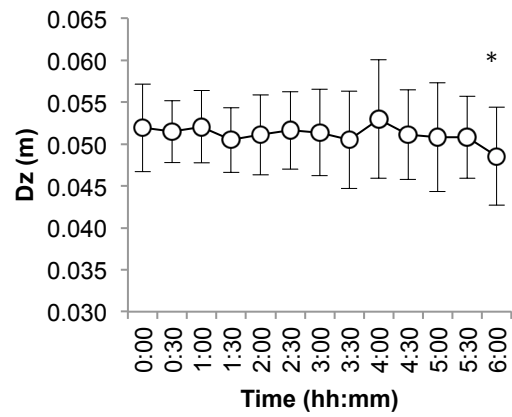
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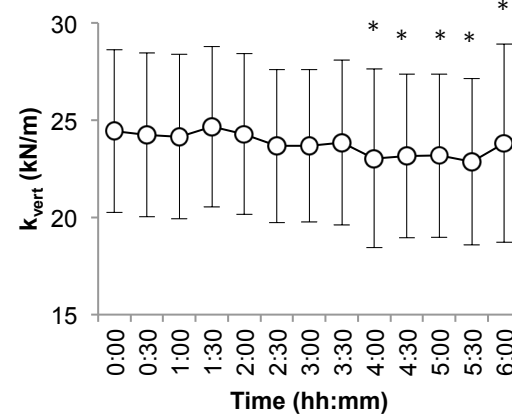
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e.



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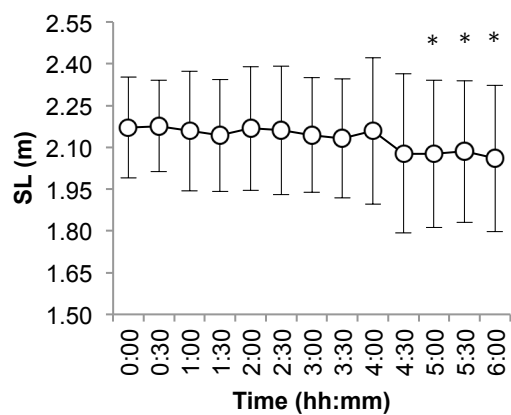


FIG. 2.2 – mechanical parameters measured every 30 minutes (a: contact time, t_c ; b: aerial time, t_a ; c: vertical ground reaction force, F_{max} ; d: vertical displacement of the center of mass, Δz); e: vertical stiffness, (k_{vert}); f: stride length, SL. *: $p < 0.05$, significantly different from the first point.

Discussion

The main results of the present study show that: 1) running mechanics change significantly after the fourth hour of exercise, regardless of absolute running velocity; and 2) athletes chose their preferred pace throughout all the race.

Running mechanics did not change in the first part of the race, rejecting our hypothesis that changes would be seen between the third and fourth hour of the race. Indeed, before the fourth hour we did not observe changes in the spring-mass model parameters, while at the fourth hour only k_{vert} changed. After 4^h30' of running, also F_{max} , t_a , t_c and SL changed significantly, suggesting that low-frequency fatigue affects the gait (Fourchet et al. 2012). Indeed, a lower force production capacity and/or a reduced stretch-shortening-cycle efficiency of the lower limb extensor muscles may affect the mechanical behavior after this time-threshold (Dierks et al. 2010; Fourchet et al. 2015). The decrease observed in F_{max} was in agreement with all previous studies that analysed both shorter and longer events than six hours (Degache et al. 2013; Giovanelli et al. 2015b; Girard et al. 2013; Lazzer et al. 2015; Lazzer et al. 2014; Morin et al. 2011a; Morin et al. 2011b; Rabita et al. 2011). In our study athletes decreased their F_{max} by -5.1% and this value is similar to the values reported by the abovementioned studies: -4.4% showed after a 24h treadmill running (Morin et al. 2011a), -6.3% after a mountain ultra-marathon (Morin et al. 2011b) and -2.4% after 5h hilly running (Degache et al. 2013). A greater difference is registered when our results are compared to the uphill-only marathon in which Lazzer et al. (2015) showed a decrease of -17.6% in F_{max} . This difference could be due to the peculiar elevation profile of the race analyzed in this study. As a matter of fact our results are comparable to those reported for longer (≥ 24 hours) races. An explanation could be that F_{max} decreases in the first few hours of exercise reaching a plateau after a certain time (~ 4 hours) of running as previously pointed out (Morin et al. 2011a). The decrease in F_{max} could be due to functional and structural alterations of muscle fibers as well as to an increase in the inflammatory status occurring during this kind of races, in particular in the downhill sections (Millet et al. 2011b; Saugy et al. 2013).

However, our results are not consistent with the findings of other studies (Degache et al. 2013; Morin et al. 2011a; Morin et al. 2011b) which demonstrate different trends for Δz , k_{vert} , k_{leg} , f , t_c and t_a . These authors showed an increase in k_{vert} due to a higher

decrease in Δz than in F_{\max} explaining these changes as the result of a research of a smoother and less traumatic way to run. However, in our study, k_{vert} decrease was due to a decrease in F_{\max} without changes in Δz , suggesting the inability of the system to maintain an optimal stiffness when the subject is running at constant speed in a fatigued state (Dutto and Smith 2002).

As we hypothesized, our results are in agreement with Lazzer et al. (2015) who analyzed running mechanics during an uphill-only race. Despite the fact that in uphill race the running pattern is different (Gottschall and Kram 2005; Padulo et al. 2012), we hypothesized that similar results could be achieved because of the similar duration of the race (~ six hours). Indeed, if we compare the present work with the work of Lazzer et al. (2015), changes in all parameters are smaller in a flat race compared to an uphill-only running race of similar duration (F_{\max} : -5.1 vs -17.6%; Δz : -6.5 vs +52.9%; ΔL : NS vs +44.5%; k_{vert} : -6.4 vs -45.6%; k_{leg} : -7.2 vs -42.3%; t_c : +6.1 vs +28.6%; t_a : -29.2 vs -58.6%). These differences could be due to the work done to elevate the center of mass during uphill running, which involves higher fatigue and bigger changes in running mechanics. Further, the different trend of Δz can be explained as the different effort sustained by the athletes (flat vs. uphill running). Also, Vernillo et al. (2015b) explained that changes in stiffness due to fatigue could induce the runners to generate force less rapidly, thus having longer t_c , according to the cost of generating force hypothesis proposed by Kram and Taylor (1990).

In sprint and middle-distance running events athletes start fast, then slow down (Hanon et al. 2010) and then increase their speed again in the last part of the race (Girard et al. 2013). Conversely, in endurance races, athletes try to keep a regular and comfortable pace for the whole duration of the event (Hoffman 2014). Considering the mean speed over the six hours, the average velocity was $2.91 \pm 0.37 \text{ m} \cdot \text{s}^{-1}$, which corresponds to $67.4 \pm 6.9 \%$ of the running velocity at $\dot{V}O_2\text{max}$, as reported by previous studies (Davies and Thompson 1979). This speed was slightly slower than the running velocity at which the mechanical analysis was carried out because it actually includes also the rest time to enable athletes to feed during the six hours. Unlike other protocols (Martin et al. 2010; Millet et al. 2011a; Morin et al. 2011a), athletes organized their own feeding strategy, so that we could not control when and how long for they rested during the race. However,

we supposed that these breaks did not affect running mechanics. Furthermore, we allow that the method we used to calculate the spring-mass parameters (Morin et al. 2005) is dependent upon ground contact times. Nevertheless, previous studies considered this model for measuring the changes in running mechanics during both short (Hobara et al. 2010) and long performance (Giovanelli et al. 2015b; Lazzer et al. 2015; Morin et al. 2011a; Morin et al. 2011b). In addition, the changes in running velocity (coefficient of variation $3.7\pm 2.6\%$) observed in this study were not great enough to affect the computation of the F_{\max} and k_{vert} . In effect, in agreement with previous study (Lazzer et al. 2015), a decrease of $-5.6\pm 0.3\%$ in the running velocity had only a partial effect on the changes in the mechanical parameters. As well, the range of speed accepted by Morin et al. (2011b) for calculation of the mechanical parameters during running was $\pm 5\%$ the reference speed ($3.33 \text{ m}\cdot\text{s}^{-1}$). In particular, Arampatzis et al. (1999) showed that k_{vert} did not change significantly for speeds ranging from 2.5 to $3.5 \text{ m}\cdot\text{s}^{-1}$, which are very similar to the range of speeds that our athletes maintained throughout the whole race (min= $2.4 \text{ m}\cdot\text{s}^{-1}$; max= $3.9 \text{ m}\cdot\text{s}^{-1}$).

Conclusions

In conclusion, we observed that, most mechanical changes happen after four hours of continuous running. This suggests the existence of a “time threshold” that could affect performance regardless of absolute running speed. Future studies should focus on the reason why spring-mass model changes after this “threshold”, proposing some specific training to preserve the correct running mechanics for more hours.

Effects of strength, explosive and plyometric training protocol on energy cost of running in high-level ultra-endurance athletes

As extensively reported throughout this thesis, Cr plays an important role in determining the performance and it is affected by several factors. We suggested to add strength and explosive training in the ultra-marathoners training program because an increase in MMP might lead to a decrease in Cr (Lazzer et al. 2015; Lazzer et al. 2014). Thus, our next objective was to evaluate the effects of a 12-week of strength, explosive and plyometric (SEP) training protocol on the Cr in ultra-marathoners and to define which biomechanical parameters and anthropometric characteristics of the gastrocnemius medialis and Achilles tendon affected the Cr. The experiments performed and the results of this study are exposed in the below manuscript, which is actually in revision of the Eur J Appl Physiol.

Effects of strength, explosive and plyometric (SEP) training on short (<15 minutes) and long (>15 minutes) endurance performance have been extensively studied in different populations and sport situations (Aagaard et al. 2011; Hakkinen et al. 2003; Hoff et al. 2002; Hoff et al. 1999; Millet et al. 2002; Paavolainen et al. 1999; Ronnestad et al. 2012; Ronnestad and Mujika 2014; Spurrs et al. 2003; Storen et al. 2008; Sunde et al. 2010; Turner et al. 2003). Cyclists, rowers, triathletes and runners underwent different types of training protocols to improve the endurance performance, but literature misses data about ultra-marathoners. Several sports are analyzed in the above-mentioned studies. Although different points of view are present between authors, it appears that the optimal training regime includes concurrent strength, explosive and plyometric exercises added to endurance training. Indeed, concurrent endurance and strength training may improve endurance performance more than endurance training alone (Aagaard et al. 2011; Hoff et al. 1999; Spurrs et al. 2003; Storen et al. 2008).

The first objective of the present study was to evaluate the effects of a 12-week SEP training protocol on the Cr in high-level ultra-marathoners. We hypothesized I) a decrease in Cr and we expected II) higher MMP of the lower limbs. Secondly, if the training protocol led to a decrease in cost of running, we aimed to define which factors affect this change analysing some running mechanical parameters and some characteristics of the Achilles tendon and gastrocnemius medialis (GM). We also hypothesized that SEP training led III) higher tendon stiffness.

Materials and methods

Participants

Twenty-five male runners (38.2±7.1 years; BMI: 23.0±1.1 kg·m⁻²; $\dot{V}O_2$ max: 55.4±4.0 mlO₂·kg⁻¹·min⁻¹, Table 2.2) participated in this study and provided informed consent. The experimental protocol was approved by the Ethics Committee of the University of Udine, Italy. The participants were recruited among Italian high-level ultra-endurance runners (both road- and trail-runners); some of them joined the national team in the latest two years (Italian Ultra-Marathon and Trail Association, IUTA). The inclusion criteria were: the athletes had run at least one race longer than 50 km and their training volume in the latest 3 months was more than 60 km·week⁻¹. Further, they did not perform strength training in the last six months and none of the athletes had a history of neuromuscular or musculoskeletal impairments at the time of the study that could affect the results.

On average their training experience amounted to (mean ± s.d.) 11.7±8.6 years, of which 4.7±3.4 years involved in ultra-endurance running. They reported to run on average 88.0±33.1 km·week⁻¹ and their personal best on marathon race and 100 km race were (hours:minutes) 3:00±0:17 and 9:00±1:56, respectively.

	All runners (n: 25)		Control group (n:12)	Exercise group (n:13)	P
Age (years)	38.2 ± 7.1	[26.0 - 51.0]	40.3 ± 6.5	36.3 ± 7.4	0.17
BM (kg)	71.3 ± 8.5	[59.0 - 93.0]	70.7 ± 7.9	71.9 ± 9.4	0.721
Height (m)	1.75 ± 0.07	[1.65 - 1.84]	1.75 ± 0.07	1.76 ± 0.08	0.797
BMI (kg·m ⁻²)	23 ± 1.1	[20.3 - 24.9]	22.9 ± 1.3	23.1 ± 0.9	0.735
FFM (kg)	55.6 ± 6.2	[45.8 - 71.7]	55.7 ± 7.2	55.4 ± 5.4	0.901
FM (kg)	15.8 ± 4.6	[8.2 - 27.7]	14.9 ± 3.9	16.5 ± 5.2	0.404
FM (%BM)	21.9 ± 4.7	[12.6 - 29.8]	21.1 ± 4.8	22.6 ± 4.7	0.44
$\dot{V}O_2$ max (ml·kg ⁻¹ ·min ⁻¹)	55.4 ± 4	[50.0 - 64.0]	55.6 ± 4.1	55.2 ± 4	0.831
RERmax	1.15 ± 0.04	[1.06 - 1.22]	1.16 ± 0.04	1.14 ± 0.04	0.187
HRmax (bpm)	176 ± 9.1	[160 - 193]	175.6 ± 8.1	176.9 ± 10.2	0.736
vmax (km·h ⁻¹)	17.6 ± 0.9	[16.1 - 19.6]	17.7 ± 0.8	17.6 ± 0.9	0.849
v $\dot{V}O_2$ max (km·h ⁻¹)	17.2 ± 0.8	[16.1 - 18.9]	17.2 ± 0.7	17.2 ± 0.7	0.797
Gas exchange threshold					
$\dot{V}O_2$ (ml·kg ⁻¹ ·min ⁻¹)	46.8 ± 3.1	[41.0 - 53.1]	46.7 ± 2.6	46.9 ± 3.6	0.79
$\dot{V}O_2$ (% $\dot{V}O_2$ max)	84.6 ± 3.8	[78.9 - 92.4]	84.1 ± 4.2	85.1 ± 3.5	0.528
RER	0.97 ± 0.01	[0.89 - 1.05]	0.97 ± 0.03	0.96 ± 0.04	0.546
RER (%RERmax)	84 ± 2.8	[79.0 - 90.0]	83.6 ± 3	84.6 ± 2.6	0.433
HR (bpm)	166 ± 9.1	[151 - 184]	165.1 ± 9.4	167.8 ± 9.2	0.64
HR (%HRmax)	94.2 ± 1.8	[90.1 - 97.0]	94 ± 1.7	94.4 ± 1.9	0.597
v (km·h ⁻¹)	15.7 ± 0.5	[14.7 - 16.8]	15.7 ± 0.6	15.7 ± 0.4	0.716
v (%v $\dot{V}O_2$ max)	91.4 ± 2.2	[88.0 - 95.8]	91.9 ± 2.3	91 ± 2.1	0.329

Table 2.2. Physiological characteristics of the subjects. All values are means ± s.d. BM: body mass; BMI: body mass index; FFM: fat-free mass; FM: fat mass; $\dot{V}O_2$ max: maximal oxygen uptake; RER: respiratory exchange ratio; HR: heart rate; vmax: maximal running speed; v $\dot{V}O_2$ max: running speed at $\dot{V}O_2$ max. P: unpaired t-test between Control and Exercise groups.

Experimental design

Subjects came into the laboratory three times. During the first visit, the athletes were fully informed regarding the experimental procedures, underwent a medical examination and particularly attention was paid to familiarize them with all the procedures.

During the second visit (PRE), body mass (BM), height, body composition, morphological properties of the GM, triceps surae tendon stiffness (k_{tendon}) and MMP were determined. Then, Cr and spring-mass model parameters at four speeds (8, 10, 12 14 $\text{km}\cdot\text{h}^{-1}$) were calculated before performing a maximal test on a motorized treadmill. We used this test for determining anaerobic threshold, maximal oxygen uptake ($\dot{V}\text{O}_2\text{max}$) and the velocity associated with $\dot{V}\text{O}_2\text{max}$ ($v\dot{V}\text{O}_2\text{max}$).

After the second visit the subjects were randomly split into two homogenous groups (exercise group, EG, $n=13$; control group, CG, $n=12$). The EG added a 12-week SEP training protocol to its normal running training whilst the CG continued its usual running training.

Immediately after the 12-week SEP training protocol, EG and CG came into the laboratory for the third visit (POST) and performed the identical procedures done during the second visit.

Anthropometric characteristics and body composition

Body mass (BM) was measured with a manual weighing scale (Seca 709, Hamburg, Germany). Height was measured on a standardized wall-mounted height board. Body mass index (BMI) was then calculated as body mass (kg) \cdot height (m)⁻². Body composition (fat-free mass, FFM and fat mass, FM) was measured by bioelectrical impedance analysis (BIA, Akern, Florence, Italy) according to the method of Lukaski et al. (1986).

Energy cost of running and maximal oxygen uptake

Metabolic rate at 8, 10, 12 and 14 $\text{km}\cdot\text{h}^{-1}$ were measured during four steady state steps performed before a maximal test on a motorized treadmill (Saturn, HP Cosmos, Nußdorf, Germany) under medical supervision. Ventilation, oxygen consumption ($\dot{V}\text{O}_2$)

and carbon dioxide production ($\dot{V}CO_2$) were measured continuously with a metabolic unit (Quark-b², Cosmed, Rome, Italy). The volume and gas analyzers were calibrated before every trial as described elsewhere (Lazzer et al. 2014). Heart rate was measured with a dedicated device (Polar, Kempele, Finland).

The test included a 5 minutes rest period followed by 4 running steps at 8, 10, 12, 14 km·h⁻¹ for 5 minutes each; then, the speed was increased by 0.7 km·h⁻¹ every minute until the volitional exhaustion.

After subtracting the metabolic rate measured during the standing phase to the gross metabolic rate, the Cr (in mlO₂·kg⁻¹·m⁻¹) at 8, 10, 12 and 14 km·h⁻¹ was calculated as the ratio between the net $\dot{V}O_2$ (averaged in the last minute of every step (Lazzer et al. 2014)) and the corresponding running speed. Respiratory exchange ratio (RER= $\dot{V}CO_2/\dot{V}O_2$) was required to be lower than 1.0.

During the incremental test, a leveling off of oxygen uptake (defined as an increase of no more than 1 ml·kg⁻¹·min⁻¹) was observed in all subjects during the last one or two minutes indicating that $\dot{V}O_{2max}$ was attained. $\dot{V}O_{2max}$ and maximal heart rate (HR_{max}) were calculated as the average $\dot{V}O_2$ and HR of the last 30 s of the test.

The gas exchange threshold was then determined by the V-slope method (Beaver et al. 1986).

Mechanical measurements

Running mechanics were studied at four different speeds (8, 10, 12, 14 km·h⁻¹) using a digital camera with a sample frequency of 400 Hz (Nikon J1, Japan). The camera was placed next to the treadmill and ten subsequent steps between the 4th and the 5th min were analyzed in order to measure contact (t_c , s) and aerial (t_a , s) time. Step frequency (f , step·s⁻¹) was then calculated as: $1/(t_a+t_c)$.

Given t_c (s), t_a (s), v (m·s⁻¹), subject's BM (kg), and lower limb length (distance between great trochanter and ground during standing, L in m), spring-mass model parameters were calculated using the method proposed by Morin et al. (2005).

Maximal power of the lower limbs

The MMP during a SJ was assessed by means of the Explosive-Ergometer (EXER, University of Udine, Italy), previously described elsewhere (Lazzer et al. 2014). Subjects were asked to perform four all-out SJ starting from a knee angle of 110 degrees with two minutes of rest interval between each trial. The starting position was assured by two blocks, which prevent any counter-movement. The MMP was obtained from the instantaneous product of the developed force (F, N) multiplied by the backward speed ($v, m \cdot s^{-1}$). The SJ with the highest peak of power was taken into account for the analysis.

Further, morphological properties of the gastrocnemius medialis and triceps surae tendon stiffness were measured as previously described (Lazzer et al. 2014).

Training protocol

EG underwent a 12-week training protocol adding three training sessions per week to its usual running training. Athletes performed the training protocol at their home on alternate days avoiding the day after races or after high intensity or long (>2 hours) training sessions.

The training protocol was divided into three 4-week macro-cycles.

The sessions in the first cycle included three exercises for the core, three exercises for the running technique and four strength exercises for the lower limbs.

The sessions in the second and third cycle included two plyometric exercises and five explosive exercises for the lower limbs. In these two cycles, after a familiarization period, three exercises were performed on unstable board (Disc'o'Sit, Ledraplastic, Osoppo, Italy).

Participants underwent 5-8 exercises three times per week. 1-3 sets for 6-15 repetitions were performed for each exercise. The sessions lasted about 25-30 minutes and athletes were free to undergo the workout without rest or with a short rest (<30 seconds) between each exercise. All the exercises were performed without weight loading. During the first two weeks, athletes were supported by a research assistant, who verified that athletes performed the exercises correctly.

Conversely, the CG continued to perform its normal endurance training, including 5-7 running session per week.

Statistical analyses

Statistical analyses were performed using PASW Statistic 18 (SPSS Inc., Chicago, IL, USA) with significance set at $p < 0.05$. All results are expressed as means and standard deviation (SD). Normal distribution of the data was tested using the Kolmogorov-Smirnov test. Sphericity (homogeneity of covariance) was verified by the Mauchly's test.

Changes of anthropometrics characteristics, body composition, morphological properties of the gastrocnemius medialis, triceps surae tendon stiffness, MMP, anaerobic threshold and $\dot{V}O_2\text{max}$ were studied with a general linear model repeated measures considering two factors (time: PRE and POST; group: CG and EG).

Changes of Cr, biomechanical and spring-mass model parameters were studied with a general linear model repeated measures considering three factors (speed: 8, 10, 12, 14 $\text{km}\cdot\text{h}^{-1}$; time: PRE and POST; group: CG and EG). When significant differences were found, a Bonferroni post hoc test was used to determine the exact location of the difference.

In addition, the relationships between changes in mechanical parameters, MMP, morphological properties of the gastrocnemius medialis and triceps surae tendon variables affecting Cr were investigated using Pearson's product-moment correlation coefficient.

Results

Characteristics of the athletes

All the subjects included in the EG completed more than 95% of the training program (self-reported). The physiological characteristics of the athletes measured at PRE are reported in Table 1. No significant differences were found between CG and EG on anthropometrics (BMI: 22.9 ± 1.3 vs. 23.1 ± 0.9 $\text{kg}\cdot\text{m}^{-2}$, $p=0.735$) and body composition (%FM: 21.1 ± 4.8 vs. $22.6 \pm 4.7\%$, $p=0.440$) characteristics. As well, no significant differences were found in $\dot{V}O_2\text{max}$ (55.6 ± 4.1 vs. 55.2 ± 4.0 $\text{ml}\cdot\text{kg}^{-1}\cdot\text{min}^{-1}$, $p=0.831$), $\dot{V}O_2$ at GET (46.7 ± 2.6 vs. 46.9 ± 3.6 $\text{ml}\cdot\text{kg}^{-1}\cdot\text{min}^{-1}$, $p=0.790$) and speed at GET (15.7 ± 0.6 vs. 15.7 ± 0.4 $\text{km}\cdot\text{h}^{-1}$, $p=0.716$) between the two groups. There were no significant differences between PRE and POST in the above mentioned parameters both when athletes were analyzed all together and when they were analyzed split in CG and EG.

Further, no differences in mechanical parameters, spring-mass model parameters and MMP were detected between PRE and POST in the CG.

Energy cost of running

At PRE, no significant differences were shown in Cr between CG and EG. Further, when all subjects were analyzed together Cr at 8 km·h⁻¹ was significantly higher than Cr at other selected speeds (+6.5±2.0% on average, p<0.001). Conversely, Cr was not significantly different between 10, 12 and 14 km·h⁻¹ (p>0.05).

At POST, Cr decreased significantly in EG at all tested running speeds (-6.4±6.5%, p=0.005, at 8 km·h⁻¹; -3.5±5.3%, p=0.032, at 10 km·h⁻¹; -4.0±5.5%, p=0.020, at 12 km·h⁻¹; -3.2±4.5%, p=0.022, at 14 km·h⁻¹, Fig. 2.3). In addition, Cr was significantly lower in EG than CG at every tested speed (-6.2±1.7% on average, p<0.05).

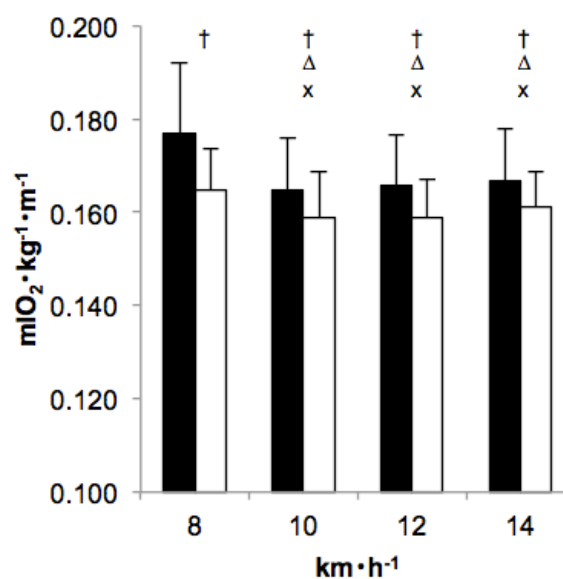


Fig 2.3. Cr (mlO₂·kg⁻¹·m⁻¹) as a function of speed (km·h⁻¹) in EG (n=13), before (PRE, black bars) and after (POST, white bars) the training protocol. †: significantly different POST vs. PRE; Δ: significantly different compared with 8 km·h⁻¹ PRE; x: significantly different compared with 8 km·h⁻¹ POST.

Running mechanics and spring-mass model parameters

At PRE, no significant differences were shown in spring-mass model parameters between CG and EG.

As well, in the EG contact time (t_c , Fig. 2.4A) decreased by mean $-8.9\pm 4.2\%$ as a function of speed. Further, in the EG the following mechanical parameters increased as a function of the speed ($p < 0.05$): aerial time (t_a , mean $+30.1\pm 33.4\%$, Fig. 2.4B), stride frequency (SF, mean $+2.6\pm 0.1\%$ Fig. 2.4C), stride length (SL, mean $+17.6\pm 4.0\%$, Fig. 2.4D), maximal ground reaction force (F_{max} , mean $+7.1\pm 5.1\%$, Fig. 2.5), leg length changes (ΔL , mean $+12.9\pm 1.6\%$, Fig. 2.6A) and vertical stiffness (k_{vert} , mean $+7.2\pm 1.0\%$, Fig. 2.6B). While leg stiffness (k_{leg}) decreased as a function of the speed by mean $-4.6\pm 5.1\%$ (Fig. 2.6C). At POST, similar changes in the above-mentioned parameters, as a function of speed, were observed in the EG.

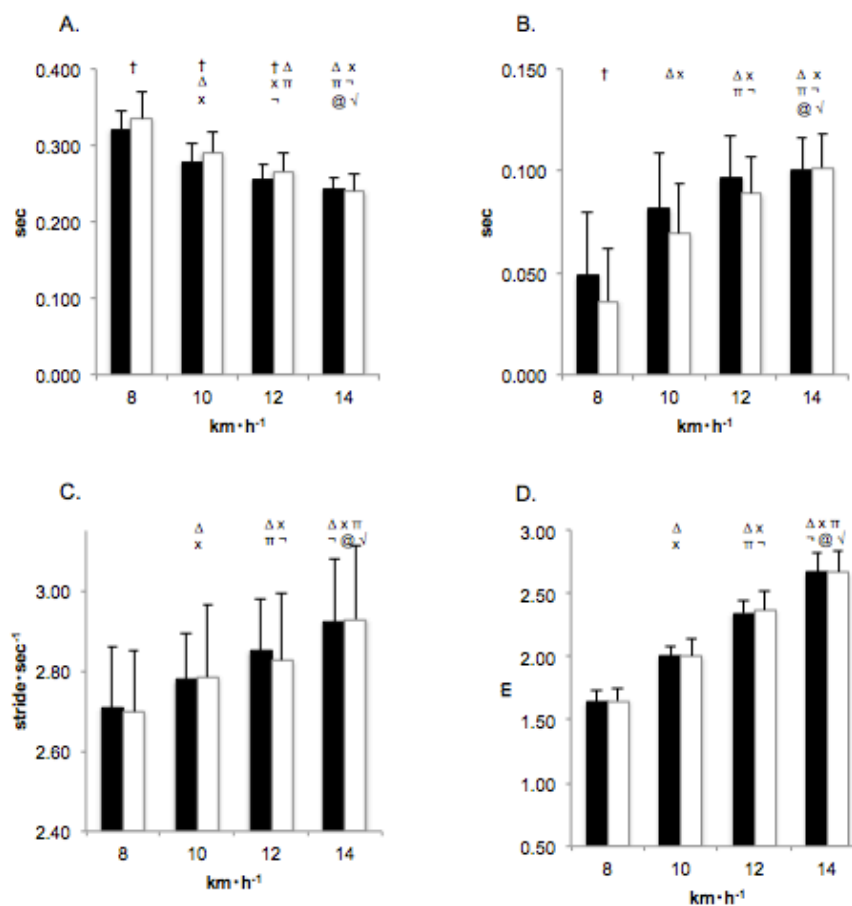


Fig 2.4. t_c (in s, Fig. 2.4A), t_a (in s, Fig. 2.4B), SF (in stride·sec⁻¹, Fig. 2.4C) and SL (in m, Fig. 2.4D) in EG (n=13), before (PRE, black bars) and after (POST, white bars) the training protocol. †: significantly different POST vs. PRE; Δ: significantly different compared with 8 km·h⁻¹ PRE; x: significantly different compared with 8 km·h⁻¹ POST; π: significantly different compared with 10 km·h⁻¹ PRE; ∩: significantly different compared with 10 km·h⁻¹ POST; @: significantly different compared with 12 km·h⁻¹ PRE; √: significantly different compared with 12 km·h⁻¹ POST

After the training protocol, in the EG t_c increased at 8, 10 and 12 $\text{km}\cdot\text{h}^{-1}$ by mean $4.4\pm 0.1\%$ (Fig. 2.4A) ($p<0.05$) and t_a decreased by -25.6% ($p=0.035$) at 8 $\text{km}\cdot\text{h}^{-1}$, while t_a decreased but not significantly at 10 and 12 $\text{km}\cdot\text{h}^{-1}$ (-15.2% , $p=0.093$ and -8.0% , $p=0.117$, respectively) (Fig. 2.4B). Consequently, F_{max} decreased by -3.7% ($p=0.032$) at 8 $\text{km}\cdot\text{h}^{-1}$ and it slightly decreased at 10 and 12 $\text{km}\cdot\text{h}^{-1}$ (-4.4% , $p=0.077$ and -3.3% , $p=0.076$, respectively) (Fig. 2.5). Further, k_{leg} decreased at 10 and 12 $\text{km}\cdot\text{h}^{-1}$ (-9.5% , $p=0.034$ and -10.1% , $p=0.038$, respectively), while the decrease was not significant at 8 $\text{km}\cdot\text{h}^{-1}$ (-7.6% , $p=0.054$) (Fig. 2.6C). No changes in SF, SL (Fig. 2.6C and 2.6D), Δz and k_{vert} (Fig. 2.6C and 2.6D) were detected in the EG after the training protocol.

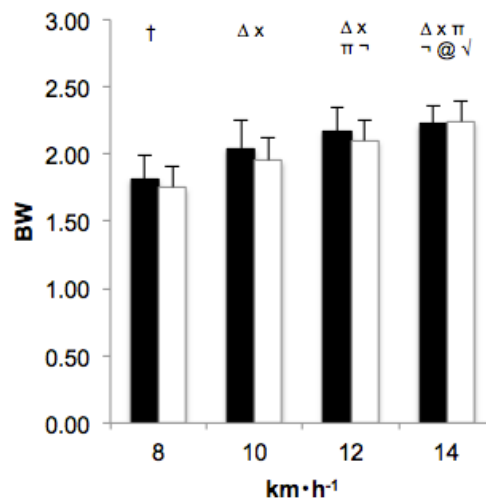


Fig 2.5. F_{max} (in BW) in EG ($n=13$), before (PRE, black bars) and after (POST, white bars) the training protocol. †: significantly different POST vs. PRE; Δ : significantly different compared with 8 $\text{km}\cdot\text{h}^{-1}$ PRE; x: significantly different compared with 8 $\text{km}\cdot\text{h}^{-1}$ POST; π : significantly different compared with 10 $\text{km}\cdot\text{h}^{-1}$ PRE; \cap : significantly different compared with 10 $\text{km}\cdot\text{h}^{-1}$ POST; @: significantly different compared with 12 $\text{km}\cdot\text{h}^{-1}$ PRE; \sqrt : significantly different compared with 12 $\text{km}\cdot\text{h}^{-1}$ POST

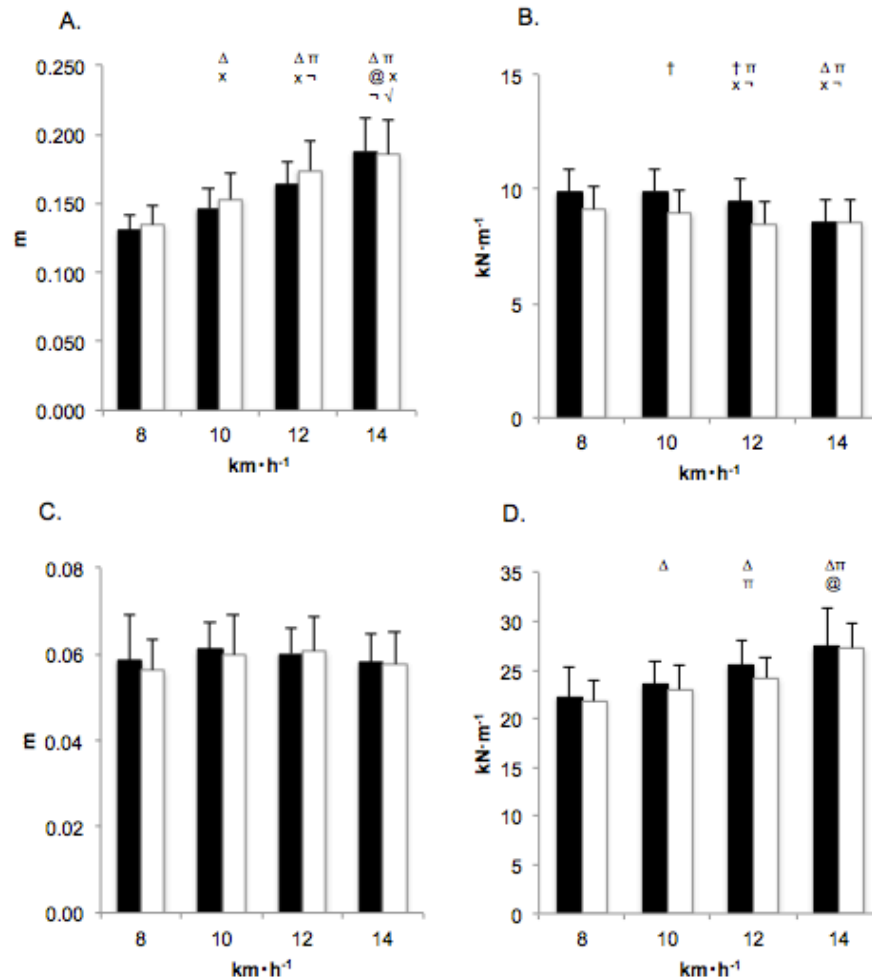


Fig 2.6. ΔL (in m, Fig. 2.6a), k_{leg} (in m, Fig. 2.6b), Δz (in m, Fig. 2.6c) and k_{vert} (in $\text{kN}\cdot\text{m}^{-1}$, Fig. 2.6d) in EG ($n=13$), before (PRE, black bars) and after (POST, white bars) the training protocol. †: significantly different POST vs. PRE; Δ : significantly different compared with $8 \text{ km}\cdot\text{h}^{-1}$ PRE; x: significantly different compared with $8 \text{ km}\cdot\text{h}^{-1}$ POST; π : significantly different compared with $10 \text{ km}\cdot\text{h}^{-1}$ PRE; \neg : significantly different compared with $10 \text{ km}\cdot\text{h}^{-1}$ POST; @: significantly different compared with $12 \text{ km}\cdot\text{h}^{-1}$ PRE; $\sqrt{\quad}$: significantly different compared with $12 \text{ km}\cdot\text{h}^{-1}$ POST

Maximal muscle power of the lower limbs

At PRE, MMP was not significantly different between CG and EG in absolute (2961 ± 422 vs. $3257\pm 632 \text{ W}$, $p=0.186$) and relative (42.3 ± 6.72 vs. $43.8\pm 7.4 \text{ W}\cdot\text{kg}^{-1}$, $p=0.585$) values. As well, at POST, MMP increased in the EG, although this increment was not statistically significant ($+5.1\pm 12.2\%$, $p=0.174$, Table 2.3). Then, in EG inverse relationships between changes in Cr and MMP at 10 ($p=0.013$; $r=-0.67$) and $12 \text{ km}\cdot\text{h}^{-1}$ ($p<0.001$; $r=-0.86$) were shown (Fig. 2.7).

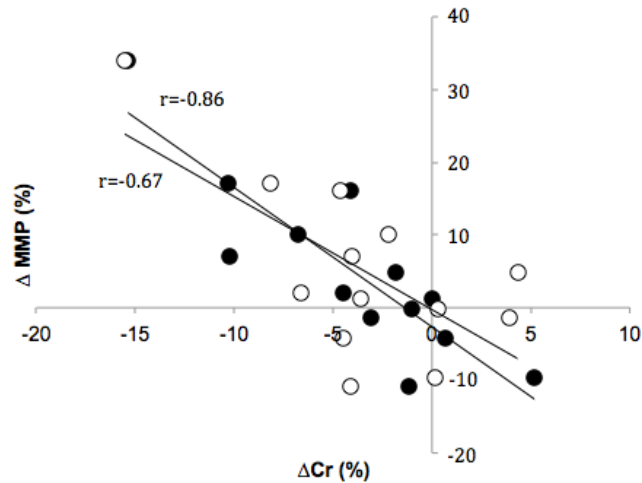


Fig 2.7. Relationships between changes in energy cost of running (ΔCr , %) and maximal muscle power (ΔMMP , %) in the experimental group (EG) at 10 km/h (white dots) and 12 km/h (black dots)

Gastrocnemius medialis and triceps surae tendon proprieties

At PRE and POST, no significant differences were shown in proprieties of GM and triceps surae tendon between CG and EG. Moreover, these proprieties did not change significantly between PRE and POST training protocol both in CG and in EG (Table 2.3).

	Control Group				Exercise Group				p		
	Pre		Post		Pre		Post		Group	Time	G x T
MMP	42.3 ± 6.7	42.1 ± 4.9	43.8 ± 7.4	45.6 ± 6.7	0.317	0.311	0.23				
Triceps surae tendon											
Resting length (L_0 , mm)	202.8 ± 12.8		217.1 ± 24.1		0.123						
Elongation (ΔL , mm)	22.5 ± 3.6	22.1 ± 4.4	21.5 ± 3.4	21.5 ± 3	0.569	0.738	0.789				
Strain ($\Delta L \cdot L_0^{-1}$, %)	11.1 ± 1.6	10.9 ± 2.4	9.9 ± 1.1	9.9 ± 1.4	0.094	0.884	0.77				
Cross-sectional area (mm^2)	59 ± 15.9	57 ± 15.4	69.1 ± 13.2	67.7 ± 16	0.118	0.178	0.803				
Force (N)	4865.6 ± 1617.71	4754.2 ± 1846.6	5621.2 ± 497.9	5436.4 ± 954.6	0.191	0.414	0.839				
Stiffness ($N \cdot mm^{-1}$)	420.2 ± 202	370.4 ± 169.9	442.9 ± 88.6	409.4 ± 61.3	0.59	0.086	0.668				
Young's modulus (Gpa)	1.42 ± 0.38	1.31 ± 0.44	1.4 ± 0.32	1.33 ± 0.29	0.984	0.189	0.737				
Gastrocnemius medialis											
Fiber length (mm)	48.9 ± 9.3	49.1 ± 9.3	48.8 ± 9.2	49.9 ± 9.8	0.936	0.22	0.362				
Pennation angle (deg)	21.2 ± 2.4	20.9 ± 2.6	20.7 ± 1.8	20 ± 2	0.448	0.052	0.497				
Thickness (mm)	17.5 ± 2.5	17.2 ± 2.3	17.1 ± 3.1	16.9 ± 3	0.786	0.16	0.876				
Torque ($N \cdot m^{-1}$)	251 ± 62.9	245 ± 73.7	268.8 ± 40.7	267.3 ± 66.9	0.437	0.699	0.819				

Table 2.3. Physiological characteristics of the triceps surae tendon and gastrocnemius medialis muscle of athletes, before (PRE) and after (POST) the training period in the control group (n=12) and in the exercise group (n=13). All values are means \pm s.d. MMP: maximal muscle power of the lower limbs. p: Significance by GLM repeated measures with two factors of the main effects of Group (CG vs EG), time (PRE vs POST) and their interaction (G x T).

Discussion

The main findings of the present study showed that in high-level ultra-marathoners a 12-week SEP training protocol led to a lower Cr at submaximal speeds and MMP might have an important role in decreasing Cr.

Conversely to previous works in which recreational runners were involved (Ferrauti et al. 2010; Hakkinen et al. 2003; Turner et al. 2003), we enrolled high-level, non-professional ultra-marathoners. As we hypothesized, SEP training led to a lower Cr ($-4.3 \pm 1.5\%$), considering the four selected running speeds altogether. We tested four different running speeds (8, 10, 12, 14 $\text{km} \cdot \text{h}^{-1}$) because we aimed to test the range of speeds the athletes likely select during ultra-marathons (on average they ran a 100 km race in $9:00 \pm 1:56$ hours, which means $\sim 11 \text{ km} \cdot \text{h}^{-1}$) or during most of their running training. The improvement in Cr ($\sim 4\%$) might seem a small progress; however, for these athletes a small performance enhancement can lead to an important step forward in the final rankings. According to the equation of di Prampero et al. (1986), where the speed of running is determined by the ratio between metabolic power and Cr, and assuming that athletes run a 100 km race at 70% of their $\dot{V}\text{O}_2\text{max}$ (Davies and Thompson 1979; Davies and Thompson 1986), decreasing Cr by -4% would improve their performance by ~ 17 minutes (from 7h05' min to 6h48' min). Although this computation does not take into account possible changes in Cr due to the distance covered (Lazzer et al. 2015; Lazzer et al. 2014), it highlights the relevance of Cr in ultra-endurance competitions.

Previous works (di Prampero et al. 1986; Margaria et al. 1963) described that Cr is independent from the speed between 8 and 20 $\text{km} \cdot \text{h}^{-1}$. However, at 8 $\text{km} \cdot \text{h}^{-1}$ we reported higher Cr compared to other speeds ($+6.5 \pm 2.0\%$). We suppose that this could be due to the fact that our athletes never run slower than $\sim 10 \text{ km} \cdot \text{h}^{-1}$, thus they are not adapted to this slow speed. They can carry out a 100 km running race in less than 10 hours and some of them were able to run more than 240 km in 24 hours running race. Farley et al. (1991) predicted that metabolic rate increases at lower frequency during hopping because the body does not behave in an optimal spring-like manner and some elastic energy is dissipated. If we compare running to a series of subsequent hops, this may explain the higher Cr at 8 $\text{km} \cdot \text{h}^{-1}$ compared with other "optimal speeds" (Stuedel-Numbers and Wall-Scheffler 2009). Also, at such slow speed the relaxation phase is shorter and the constriction during the contraction phase is prolonged, promoting a

worse blood flow, thus the access of O₂ and substrates to working muscles (Hoff et al. 1999; Storen et al. 2008; Sunde et al. 2010). Further, F_{max} and ΔL increased as a function of the speed but, conversely to previous work (Arellano and Kram 2014), Δz did not change. Consequently, k_{leg} decreased as a function of the speed while k_{vert} increased. We speculate that since they are high-level ultra-marathoners they may be adapted to a different running pattern compared with short and middle distance runners. Nevertheless, new studies comparing these athletes are required in order to define possible differences in running technique.

In the present study SL and SF did not change after the training protocol, as previously shown by Ferrauti et al. (2010). These authors considered recreational marathon runners who underwent to 8-week intervention that consisted in two strength-training sessions per week. However, they showed increased t_c at 8.6 and 10.1 km·h⁻¹ by ~3%. Our results agree with this work (Ferrauti et al. 2010), since t_c increased by mean +4.4±0.1% at 8, 10 and 12 km·h⁻¹ at POST. According to the cost of generating force hypothesis (Kram 2000; Kram and Taylor 1990), running with a longer t_c should be more economical, since it requires slower and less expensive fibers and the force is applied in a longer period of time (Kram and Taylor 1990; Roberts et al. 1998). In agreement with this hypothesis the increased t_c could in part explain the lower Cr.

We reject our second hypothesis although MMP during the squat jump slightly increased (+5.1±12.1%, p=0.174) after the SEP training protocol. Anyway, this increase was not significant as opposed to previous studies' results (Hakkinen et al. 2003; Hoff et al. 2002; Millet et al. 2002). We suppose that for these athletes the training protocol was too light and probably they need to train with maximal loads to improve the MMP. Since ultra-endurance athletes are rarely professionals (no one among our subjects), we proposed a training protocol that athletes could easily perform at home three times per week without renouncing to their usual running training.

However, an inverse relationship between changes in MMP and changes in Cr at 10 and 12 km·h⁻¹ (Fig. 2.5) suggests that athletes who slightly improved their MMP also decreased their Cr at submaximal speeds suggesting that MMP is an important parameter in determining Cr, as previously shown (Lazzer et al. 2015; Lazzer et al. 2014). Moreover, our group has reported that lower Cr values were related to higher MMP (Lazzer et al. 2014) and athletes with greater MMP had lower changes (i.e.

increase) in Cr during an uphill marathon (Lazzer et al. 2015). As well, in the same race MMP was inversely related with race time (Giovanelli et al. 2015b), emphasizing the importance of high MMP values in ultra-endurance events.

A number of adaptive mechanisms may be involved in the decrease of the Cr after a concurrent strength training protocol (Aagaard et al. 2011; Millet et al. 2002; Spurrs et al. 2003). We analyzed some aspects of the mechanics of running and the properties of the GM and triceps surae tendon, which did not change at POST. We reject our third hypothesis even if previous studies supported the idea that power training leads to a higher MTS (Millet et al. 2002; Spurrs et al. 2003) that affects positively the Cr (Arampatzis et al. 2006). Probably, high-level athletes need longer and/or heavier training protocol to stimulate tissue changes, whereas in a group of both physically active and untrained subjects 4 weeks of training were enough to increase the synthesis of collagen type I in triceps surae tendon (Langberg et al. 2001).

Conclusion

In conclusion, 12-week SEP training program led to a Cr improvement in high-level ultra-marathoners at different submaximal speeds. Increased t_c and an inverse relationship between changes in Cr and changes in MMP can partially explain the decreased Cr. Even if the mechanisms that led to a lower Cr are not clarified in high-level ultra-marathoners, we suggest to add at least three sessions per week of SEP exercises in the normal endurance training program.

Critique of methods

We acknowledge that our study has some limitations. First, athletes enrolled in this study were well trained and the training protocol they underwent was probably too light to induce significant improvements. We preferred to propose a training protocol that could be easily performed at home by not professional athletes and they could integrate this specific training in their habitual activities.

Second, since many of them had never performed strength or explosive training before, we decided to use the first four weeks of training as “adaptation” period. We assumed that this cycle was important to avoid discomfort or lower the injury risk. Indeed, it has been reported that core training improves endurance performance, likely by reducing Cr (Tong et al. 2014). Moreover, the muscles of the core have a critical role for the transfer

of energy from the larger torso to the terminal segments, which may be more involved in the ability to control the position and motion of the trunk over the pelvis during running and allows a better force transfer to the extremities (Kibler et al. 2006). Further, some specific exercises (i.e. high knees, butt kicks...) could affect the running posture, which would lower Cr by moving the ground reaction force application point (Biewener et al. 2004; Lacour and Bourdin 2015). As well, exercises performed on a balance board may reduce the chances for lower back and extremity injuries and would allow exerting greater forces when there is an unstable situation (Behm and Colado 2012; Verhagen et al. 2005), which is common in trail running.

Conclusions of Part I

Our studies confirm that the maximal oxygen uptake, the fraction of it maintained throughout the race and the cost of transport are the main physiological parameters affecting the ultra-endurance performance, both on level and uphill (Lazzer et al. 2015; Lazzer et al. 2014).

Also, during a 6h-running race on a *flat* loop, athletes tend to change their running pattern after a certain time (~4 hours) rather than after a certain distance covered. This confirms previous results in which our group reported similar mechanical behavior during an *uphill* only marathon of similar duration (Giovanelli et al. 2015b). Moreover, when the slope becomes very steep athletes can reduce their energy expenditure by walking rather than running (Giovanelli et al. 2015a).

These results suggest that athletes may improve their performance by adding specific trainings to their training plan and trying to maintain a regular mechanical running pattern during the race. Also, to improve the performance on steep terrain they should add the walking gait during their training.

Further, we found a relationship between MMP and performance. Indeed, higher MMP was related to lower Cr and lower deterioration of the running pattern. Thus, our results suggest that an improvement in the MMP would lead to a more economic running pattern and a better performance.

In conclusion, by adding strength, explosive and power training to the usual endurance training it is possible to improve the cost of running (i.e. lower) without affecting other parameters. Many endurance athletes and coaches often underestimate the SEP training. We suggest to include at least three sessions per week of SEP training in the training program in order to optimize the performance through a lower Cr.

PART II

DEVELOPMENT OF INSOLE SHOE SENSOR FOR GAIT ANALYSIS: A PILOT STUDY

Introduction

Ground reaction forces are often investigated in gait biomechanics studies (Blickhan 1989; Cavanagh and LaFortune 1980; Girard et al. 2013; Gottschall and Kram 2005; Lieberman et al. 2015). The measurements are often limited by the positioning of force plates, which makes difficult to obtain data outdoor, in the field. Different devices have been developed to measure vertical and horizontal ground reaction forces in healthy subjects and patients with different pathologies. Davis et al. (1998) used a thin layer of strain gauge transducer whereas Razian and Pepper (2003) adopted piezoelectric copolymer film. Liedtke et al. (2007) used an instrumented shoe with two sensors mounted beneath the forefoot and rearfoot. However, these devices were limited to its specific purpose and thus were not readily available for other researchers. Further, they increased the height of the effective sole and also the weight of the sole altering the correct gait (Veltink et al. 2005).

Thus, the second part of my thesis is focused on designing, developing and validating a mechatronic device for gait data collection. Our objectives were to develop and validate an insole-shoe sensor to collect the vertical and horizontal GRF and the contact and aerial times. The device should be flexible, comfortable and low cost.

Shoe sensor equipment

The sensor equipment was composed by:

- A plastic or rubber insole
- Five piezoresistive force sensors (FSR, Tekscan Flexiforce A401)
- A s-beam load cell (Futek LSB200)
- A NI myRIO-1900 acquisition device
- A battery case

Insole

The very first prototype of our insole was a leather insole on which we fixed the FSRs (Fig. 3.1). With this model it was possible to collect data about the vertical GRF and the contact time, while we could not fix the load cell for the horizontal GRF because of the thin of the insole. The results of the first prototype are presented in the manuscript “A mechatronic system mounted on insole for analyzing human gait” by Giovanelli D et al.

presented at the International Conference on Robotics and Mechatronics in Iran (2014, see below).

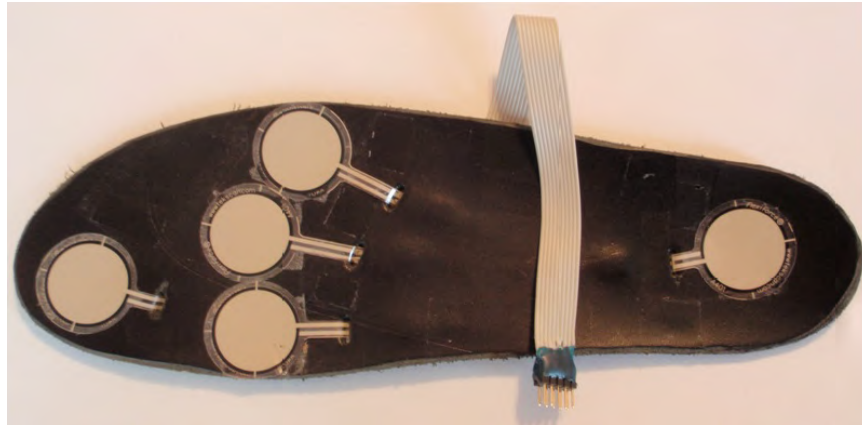


Fig. 3.1 - The leather insole with the 5 PFSs and the cable for the data acquisition

Then, in order to fit the load cell (which has a height of 6.7 mm) we re-designed the prototype using CAD 3D (Fig. 3.2).

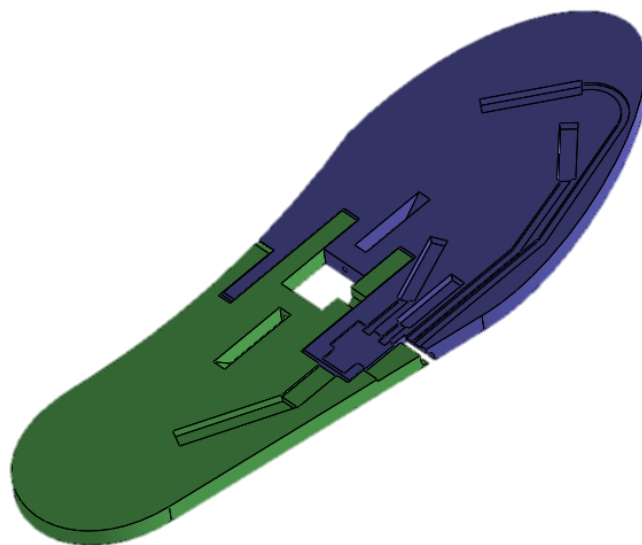
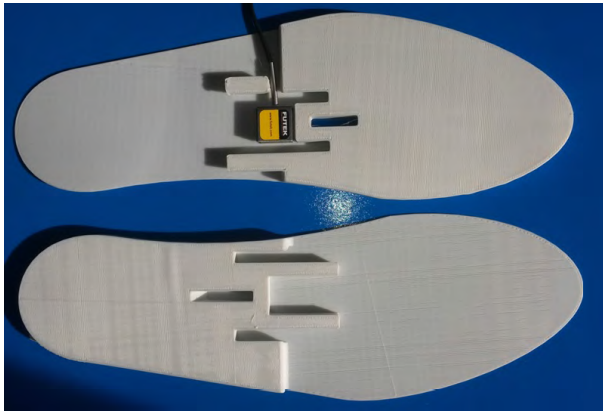


Fig. 3.2 - The 3D model designed with CAD 3D.

This model was composed by two plastic semi-insole (e.g. anterior and posterior, Fig. 3.3 A and B), printed with a 3D printer, which allowed us to fix the load cell in the middle (Fig. 3A).

A.



B.



Fig. 3.3 - The two plastic semi-sole with the load cell divided (A) and united (B)

The plastic used in this model was not enough resistant and we had to choose a new material. The new prototype was made by thermoplastic polyurethane (TPU) 70 shore. The two semi-insoles were glued to a carbon sheet (thickness 0.2 mm) to assure a good rigidity. In order to guarantee a good slip we fixed a kapton polyimide film on the surface (Fig 3.4).



Fig 3.4 - The two TPU semi-sole with the kapton polyimide film

Resistive force sensors

In order to minimize the height of the insole we adopted piezoresistive force sensors (Tekscan Flexiforce A401, Fig. 3.5A). These sensors have a sensing area of 506 mm^2 (25.4 mm diameter) and they have a 2-pin connector. We used the sensors with a single voltage source circuit as recommended by the manufacturer (Fig. 3.5B).

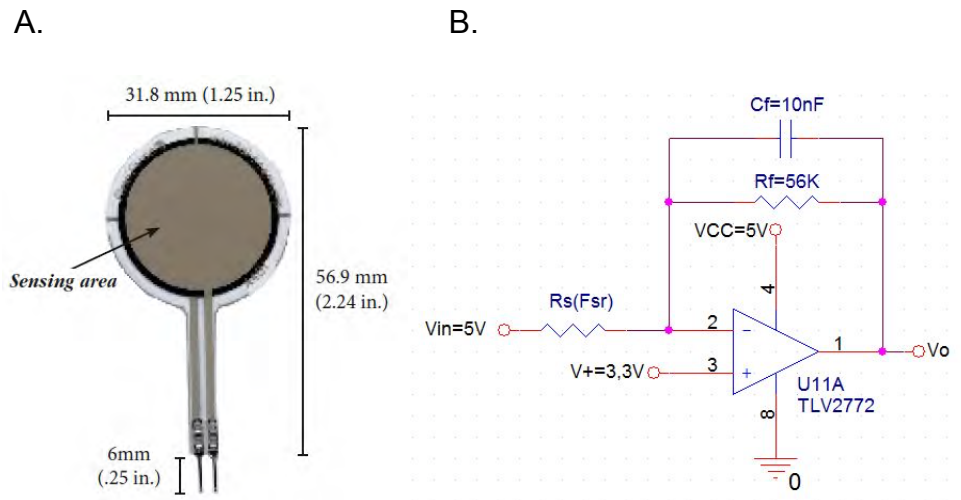


Fig. 3.5 - The piezoresistive force sensor (A) and the circuit adapted for the acquisition (B).

Sensors positioning

Different configurations in positioning the sensors have been attempted by different authors (Bamberg et al. 2008; Edgar 2010; Healy et al. 2012; Howell et al. 2013; Salpavaara 2009; Sazonov et al. 2011; Yan 2010). We adopted the one proposed by Sazonov et al. (2011) with a total of five sensors positioned in coincidence of the first toe, the first, the third and the fifth metatarsus and under the heel (Fig. 3.6).



Fig. 3.6 - The sensors position as suggested by Sazanov et al. (2011)

Conversely to other prototypes (Edgar 2010) we preferred to use bigger sensors because after some trials we noted that with the smallest ones we had more noise in the signal processing.

Load cell

In order to measure the horizontal GRF we applied a load cell (JR S-Beam, Futek, LSB200) in the middle of the insole. The load cell was fixed with two screw in the place prepared in the insole. The connection wire was positioned in the right side of the prototype (Fig. 3.7 and 3.8).

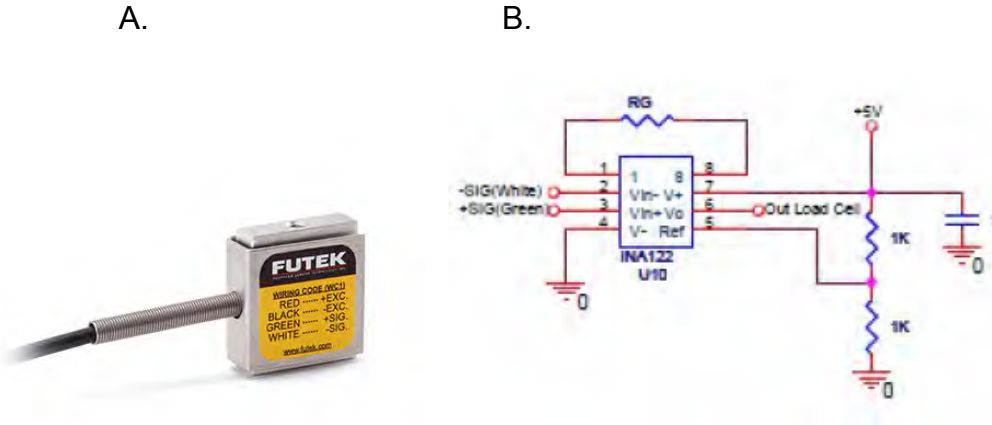


Fig 3.7 - The load cell we used for the acquisition of the horizontal GRF (A) and the amplification circuit adapted for the acquisition (B).



Fig. 3.8 – The whole insole with the five FSRs and the load cell.

Acquisition device and battery case

The data recorded by the load cells and the FSRs were logged into a specific portable acquisition device (NI myRIO-1900, Fig. 3.10), which provides for signal conditioning and data logging. The acquisition device was placed in a belt and was powered by a 4v battery positioned in a battery case. Data were acquired in a flash drive and then copied into a PC and analyzed with a Matlab customized program.

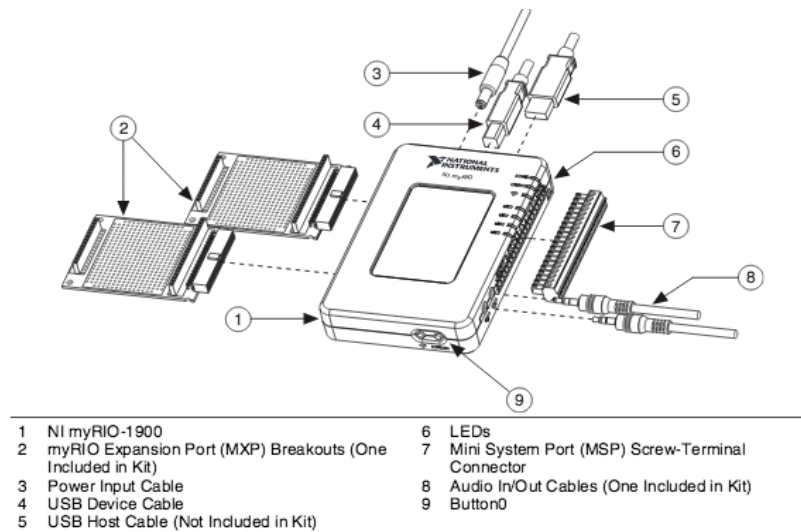


Fig.3.10 - the NI myRIO-1900

Validation procedures

Participants

Three healthy individuals (27.6 ± 2.5 yr; 69.3 ± 3.5 kg) took part in the study. None of the participants had any history of physical or neurological conditions that might interfere with their respective gait. Written informed consent was obtained from all participants and the experimental protocol was approved by the ethical committee of the University of Udine.

Insole

The TPC insole weighs 175 g. The width was 90 mm and the length was 270 mm (Fig. 3.11). Although the thickness was 6.8 mm it fits good in a shoe half number bigger than usual subjects' shoes.

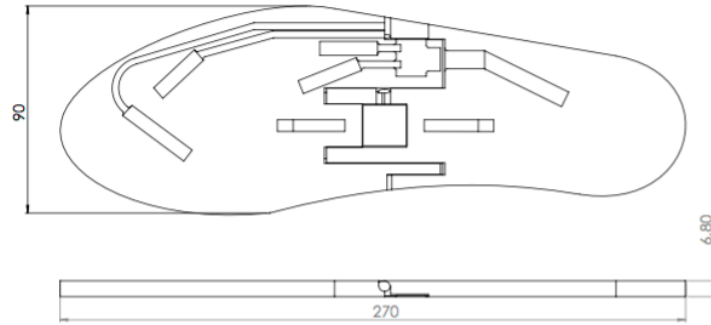


Fig. 3.11 – Details of the insole

Calibration of the sensors

Before every trial the sensors were calibrated using known weights. The calibration of the FSRs was performed after the sensors were fixed on the insole as suggested by the manufacturer. We used eleven different weights (see Table 3.1 and Fig. 3.12) and we averaged the values (in volt, V) obtained from three attempts with a customized LabView program.

Weight (kg)	Newton (N)	FSR output tension [V]			Averaged value [V]
0	0	3.28	3.22	3.26	3.25
0.1	1.4	3.27	3.21	3.25	3.24
1.2	11.4	3.12	3.00	3.09	3.07
2.2	21.2	2.93	2.87	2.91	2.90
3.2	31.2	2.83	2.81	2.83	2.82
4.2	41.4	2.8	2.81	2.76	2.79
5.4	52.7	2.56	2.55	2.56	2.56
6.2	60.9	2.36	2.34	2.39	2.36
7.4	72.4	2.15	2.12	2.16	2.14
8.2	80.8	2.07	2.1	2.04	2.07
10.7	105.4	1.49	1.53	1.56	1.53
12.8	125.2	1.27	1.22	1.25	1.25

Table 3.1 – Calibration of the FSR sensors

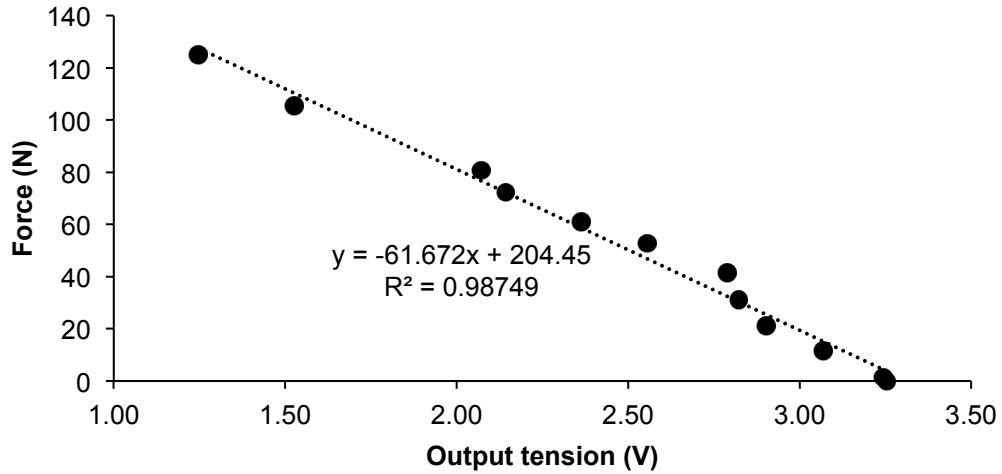


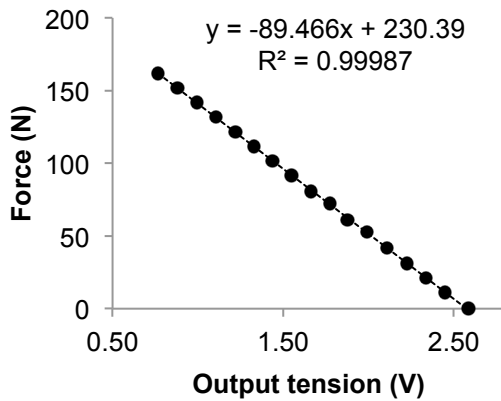
Fig 3.12 – Calibration curve of the FSR sensors

The calibration of the load cell was performed in compression and in traction. We used 16 different weights (Table 3.2 and Fig. 3.13 A and B) and the output tension (in volt, V) was recorded using a customized LabView program.

Weight (kg)	Newton (N)	Output tension	
		Compression (V)	Traction (V)
0.0	0.0	2.59	2.59
1.2	11.4	2.45	2.75
2.2	21.2	2.34	2.85
3.2	31.2	2.22	2.96
4.2	41.4	2.11	3.07
5.4	52.7	1.99	3.20
6.2	61.0	1.88	3.29
7.4	72.4	1.77	3.40
8.2	80.8	1.66	3.52
9.3	91.6	1.55	3.64
10.4	101.7	1.44	3.77
11.4	111.7	1.33	3.87
12.4	121.7	1.22	3.99
13.4	131.8	1.11	4.10
14.5	141.8	0.99	4.22
15.5	151.8	0.88	4.34
16.5	161.8	0.77	4.45

Table 3.2 – Calibration of the load cell

A.



B.

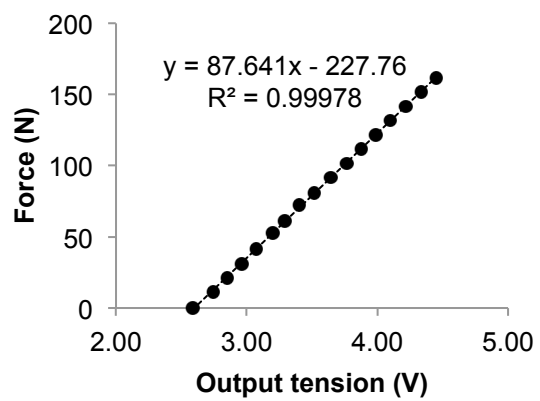


Fig. 3.13 – Calibration curve of the load cell in compression (A) and in traction (B)

Experimental protocol

Every participant performed three runs along a 30 m-runway in which a force plate was positioned. They were instructed to run at three different speeds (10, 12 and 14 km·h⁻¹, respectively). Practice trials were permitted to allow subjects to become familiar with the running speeds. A successful trial was defined when the foot in which the sensorized insole was placed (the right) fell within borders of the force plate from initial contact to toe-off, and the running speed was within $\pm 5\%$ of the target speed (Teng and Powers 2015). At every condition 10 steps per subject were analyzed and a total of 30 steps for each speed was used for the validation. Data were continuously registered at 1000 Hz in a flash drive and then analyzed with a customized Matlab program. The data obtained were compared with those collected by a force plate (Kistler, 9281 E) positioned in the track field.

Statistical analysis

Mean and standard deviation were calculated independently for every gait parameter measured at each speed. Bland-Altman test was performed in order to validate the obtained Fmax and t_c , $p < 0.05$ was defined as statistically significant.

Results

Contact times recorded with the RFSs were higher than t_c collected with the force plate (+2.47%, $p=0.001$; Fig. 3.14 A and B). Further, contact time decreased by increasing the speed by mean -9.02% ($p<0.05$) when compared with $10 \text{ km}\cdot\text{h}^{-1}$.

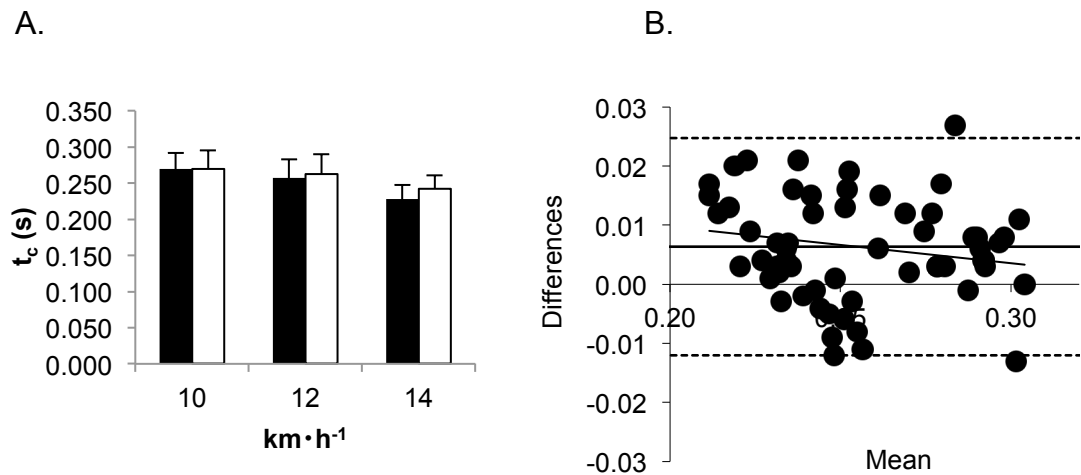


Fig. 3.14 – A. Contact time (t_c , in s) measured with the force plate (black bars) and with the insole sensor (white bars) at 10, 12 and $14 \text{ km}\cdot\text{h}^{-1}$. B, the Bland-Altman plot for the contact time.

No differences in F_{max} were detected at the three speeds analyzed between the force plate and the insole sensors ($p>0.05$, Fig. 3.15 A and B). Further, F_{max} increased by increasing the speed by mean +4.61% ($p<0.05$) when compared with $10 \text{ km}\cdot\text{h}^{-1}$.

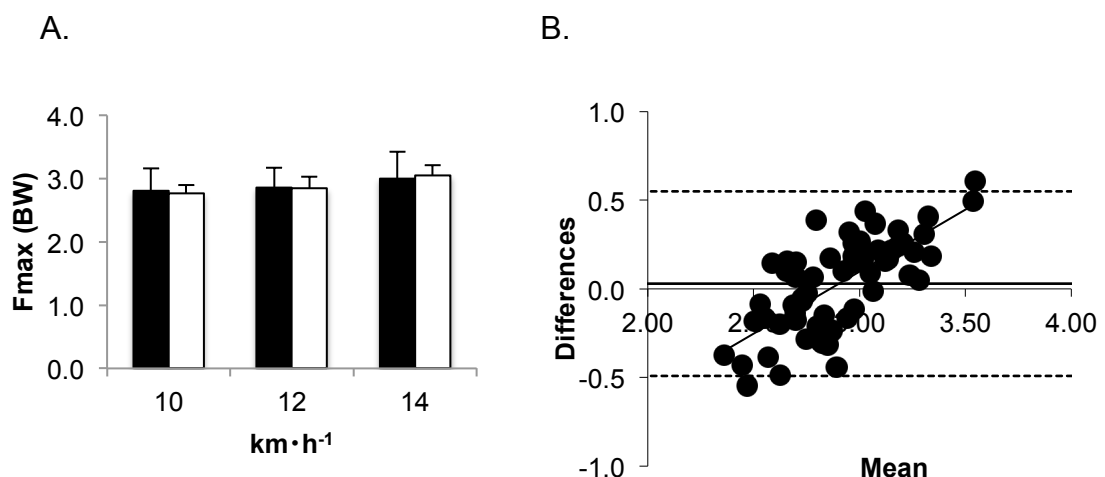


Fig. 3.15 – A. Maximal vertical ground reaction force (F_{max} , in BW) measured with the force plate (black bars) and with the insole sensor (white bars) at 10, 12 and $14 \text{ km}\cdot\text{h}^{-1}$. B, the Bland-Altman plot for the F_{max} .

Discussion

The aim of the present study was to develop and validate an insole shoe sensor for detecting vertical and horizontal ground reaction forces and contact times. Our prototype allows the measurements of the F_{max} and t_c with a small error compared with the gold standard. Although the difference between the t_c measured with the sensors is statistically significant, the error is ~2% which is acceptable when the running gait is analyzed (Giovanelli et al. 2015b; Lazzer et al. 2015; Morin et al. 2011b).

With this device we can obtain the F_{max} and t_c and we can compute other parameters by using the formula proposed by Morin et al. (2005). With this method we can calculate the vertical displacement of the centre of mass and the vertical stiffness, which are parameters commonly used in the gait analysis.

We developed our prototype by trying different solutions in materials and sensors positioning. At the end we obtained a comfortable tool which could be worn by the subjects with no trouble during running.

Limitations

This study has several limitations, one being the low number of participants. However, this was a pilot study to clarify if it was possible to develop a sensor for measuring some mechanical parameters.

However, during our experiments we attempted to collect the horizontal GRF with a small load cell. After few trials we identified some issues with the load cell. Although we tried to use some slippery materials in order to obtain two semi-insole which were able to slip on each other, this was not enough and the load cell experienced some problems in recording the data. After trying different solutions we decided to renounce in collecting the horizontal GRF.

Conclusion

We developed a device which can be used in detecting the vertical GRF and contact time during overground running without using force platforms. This prototype is comfortable and can be worn by athletes during running.

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1 **FACTORS AFFECTING METABOLIC COST OF TRANSPORT**
2 **DURING A MULTI-STAGE RUNNING RACE**

3
4
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1 **ABSTRACT**

2 **Purpose:** to investigate: 1) the role of $\dot{V}O_{2max}$, fraction of it (F) and metabolic cost of
3 transport (CoT) in determining performance during an ultra-endurance competition and 2) the
4 effects of the race on several biomechanical and morphological parameters of the lower limbs
5 that are likely to affect CoT. **Methods:** Eleven runners (age: 29-54 years) participated in an
6 ultra-endurance competition consisting of three running stages of 25, 55 and 13 km on three
7 consecutive days. Anthropometric characteristics, body composition, morphological
8 properties of the gastrocnemius medialis, maximal explosive power of the lower limb and \dot{V}
9 O_{2max} were determined before the competition. In addition, biomechanics of running and CoT
10 was determined, before and immediately after each running stage. **Results:** Performance was
11 directly proportional to $\dot{V}O_{2max}$ ($r=0.77$), and F ($r=0.36$) and inversely proportional to CoT
12 ($r=-0.30$). Low CoT values were significantly related to high maximal power of the lower
13 limbs ($r=-0.74$), vertical stiffness ($r=-0.65$); and low foot-print index (FPI, $r=0.70$), step
14 frequency ($r=0.62$) and external work ($r=0.60$). About 50% of the increase in CoT during the
15 stages of the competition was accounted for by changes in FPI, which represents a global
16 evaluation of medio-lateral displacement of the foot during the whole stance phase, which in
17 turn are associated with the myotendinous characteristics of the lower limb. **Conclusions:**
18 lower CoT values were related to greater muscular power and lower FPI, suggesting that a
19 better ankle stability is likely to achieve better performance in ultra endurance running
20 competition.

21

22 **Key Words:** maximal oxygen uptake; ultra-marathon; kinematics; stiffness; energy cost of
23 running

24

1 INTRODUCTION

2 Middle- and long-distance running performances depend on several physical, physiological,
3 biomechanical, metabolic, psychological and social factors (di Prampero, 2003; di Prampero
4 et al., 1986). In particular, the three most important physiological factors determining high
5 level performances are: 1) a large value of maximal oxygen uptake ($\dot{V}O_{2max}$, $mlO_2 \cdot kg^{-1} \cdot$
6 min^{-1}), 2) a large fraction (F , %) of $\dot{V}O_{2max}$ that can be sustained throughout the competition
7 and 3) a small value of metabolic cost of transport (CoT, $mlO_2 \cdot kg^{-1} \cdot m^{-1}$). As shown by di
8 Prampero et al., 1986, the endurance speed (v_{end} , $m \cdot min^{-1}$) in long distance running can be
9 predicted, for any given runner, provided that his values of CoT, $\dot{V}O_{2max}$, and F are known:

10

$$11 \quad v_{end} = F \cdot \dot{V}O_{2max} \cdot CoT^{-1} \quad (1)$$

12

13 Indeed, strong correlations were found between $\dot{V}O_{2max}$ and running performance in
14 heterogeneous-level runners (Billat et al., 2003; Maughan and Leiper, 1983). Additionally,
15 several studies showed that, in elite distance runners, F , which is linked primarily to
16 adaptations resulting from prolonged training (Holloszy and Coyle, 1984), is a crucial
17 parameter to determine performance (Maughan and Leiper, 1983). Finally, at the metabolic
18 intensity imposed by the product $F \cdot \dot{V}O_{2max}$, the running velocity is determined by the
19 individual's ability to translate energy into performance (Daniels, 1985), i.e. to the energy
20 expenditure per unit of mass and distance (CoT).

21 CoT is generally expressed as the amount of energy spent above resting to transport 1 kg body
22 mass (BM) over 1 meter distance. CoT is independent of speed, at least for speeds ranging
23 from $2.2 \text{ m} \cdot \text{s}^{-1}$ ($8 \text{ km} \cdot \text{h}^{-1}$) to about $5 \text{ m} \cdot \text{s}^{-1}$ ($18 \text{ km} \cdot \text{h}^{-1}$) wherein the air resistance is
24 negligible (Jones and Doust, 1996). When normalized per unit of BM, CoT above resting, on
25 flat compact terrain, shows a variability among subjects of 10-20%; its average value reported
26 by di Prampero et al., 1986 amounts to $0.182 \pm 0.014 \text{ mlO}_2 \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$. CoT in trained runners
27 depends on several physiological and biomechanical factors, including metabolic adaptations,
28 the ability of the muscle-tendon complex to store and release elastic energy, and more
29 efficient mechanics leading to less energy wasted for accelerating-decelerating and lifting-
30 lowering the body at each stride (Lichtwark and Wilson, 2007; Saunders et al., 2004).

31 Previous study showed the relevant role of CoT in determining performance in middle and
32 long distance running (di Prampero, 2003). It was also proposed that an increase of CoT

1 throughout the event could explain the worse performance observed in some runners
2 compared with others with similar $\dot{V}O_{2max}$ and F (Lazzer et al., 2012; Scrimgeour et al.,
3 1986). Indeed, Brueckner et al., 1991 , reported an increased CoT throughout a marathon,
4 although to a relatively minor extent (0.142% per km of distance), leading to an average
5 increment of CoT at the end of the marathon of ~5%. However, these authors observed that
6 the increase of CoT was widely different among runners with similar characteristics in terms
7 of $\dot{V}O_{2max}$, F , training level, age, etc., being essentially negligible at one extreme of the
8 sample, and twice the average for some other athletes. Davies and Thompson, 1986 ,
9 observed a linear increase of $\dot{V}O_2$ with time from the 50th to 240th minutes during a 4-hours
10 race on a treadmill at constant speed, the rise becoming significant ($p < 0.01$) after 110 min of
11 exercise. In addition, Gimenez et al., 2013, and Millet et al., 2011 , observed that the ability
12 to maintain a high F over a 24 hours running on treadmill is mainly related to a low CoT, and
13 Morin et al., 2011 , in the same study participants, observed significant changes in running
14 biomechanics such as higher oscillation frequency, lower vertical stiffness and lower ground
15 reaction force.

16 Indeed, interventions to reduce CoT are constantly sought after by athletes, coaches and sport
17 scientists. Strength (Storen et al., 2008) and plyometric (Spurrs et al., 2003) training allow
18 muscles and tendons to utilize more elastic energy and to reduce the amount of energy wasted
19 in braking forces. In addition, the most economical runners display a higher triceps-surae
20 tendon stiffness (k_{tendon}) compared to less economical ones (Arampatzis et al., 2006), thus
21 suggesting that the functionality of the muscle tendon unit at submaximal running speeds is
22 not only dependent on the stiffness of the series elastic elements but also on the maximal
23 strength of the contractile element (Hof et al., 2002).

24 The primary purpose of the present study was to investigate the role of $\dot{V}O_{2max}$, F and CoT in
25 determining the performance of runners who participated in a 93 km trail over three
26 consecutive days, named “Magraid”. The second aim was to evaluate the relationship between
27 CoT, k_{tendon} and the morphological properties of the gastrocnemius medialis (GM). The third
28 aim was to investigate the effects of the race fatigue on several biomechanical parameters that
29 are likely to affect CoT.

30

1 RESULTS

2 Characteristics of subjects

3 The anthropometric characteristics of the 11 subjects who completed the race are reported in
4 Table 1. Their average $\dot{V}O_{2\max}$ and maximal explosive power of the lower limb were
5 $55.2 \pm 6.7 \text{ ml} \cdot \text{min}^{-1} \cdot \text{kgBM}^{-1}$ and $1759 \pm 202 \text{ W}$, respectively. The characteristics of triceps surae
6 muscle-tendon complex are reported in Table 2.

8 Factors determining performance

9 The role of the three factors of equation 9 individually evaluated with a simple linear
10 regressions, showed that $\dot{V}O_{2\max}$ ($\text{ml} \cdot \text{min}^{-1} \cdot \text{kg}^{-1}\text{BM}$) had the largest role in determining the
11 mean speed ($r=0.79$) followed by the mean value of CoT throughout the race (CoT_{mean} , $r=-$
12 0.64) and F ($r=0.58$).

13 When the multiple regression between them and $v_{\text{end-mean}}$ (equation 9) was considered, the
14 overall r increased to 0.91 , whereas r values for $\dot{V}O_{2\max}$, F and CoT_{mean} were 0.77 , 0.36 and
15 -0.30 , respectively, the multiple regression being described by:

$$17 \log v_{\text{end-mean}} = 0.708 \cdot \log \dot{V}O_{2\max} + 0.979 \cdot \log F - 1.559 \cdot \log \text{CoT}_{\text{mean}} - 3.067 \quad (2)$$

18 ($R^2 = 0.83$, $\text{SE} = 0.035 \text{ km} \cdot \text{h}^{-1}$)

19
20 One of the main topic of this study was to investigate the role of several biomechanical
21 factors in determining CoT. Therefore the relationships between CoT, measured before the
22 first stage, and the biomechanical variables, showed an inverse relationship between CoT and
23 1) the peak power of the lower limb (P_{\max} , $r = -0.74$, $P < 0.001$) and 2) the vertical stiffness
24 (k_{vert} , $r = -0.65$, $P < 0.05$). In addition, direct relationships between CoT and food print index
25 (FPI, $r = 0.70$, $P < 0.05$), step frequency (f , $r = 0.62$, $P < 0.05$) and external work per unit distance
26 (W_{ext} , $r = 0.60$, $P < 0.05$) were found.

27 In view of these data, a multiple linear regression among these 5 biomechanical parameters
28 and CoT was performed. Only 3 retained a significant role in affecting CoT: 1) the P_{\max} ($r =$
29 -0.74 , $P < 0.001$) followed by 2) W_{ext} ($r = 0.42$, $P < 0.05$) and 3) f ($r = 0.38$, $P < 0.05$). The
30 resulting overall relationship was described by the equation that follows:

$$32 \text{CoT} = -0.000004 \cdot P_{\max} + 0.195193 \cdot W_{\text{ext}} + 0.022361 \cdot f + 0.115432 \quad (3)$$

33 ($R^2 = 0.86$, $\text{SE} = 0.003 \text{ ml} \cdot \text{kgBM}^{-1} \cdot \text{m}^{-1}$)

1

2 **Physiological and biomechanical responses to the race**

3 Running time, v_{mean} and mean heart rate (HR) of the three stages are reported in Table 3.

4 Mean cumulative running time was 8:15:08±1:36:49 hours:min:sec, mean speed was 12.8±2.0
5 km·h⁻¹ and mean %HRmax was 85.0±3.2% (corresponding to 76.2±4.6% of $\dot{V}O_{2\text{max}}$).

6 As shown in Table 4, there was not a chronic stage effect (i.e: P=0.124) on BM, conversely,
7 an acute stage effect (i.e.: P<0.001) on BM was observed after the first and second stage (by -
8 1.3±1.1 and -3.9±3.0 kg, P<0.001, respectively). The mean CoT of the individual stages did
9 not increase significantly with stage number (P=0.135), thus ruling out any chronic stage
10 effect. However, a statistically significant acute stage effect on CoT was observed at the end
11 of the first, second and third stages (+4.3±5.1, +6.6±4.1 and +4.2±4.0 %, respectively,
12 P<0.05). Finally, no chronic or acute stage effect on respiratory exchange ratio (RER) was
13 observed.

14 No significantly changes on biomechanical parameters were observed before and after the
15 three stages (Tab. 4), with the exception of the FPI which increased significantly at the end of
16 the first, second and third stages (11.9±9.1, 31.6±24.6 and 22.2±21.2 %, respectively,
17 P<0.001) and for the maximal ground reaction force (GRF) which decreased significantly at
18 the end of the first and second stage (-4.0±4.6 and -3.8±4.9 %, respectively, P<0.05).

19 In order to identify the main factors affecting CoT during an ultra-endurance running race, the
20 effects of the relative changes of the biomechanical parameters before and after the three
21 stages on the corresponding relative changes of CoT were investigated as follows. The
22 relative changes of each variable (X) were calculated as $[(X_b - X_a) \cdot X_{bc}^{-1}] \cdot 100$ where X
23 denotes any given variable before (b) or after (a) the stage considered divided by the
24 corresponding X measured before competition (X_{bc}). To this aim, only the biomechanical
25 parameters which were significantly correlated with CoT before the race (k_{vert} , FPI, f and
26 W_{ext}) were considered.

27 Considering all the stages together, the results of multiple regression showed that changes in
28 FPI ($r = 0.59$, P<0.001) had the largest role in determining ΔCoT followed by changes in f (r
29 $= 0.39$, P<0.001) and changes in k_{vert} ($r = -0.35$, P<0.05). The resulting overall relationship
30 was described by the following equation:

31

$$32 \Delta\text{CoT} = 0.09 \cdot \Delta\text{FPI} + 0.69 \cdot \Delta f - 0.09 \cdot \Delta k_{\text{vert}} + 33.97 \quad (4)$$

$$33 (R^2 = 0.62, \text{SE} = 4.73 \%)$$

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It is worth to note that an analysis of the second stage only, which corresponded to the longest and the hardest one, showed the same trend as reported above for the entire competition. However, the multiple regression analysis showed that the role of the Δ FPI in determining Δ CoT increased substantially ($r = 0.74$, $P < 0.001$). Whereas, that of f decreased ($r = 0.32$, $P < 0.05$) and that of k_{vert} ($r = -0.38$, $P < 0.05$) remained essentially unchanged. The corresponding overall multiple regression between these three variables and Δ CoT (%) is described by the following equation:

$$\Delta\text{CoT} = 0.12 \cdot \Delta\text{FPI} + 0.41 \cdot \Delta f - 0.10 \cdot \Delta k_{\text{vert}} + 59.10 \quad (5)$$

($R^2 = 0.79$, $SE = 3.35\%$).

Since Δ FPI had the greatest role in setting Δ CoT during the hardest stage of the race ($r = 0.74$, $P < 0.001$), a further statistical analysis was performed to investigate the physiological characteristic of the lower limbs which had the largest correlation with FPI. The results showed that FPI was inversely related to P_{max} ($r = -0.69$, $P < 0.05$), k_{vert} ($r = -0.63$, $P < 0.05$), k_{tendon} ($r = -0.76$, $P < 0.05$) and tendon force (F_{tendon} , $r = -0.69$, $P < 0.05$). Conversely, F_{tendon} was directly related to morphological properties of the GM as pennation angle ($r = 0.73$, $P < 0.001$), fiber length ($r = 0.74$, $P < 0.001$) and muscle thickness ($r = 0.70$, $P < 0.001$).

DISCUSSION

The main results of the present study showed that 1) high level performance in long-distance running depends on high $\dot{V}O_{2\text{max}}$ ($r = 0.77$), high F ($r = 0.36$) and low CoT_{mean} ($r = -0.30$); 2) low CoT values before the race are related to high P_{max} and k_{vert} , and low FPI, f and W_{ext} ; and 3) about 50% of the increase in CoT during the stages of the competition is related to changes in FPI which in turn is associated with the myotendinous characteristics of the lower limb.

Factors determining performance

As previously observed by di Prampero et al., 1986, high level performance in long-distance running depends on, 1) a large value of $\dot{V}O_{2\text{max}}$, 2) a large fraction of it, F , that can be sustained throughout the competition and, 3) a small value of CoT . Indeed, high correlations have been demonstrated between $\dot{V}O_{2\text{max}}$ and running performance in groups of runners of quite different abilities (Maughan and Leiper, 1983). Also in the present study, $\dot{V}O_{2\text{max}}$ was

1 found to be the single variable having the largest role in determining performance ($r=0.79$).

2 However, when groups of athletes with a relatively narrow range of $\dot{V}O_{2max}$ are studied, \dot{V}
3 O_{2max} becomes a less sensitive predictor of performance, F and CoT becoming crucial for
4 performance in distance running (Maughan and Leiper, 1983).

5 Saunders et al., 2004 , showed that a number of physiological and biomechanical factors
6 appear to influence CoT in trained runners. In the present study, a low CoT value was
7 significantly related to high Pmax ($r= -0.74$), high k_{vert} ($r= -0.65$) and low FPI ($r= 0.70$),
8 confirming previous studies which underline the role of the muscle-tendon complex stiffness
9 in storing and releasing elastic energy (Spurrs et al., 2003). Particularly, a low FPI indicates
10 that the trajectory of the foot center of pressure remains close to the foot axis, thus suggesting
11 that a better ankle stability (Huang et al., 2011; Willems et al., 2005) allows better elastic
12 energy absorption along the foot axis (Ker et al., 1987). It should be noted that, Arellano and
13 Kram, 2011 , reported that step width in running is near zero and that running with relatively
14 wide steps is mechanically and energetically wasteful since the goal of running is to move the
15 body in the forward direction. After prolonged exercise, the subjects may experience
16 difficulty balancing due to fatigue (Lepers et al., 1997). Even though it was not measured, it is
17 reasonable to infer that, in order to maintain balance, the subjects increased step width. This
18 would bring about greater medio-lateral forces and hence a higher FPI.

19 As previously described by Saunders et al., 2004 and also showed in the present study, low
20 W_{ext} and low f were directly related to low CoT. A significant positive correlation between
21 CoT and W_{ext} was in fact found also by Bourdin et al., 1995 , who showed that the W_{ext}
22 could explain a large part of the variations of CoT among subjects at a given velocity.
23 In addition, Cavanagh and Williams, 1982 , showed that in well trained athletes the aerobic
24 demand of running at a given speed is lowest at a self-selected stride length and step
25 frequency due to the fact that runners naturally acquire an optimal value of these variables
26 over time, based on perceived exertion. It should also be noted that, whereas lowering step
27 frequency would be beneficial in terms of lowering CoT (Gimenez et al., 2013; Morin et al.,
28 2011), it might also cause greater muscular damage which could have negative consequences
29 in long races (Millet et al., 2012).

30

31 *Physiological and biomechanical responses to the race*

32 In the present study, CoT increased significantly at the end of the first (+4.3%), second
33 (+6.6%) and third (+4.2%) stage. The paragraphs that follows are therefore devoted to a

1 discussion of the factors associated with the increase of CoT. The above mentioned increases
2 in CoT are greater than observed over classical marathons (Brueckner et al., 1991), probably
3 because of the peculiarities of the race terrain, the characteristics of which will substantially
4 add to the physiological, biomechanical and metabolic demands of the performing athlete. On
5 the average, only two biomechanical parameters changed significantly at the end of each
6 stage: FPI and maximal GRF. These results are in line with the study of Morin et al., 2011 ,
7 who considered running biomechanics over a 24-h treadmill run and observed changes in
8 biomechanics parameters only after 4 hours. Kyrolainen et al., 2000 , showed that the
9 increase of CoT cannot be explained by changes in running mechanics after a marathon for
10 the entire group of subjects, since they observed significant interindividual variations inside
11 the group. This suggest that other parameters, such as the differences of internal work
12 between pre- and post- race could explain the increased CoT. Our measurements, even if the
13 internal work was not directly measured, showed a slight increase in step frequency, which
14 can suggest an increase in internal work (Cavagna et al., 1991).

15 To underline interindividual differences and considering the fact that an increase of CoT
16 throughout the event could explain the worse performance observed in some runners, we
17 compared the relative changes of CoT (ΔCoT , %) with the relative changes on biomechanical
18 parameters during the three stages. When considering only the second stage, i. e. the hardest
19 of the present study, a multiple linear regression showed that FPI changes (ΔFPI) has the
20 largest role ($r = 0.74$) in determining ΔCoT , followed by changes on k_{vert} (Δk_{vert} , $r = -0.38$)
21 and f (Δf , $r = 0.32$).

22 A significantly increase in FPI observed at the end of each stage underlines a reduction in
23 ankle control and then an increase on ankle instability as shown by previous authors (Huang
24 et al., 2011; Willems et al., 2005). This information suggests that the increased ankle
25 instability brings about a reduction of the fraction of elastic energy recovered thanks to the
26 arch of the foot, which, as shown by Ker et al., 1987 , is responsible for about 30% of the
27 overall elastic energy recovery. This hypothesis, is coherent with our results showing that
28 lower FPI was related to higher P_{max} , k_{vert} , k_{tendon} and F_{tendon} .

29

30 In this connection, it is interesting to point out that the k_{tendon} observed in our runners (463
31 $\text{N}\cdot\text{mm}^{-1}$, Tab. 2) is greater than observed in sedentary subjects (319 $\text{N}\cdot\text{mm}^{-1}$, Rosager et al.,
32 2002). However, this higher k_{tendon} is associated with a greater cross sectional area (CSA)
33 which in our runners turned out to be 92 mm^2 (Tab. 2) as compare to 73 mm^2 to sedentary
34 subjects (Rosager et al., 2002). Thus when normalizing k_{tendon} for the corresponding tendon

1 length and CSA, the obtained results (i.e. the Young modulus, 1.07 GPa, Tab. 2) is essentially
2 equal to that reported in the literature for sedentary subjects (1.02 GPa, Rosager et al.,
3 2002). It can be concluded that long term endurance training leads to a greater k_{tendon} . In
4 particular, in our group of runners, the increased stiffness is due to a hypertrophy of the
5 tendon (i.e. to an increased CSA) without any change of its material properties, as shown by
6 the unchanged Young modulus. It should be considered that an excessive increase of k_{tendon}
7 may lead to the opposite effect, i.e. a decreased recovery of elastic energy (Lichtwark and
8 Wilson, 2008; Magnusson et al., 2003) and hence a higher CoT, a fact that probably did not
9 occur in our subjects.

10 In addition, the greater F_{tendon} was related to greater pennation angles ($r= 0.73$) and greater
11 thickness ($r= 0.70$) of the GM muscle, both suggesting a greater packing of contractile
12 material (Kawakami et al., 1993) and hence an increased number of sarcomeres in parallel
13 (Abe et al., 1997). Moreover, the observed increase in fibre length, likely enabling the
14 sarcomeres to operate closer to optimal length, as suggested by Narici and Maganaris, 2007 ,
15 may be an additional factor contributing to the observed great F_{tendon} . As observed previously
16 (Fletcher et al., 2010), these observations emphasize the importance of the lower limb muscle
17 characteristics to maximizing gastrocnemius efficiency during running and reducing CoT
18 (Lichtwark and Wilson, 2008).

19 Finally, we would like to point out that the analysis of the relationship between the
20 biomechanical and bioenergetics characteristics of endurance running man, help us to better
21 understand the evolutionary history of this remarkable form of human locomotion (Bramble
22 and Lieberman, 2004).

23

24 In conclusion, performance was directly proportional to $\dot{V}O_{2\text{max}}$ and F and inversely
25 proportional to CoT_{mean} . Particularly, we have shown that low CoT values before the race are
26 related to high P_{max} and k_{vert} , and low FPI, f and W_{ext} . Finally, for the first time to our
27 knowledge we have shown that the increases of CoT during the stages of the competition can
28 be predicted by the changes in FPI which are responsible for about 50% of its changes which
29 in turn are associated with myotendinous characteristics of the lower limb. Taken as a whole,
30 our results suggest that athletes with better ankle stability will achieve better performance in
31 ultra endurance running competitions.

32

1 **RESEARCH DESIGN AND METHODS**

2 **Subjects**

3 Fifteen healthy Caucasian male runners (age range 29-54 years) participated in the ultra-
4 endurance competition named “Magraid”. The experimental protocol was approved by the
5 Ethics Committee of the University of Udine, Italy. Before the study, the purpose and
6 objectives were carefully explained to each subject and written informed consent was
7 obtained from all of them. Subjects having overt metabolic and/or endocrine diseases and
8 those taking medications regularly or using drugs known to influence energy metabolism
9 were excluded. The participants were recruited among experienced ultraendurance runners
10 who filled questionnaires on physical exercise activity. All the participants of this study had
11 run at least one race longer than 100 km. On average, their training experience amounted to
12 (mean \pm standard deviation) 12 ± 5 years, of which 6 ± 3 years of ultra-endurance running.
13 They reported to run on average 75.8 ± 16.8 km \cdot week⁻¹. Fifteen athletes who were eligible for
14 the study began the race, and the 11 ones who completed the entire competition were
15 considered for the data analysis.

16

17 **Experimental protocol**

18 One week before the race, the subjects came to the laboratory, where anthropometric
19 characteristics, body composition, triceps surae k_{tendon} and morphological properties of the
20 GM were performed. Furthermore, the maximal explosive jumping muscle power of the lower
21 limb was measured, and a graded exercise test to exhaustion on a treadmill was performed.
22 The subjects were asked to refrain from any vigorous physical activity during the two days
23 preceding the test and on a preliminary testing session they were thoroughly familiarized with
24 all the different measurements.

25 The competition “Magraid” took place in summer. It consisted of three stages of 25, 55 and
26 13 km on three consecutive days in the North-East of Italy. The geologic texture of the terrain
27 is an unusual soil in respect the vast majority of ultra-endurance competitions; it is
28 characterized by a gravel (locally named “Magredi”) from the braided river “Cellina-
29 Meduna”. The first day, stage 1 began at 6.00 p.m. with temperature and relative humidity of
30 26°C and 77%. The second and third days, stages 2 and 3 began at 10.00 a.m. with
31 temperature and relative humidity of 22 and 20°C and 80 and 85%, respectively.

32 Before and immediately after (mean time interval: 5 ± 3 min) each running stage, BM, CoT,
33 RER, running biomechanics and mechanical work were measured. In addition, HR and GPS

1 coordinates were continuously recorded throughout the three stages (Garmin Forerunner 305
2 GPS, Kansas City, USA).

3

4 **Physiological measurements before the race**

5 *Anthropometric characteristics and body composition*

6 BM was measured to the nearest 0.1 kg with a manual weighing scale (Seca 709, Hamburg,
7 Germany), stature was measured to the nearest 0.001 m on a standardized wall-mounted
8 height board. Body mass index (BMI) was calculated as $BM \text{ (kg)} \cdot \text{stature}^{-2} \text{ (m)}$. Body
9 composition was measured by bioelectrical impedance (BIA, Human IM Plus; DS
10 Dietosystem, Milan, Italy) according to the method of Lukaski et al., 1986 . Body
11 composition (fat-free mass, FFM, and fat mass, FM) was obtained from the software provided
12 by the manufacturer.

13

14 *Triceps surae tendon stiffness.*

15 Maximal voluntary torque (MVT) of plantarflexors was measured during an isometric
16 maximal voluntary contraction (MVC) with the participant laying prone. His right foot was
17 tightened around the adapter of an isokinetic dynamometer (Cybex Norm, CSMi, MA, USA).
18 Straps were also tightened around the hips to prevent a forward displacement of the body
19 during maximal plantarflexions. Participants were positioned with the knee fully extended and
20 an ankle angle of -20° with the lateral malleolus aligned with the axis of rotation of the
21 dynamometer (Maganaris, 2002; Maganaris, 2003). Before MVCs, the participants performed
22 five submaximal plantarflexions and dorsiflexions as a warm up. MVCs were elicited by
23 requesting the subject to increase the plantarflexion moment gradually over a 5-s period. The
24 plantarflexors torque, was obtained adding the torque generated by the activation of the
25 (antagonist) tibialis anterior, to the overall measured torque. In turn, the tibialis anterior
26 torque was estimated from its electromyographic (EMG) activity, as described below.
27 EMG activity of the tibialis anterior was recorded while performing maximal isometric
28 plantarflexions and dorsiflexions by pre-gelled surface EMG electrodes (circular contact area
29 of 1 cm diameter, BIOPAC Systems, Inc., USA) placed at one-third of muscle length to
30 avoid the motor point with an inter-electrode distance equal to 20 mm. The reference
31 electrode was placed on the lateral femoral condyle. Before placement of the electrodes, the
32 skin was shaved to remove hair, and the recording sites were rubbed lightly using abrasive gel
33 and cleansed with alcohol swabs to reduce interelectrode impedance. The raw EMG activity
34 was acquired at sampling frequency of 2000 Hz and processed with a multichannel analog-to-

1 digital converter (Biopac Systems, Santa Barbara, CA, US). The raw EMG signal was filtered
2 with band-pass filters set at 10-500 Hz, and amplified with a gain of 2000. This allowed us to
3 determine the relationship between EMG amplitude and torque exerted by the tibialis anterior
4 as determined in the relaxed state and during two submaximal ankle dorsiflexion contractions.
5 The dorsiflexion torque exerted by the tibialis anterior, as estimated from its EMG activity,
6 was then added to the net MVC plantarflexion torque, thus allowing us to obtain the
7 contribution of the triceps surae (Morse et al., 2008). The triceps surae tendon moment arm of
8 the ankle joint was measured as the distance from the center of rotation of the ankle joint to
9 the tendon axis (Morse et al., 2008). In addition, the foot moment arm of the ankle joint was
10 measured as the distance from the center of rotation of the ankle joint to the distal head of the
11 first metatarsal bone. Then, the triceps surae F_{tendon} was calculated by multiplying the force
12 measured at the footplate by the ratio of foot moment arm to tendon moment arm. The
13 compensation of moments due to gravitational forces was done for all subjects before each
14 ankle plantar flexion contraction.

15 Tendon elongation measurements were taken using a 7.5 MHz, linear, B-mode ultrasound
16 probe (Esaote Biomedica, AU3Partner, Florence, Italy). Details of the methodology employed
17 have been described elsewhere (Maganaris and Paul, 2000). First, consecutive axial-plane
18 scans were taken along the belly of the gastrocnemius medialis muscle with a 2 cm interscan
19 gap. The medial and lateral borders of the muscle in each scan were identified, and the
20 midpoint between the two borders was marked on the skin. Sagittal-plane scans were then
21 taken at the level of the heel to identify the insertion point of the triceps surae tendon in the
22 calcaneus, which was also marked on the skin. A straight line connecting the Achilles tendon
23 insertion with all midpoints marked along the muscle was assumed to be the midlongitudinal
24 mid-sagittal axis of the muscle–tendon unit. The scanning probe was displaced along this axis
25 to locate the distal myotendinous junction of the muscle, and subsequently the probe was
26 placed over a marker fixed to the skin, which cast a line on the ultrasound image and served
27 as a reference position to measure tendon tensile displacement. The relevant scans were
28 identified, and tendon displacement was measured using digitizing software (Kinovea –
29 version 0.8.7 - Joan Charmant & Contrib).

30 The length and CSA of the triceps surae tendon were quantified from sonographs recorded at
31 rest with the probe described above. The distance between the tendon's origin and insertion
32 along the mid-sagittal axis of the muscle–tendon unit was measured manually to the nearest
33 millimeter and considered to be the tendon's original length. The triceps surae tendon cross-

1 sectional area was digitized in axial-plane scans recorded 1, 2 and 3 cm above the tendon
2 insertion point in the calcaneus.
3 For each subject, the triceps surae tendon elongation was quantified during the MVC that
4 generated the highest plantarflexion moment. The elongation of the tendon at loads
5 corresponding to 0–100% of the plantarflexion moment generated was measured at 10%
6 intervals. First, the time points corresponding to the above loads were identified from the
7 moment-time relationship, and then the scans corresponding to those time-points were stored
8 in a computer and further processed. The approach followed for identifying the scans
9 corresponding to the loads examined assumes that the moment generated by the triceps surae
10 muscle during a ramp isometric contraction with the knee fully extended changes linearly
11 with the gross plantarflexion moment measured. Evidence for the validity of this assumption
12 has previously been obtained from EMG measurements (Magnusson et al., 2001).
13 Force-elongation data (i.e. tendon force vs. tendon length) were fitted with second-order
14 polynomials. k_{tendon} data were calculated from the slope of the force-elongation curve over
15 10% force-intervals (Maganaris, 2002). The corresponding tendon Young's modulus data
16 were calculated by multiplying the stiffness values by the ratio of tendon length to tendon
17 cross-sectional area.

18

19 ***Morphological properties of the Gastrocnemius Medialis.***

20 The participants laid prone, with the foot secured at -20° dorsiflexion. Fiber fascicle length
21 (L) and pennation angle (°) were measured using B-mode ultrasound probe (Esaote
22 Biomedica, AU3Partner, Florence, Italy). Images were obtained along the midsagittal plane of
23 the GM, at the mid-distance between the proximal and distal tendon insertion identified by
24 ultrasound (7.5-MHz linear-array probe). The head of the probe was held perpendicular to the
25 dermal surface to provide an image including both superficial and deep aponeuroses, and a
26 number of clearly visible fascicles that could be followed between the aponeuroses. To
27 improve acoustic coupling, water-soluble transmission gel was placed over the scan head.
28 Ultrasound scans were recorded at 25 Hz and analyzed offline with digitizing software
29 (ImageJ 1.44p, National Institute of Health, USA). Pennation angle was measured as the
30 angle of fascicle insertion into the deep aponeurosis, L was defined as the length of the
31 fascicle between the deep and superficial aponeuroses (Narici et al., 1996).

32

33 ***Maximal explosive jumping muscle power of the lower limb.***

1 The maximal explosive jumping muscle power of the lower limbs during very short all-out
2 efforts was assessed by means of the Explosive-Ergometer (EXER, University of Udine, Italy,
3 Fig. 1), previously described in detail elsewhere (Lazzer et al., 2009). Briefly, the EXER
4 consists of a metal frame supporting one rail inclined at 20° to the horizontal. The subject
5 sitting on a seat, fixed to a carriage free to move on the rail, accelerates himself and the
6 carriage seat backward pushing on two force platforms (LAUMAS PA 300, Parma, Italy).
7 The velocity along the direction of motion is continuously recorded by a wire tachometer
8 (LIKA SGI, Vicenza, Italy). The analogue outputs of the force and velocity transducers are
9 digitalized and recorded by a data acquisition system (MP 100 BIOPAC, USA). The subjects
10 were asked to perform four all-out efforts with the right leg and four with the left one, starting
11 from the same knee angle (110°). The requested starting knee angle was obtained by adjusting
12 the position of the mechanical blocks which also prevented the motion of the carriage seat
13 towards the platforms, thus impeding any counter movement. To prevent fatigue, after each
14 push the subjects rested for 2 min with their feet placed on a support. The mechanical power
15 (P, W) developed by the single lower limb was obtained from the instantaneous product of the
16 developed Force (N) times the backward speed (v , $m \cdot s^{-1}$):

17

$$18 \quad P(t) = \text{Force}(t) \cdot v(t) \quad (6)$$

19

20 Analysis of the time course of P allowed us to assess its peak (P_{\max} , W).

21

22 ***Graded exercise test to exhaustion.***

23 $\dot{V}O_{2\max}$ and maximal heart rate (HR_{\max}) were determined by a graded exercise test on a
24 treadmill (Saturn, HP Cosmos, Germany) under medical supervision. During the experiment,
25 ventilatory and gas exchange responses were measured continuously with a metabolic unit
26 (Quark-b², Cosmed, Italy). The volume and gas analysers were calibrated using a 3-L
27 calibration syringe and calibration gas (16.00% O₂; 4.00% CO₂), respectively. During the
28 tests, electrocardiogram was continuously recorded and displayed on line for visual
29 monitoring, and HR was measured with a dedicated device (Polar, Finland). The tests were
30 performed one week before the race and comprised a 5-min rest period followed by running at
31 10 $km \cdot h^{-1}$ for 5 min (on a slope of 1%); the speed was then increased by 0.7 $km \cdot h^{-1}$ every
32 minute until volitional exhaustion. A leveling off of oxygen uptake (defined as an increase of
33 no more than 1 $ml \cdot kg^{-1} \cdot min^{-1}$) was observed in all subjects during the last one or two minutes

1 of the exercise test indicating that $\dot{V}O_{2max}$ had been attained. $\dot{V}O_{2max}$ and HR_{max} were
2 calculated as the average oxygen uptake and HR of the last 20 s of the test. RER was
3 calculated as $\dot{V}CO_2 \cdot \dot{V}O_2^{-1}$. The gas exchange threshold (GET) was determined by the v-
4 slope method (Beaver et al., 1986).

6 **Metabolic cost of transport and biomechanical measurements during the race.**

7 Before and immediately after (mean time interval: 5 ± 3 min) each stage of the competition, the
8 subjects ran for 6 min on a treadmill (Zebris Medical GmbH, Isny, Germany) at a constant
9 speed of $10 \text{ km} \cdot \text{h}^{-1}$, close to the actual speed that athletes had maintained during the race. The
10 treadmill was positioned near the arrival line, integrated with a series of high quality
11 capacitive force sensors underneath the treading surface. The treadmill was connected to a
12 personal computer integrated with running software analysis (Win FDM-T, v 2.1.1. Zebris
13 Medical GmbH, Isny, Germany) yielding contact (t_c , s) and aerial (t_a , s) times at a sampling
14 rate of 100 Hz; duty factor (%), obtained dividing t_c by step time; step frequency (f , Hz);
15 maximal vertical GRF (N); and FPI (cm^2). FPI is a modified version of medio-lateral
16 trajectory of the centre of pressure (CoP) with respect to the foot axis as a function of time
17 during the stance phase used by Willems et al., 2005, and Huang et al., 2011; it was
18 obtained from the area between the foot axis (a line connecting the center of heel to the
19 midpoint of 2nd and 3rd metatarsal heads) and the CoP trajectory (see Fig. 2). This index is a
20 global evaluation of medio-lateral displacement during the whole stance phase: i.e. a FPI
21 equal or close to zero indicating that the trajectory of the CoP remains close to the foot axis,
22 higher values indicating large oscillations in the medio-lateral direction. For each subject, 10
23 subsequent “representative” steps (i.e. without anomalous movements of limbs, torsion of
24 head or trunk etc.) were analyzed and FPI was calculated by means of a custom-made Matlab
25 program.

26 CoT and RER were measured continuously with a metabolic unit (Quark-b², Cosmed, Italy),
27 as follows. The analyzer, calibrated prior to each testing session, provided breath-by-breath
28 data. The average of the final 2 min of sampling was used for further analysis. This averaging
29 phase did not start until the following two conditions had been met: 1) at least 4 min of
30 running had passed and 2) real-time plots of $\dot{V}O_2$, HR, and RER indicated that metabolic
31 steady state had been achieved. Net $\dot{V}O_2$ was obtained by subtracting pre-exercise standing
32 values, as measured before each stage, from gross $\dot{V}O_2$ at constant speed. This same

1 procedure was repeated before and after each running stage, on the implicit assumption that
 2 pre-exercise resting $\dot{V}O_2$ was not affected by the preceding running stage. CoT was then
 3 obtained by dividing net energy expenditure ($\text{mlO}_2 \cdot \text{kg}^{-1} \cdot \text{s}^{-1}$) by speed ($\text{m} \cdot \text{s}^{-1}$). As mentioned in
 4 the introduction, CoT in running, in the range of speeds where the air resistance is negligible
 5 (i.e. $< 18 \text{ km} \cdot \text{h}^{-1}$), is independent of the speed. Hence the so obtained value applies throughout
 6 the investigated speeds. RER was always below 1.0 confirming that aerobic metabolism was
 7 the main metabolic pathway.

8 The biomechanics of treadmill running was studied using two digital cameras at 210 fps
 9 (Basler - Pilot, Ahrensburg, Germany). The video sequences were recorded between the
 10 fourth and the fifth minute because in an earlier study (Karamanidis et al., 2003) found that
 11 after 2–3 min running on a treadmill the running characteristics are very reproducible.

12 The cameras were placed symmetrically 5 m behind the treadmill, spaced 6 m one from the
 13 other, and were calibrated using a square frame ($1 \text{ m} \cdot 1 \text{ m}$). To improve the quality of the
 14 video analysis, seven reflective markers (radius 10 mm) were used to identify joint positions.

15 The markers were fixed on the following landmarks (left side): metatarsal head V, lateral
 16 malleolus, calcaneus, femur lateral epicondyle, spina iliaca (right and left) and over the
 17 second lumbar vertebra. The video recordings were digitized using a software (Simi Reality
 18 Motion System, GmbH Max-Planck-Str., Germany) and three-dimensional position of each
 19 marker was reconstructed.

20 The data were smoothed through a moving-average filter (Radius = 1) and the position of
 21 centre of mass (CoM) was calculated as the mean position of the markers placed over the
 22 spina iliaca (right and left) and over the second lumbar vertebra (Bourdin et al., 1995; Myers
 23 and Steudel, 1985; Taboga et al., 2012). For each subject, 10 subsequent “representative”
 24 steps (i.e. without anomalous movements of limbs, torsion of head or trunk etc.) were
 25 analyzed by means of a custom-made Matlab program. External mechanical work was
 26 calculated from the positive variations of total mechanical energy (potential and kinetic) of
 27 CoM, as described by Cavagna et al., 1976. Total external mechanical work per unit of
 28 distance (W_{ext}^T , $\text{mlO}_2 \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$) was then calculated as:

$$29 \quad W_{\text{ext}}^T = \frac{W_{\text{ext}}^{\text{tot}}}{d} \quad (7)$$

30 where $W_{\text{ext}}^{\text{tot}}$ is the total external mechanical work and d is the distance travelled during the
 31 analyzed steps. Mass-specific external mechanical work per unit distance W_{ext} ($\text{mlO}_2 \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$)
 32 was then calculated dividing W_{ext}^T by the BM of the subject.

1 In addition, total stiffness (k_{vert} , $\text{N} \cdot \text{mm}^{-1}$) was calculated as the ratio between peak GRF and
2 the vertical displacement of the CoM during the stance phase.

3 During these ten steps, stride cycle (between two consecutive heel strikes of the same left
4 foot) was analyzed. The joint angles of the knee were also measured at maximal extension
5 (Ext_{max} , $^{\circ}$), maximal load (Load_{max} , $^{\circ}$) and maximal flexion (Flex_{max} , $^{\circ}$).

7 **Statistical analyses**

8 Statistical analyses were performed using PASW Statistic 18 (SPSS Inc., IL, USA) with
9 significance set at $P < 0.05$. All results are expressed as means and standard deviation (SD).
10 Changes of BM, CoT, RER and biomechanical parameters during the race were studied with
11 General Linear Model repeated measures with two factors considering chronic stage effect
12 (called “Stage”: Stage 1 vs Stage 2 vs Stage 3) and the acute stage effect (called “Time”:
13 before vs after). When significant differences were found, a Bonferroni post hoc test was used
14 to determine the exact location of the difference.

15 Equation 1 yields v_{end} values in long distance running; however, as written, it does not take
16 into account the increase of CoT that may occur during the competition, as observed
17 previously (Lazzer et al., 2012). Therefore, the mean value of CoT throughout the race
18 (CoT_{mean}) was estimated as follows:

19

$$20 \text{CoT}_{\text{mean}} = [[(\text{CoT}_{\text{Ib}} + \text{CoT}_{\text{Ia}}) \cdot 0.5 \cdot d_{\text{I}}] + [(\text{CoT}_{\text{IIb}} + \text{CoT}_{\text{IIa}}) \cdot 0.5 \cdot d_{\text{II}}] + [(\text{CoT}_{\text{IIIb}} + \text{CoT}_{\text{IIIa}}) \cdot 0.5 \cdot d_{\text{III}}]] \cdot (d_{\text{I}} + d_{\text{II}} + d_{\text{III}})^{-1} \quad (8)$$

22

23 where the suffix I, II, and III refer to the first, second and third stage, b and a indicate the CoT
24 value assessed immediately before (b) and after (a) the appropriate stage, the distance of
25 which are indicate by d ($d_{\text{I}} = 25000 \text{ m}$; $d_{\text{II}} = 50000 \text{ m}$; $d_{\text{III}} = 13000 \text{ m}$). Therefore, applying
26 equation 1 to the overall competition and taking into account the average value of CoT_{mean} , as
27 from equation 8, one obtains:

28

$$29 v_{\text{end-mean}} = F \cdot \dot{V}\text{O}_{2\text{max}} \cdot \text{CoT}_{\text{mean}}^{-1} \quad (9)$$

30

31 In turn, F was estimated from the mean HR determined throughout each individual stage and
32 expressed as a fraction of the corresponding maximal HR. It should be noted that F may be
33 better predicted by considering the ratio of the mean HR increase above resting, throughout

1 each stage, to the HR reserve. However, in view of the fact that resting HR is somewhat
2 difficult to assess precisely, we preferred to stick to absolute values, as described above. The
3 role of each of the three factors of equation 9 was evaluated with a simple linear regressions
4 determined between each individual variable and endurance speed; Pearson's correlation
5 coefficients were used to analyze the association between variables. Subsequently, in order to
6 calculate multiple regression coefficients of all three factors combined as in equation 9, it is
7 convenient to use the logarithmic transformation:

8

$$9 \log v_{end-mean} = \log (F \cdot \dot{V}O_{2max} \cdot CoT_{mean}^{-1}) = \log F + \log \dot{V}O_{2max} - \log CoT_{mean} \quad (9')$$

10

11 This multivariate analysis enabled us to assess the role of each variable in setting the athletes'
12 performance.

13 In addition, the relationships between biomechanical variables affecting CoT were
14 investigated using Pearson's product-moment correlation coefficient.

15

16 **LIST OF SYMBOLS AND ABBREVIATIONS**

17 BM: body mass

18 BMI: body mass index

19 CoM: centre of mass

20 CoP: centre of pressure

21 CoT : metabolic cost of transport

22 CSA: cross sectional area

23 *d*: distance travelled during the analyzed steps

24 EMG: electromyography

25 Ext_{max}: maximal extension joint angle of the knee

26 Flex_{max}: maximal flexion joint angle of the knee

27 *f*: step frequency

28 *F*: fraction of $\dot{V}O_{2max}$

29 FFM: fat-free mass

30 FM: fat mass

31 *F*_{tendon}: tendon force

32 FPI: Foot-print index

33 GM: gastrocnemius medialis

- 1 GRF: ground reaction force
2 HR: heart rate
3 k_{vert} : total stiffness
4 Load_{max} : maximal load joint angle;
5 TST: triceps surae tendon
6 k_{tendon} : tendon stiffness
7 L: fiber fascicle length
8 MVT: maximal voluntary torque
9 MVC: maximal voluntary contraction
10 P: mechanical power
11 °: degrees
12 RER: respiratory exchange ratio
13 RMS: root mean square
14 tc: contact
15 ta: aerial
16 $\dot{V}O_{2\text{max}}$: maximal O₂ intake
17 $\dot{V}CO_2$: CO₂ uptake
18 v : speed
19 X: variable
20 v_{end} : endurance speed
21 W_{ext}^T : external mechanical work per unit of distance
22 $W_{\text{ext}}^{\text{tot}}$: total external mechanical work
23 W_{ext} : mass-specific external mechanical work per unit distance
24

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31

32 **DISCLOSURES**

33 No competing interests, financial or otherwise, are declared by the author(s).

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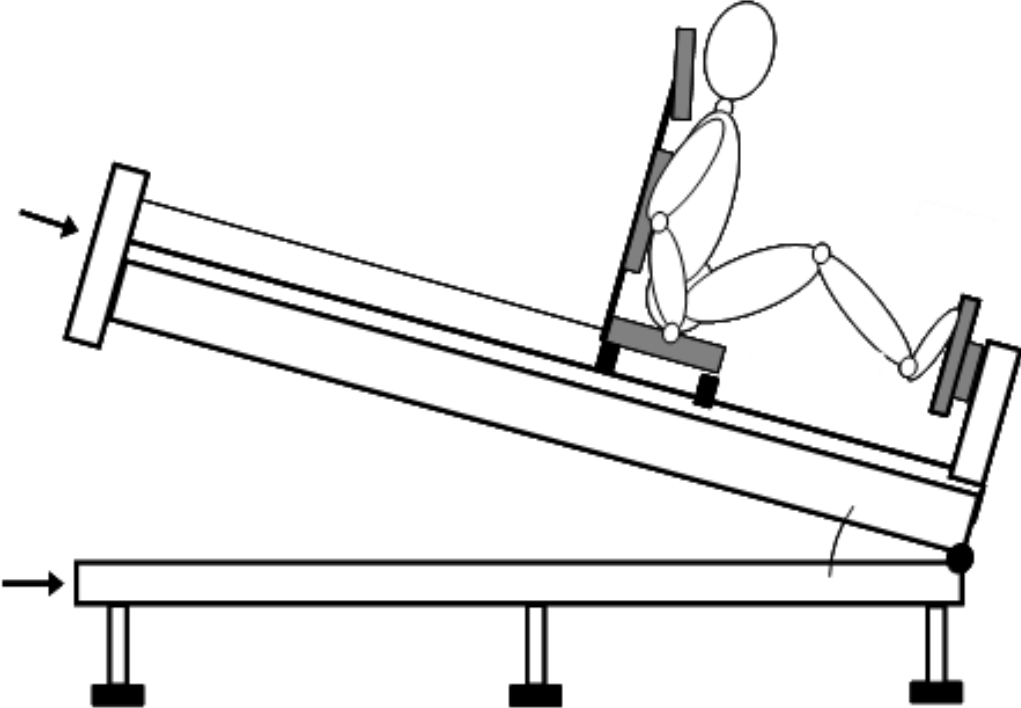
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Figure 1. Schematic view of the Explosive Ergometer (EXER).



WT: wire tachometer; CS: carriage seat; FP: force platform. Rail system (R) and lower frame (LF) are hinged (Hi).

Figure 2. Foot-print Index (FPI). Thick line (A): foot-axis; thin line (CoP): trajectory of the center of pressure during stance phase. Area between CoP and A (striped) in cm^2 is FPI.

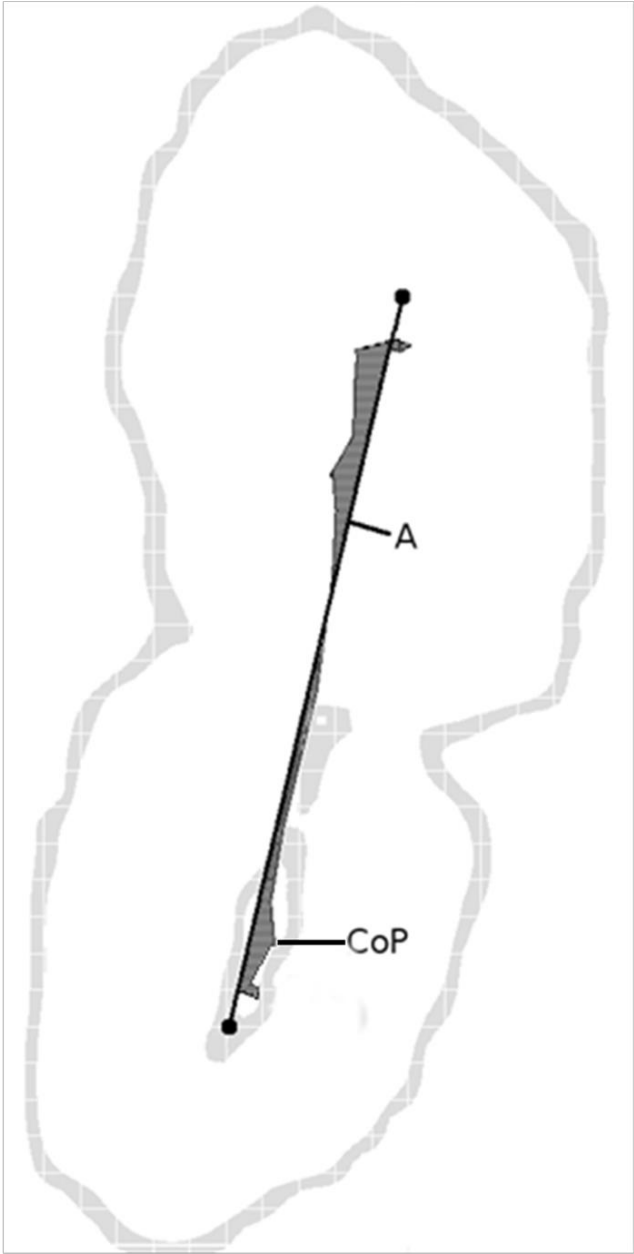


TABLE 1. Physiological characteristics of subjects (n = 11) before the race.

Age (yr)	40.5	±	8.4	[29.5	;	54.0]
Body mass (kg)	68.6	±	8.2	[57.0	;	81.0]
Stature (m)	1.72	±	0.06	[1.62	;	1.80]
Body mass index (kg·m ⁻²)	23.2	±	1.9	[20.8	;	26.4]
Fat-free mass (kg)	56.3	±	5.4	[48.4	;	64.9]
Fat mass (kg)	12.3	±	4.3	[7.6	;	22.8]
Fat mass (%)	17.6	±	4.4	[12.2	;	28.1]
P _{max} (W)	1759	±	202	[1319	;	1980]
$\dot{V}O_{2max}$ (ml·min ⁻¹)	3755	±	467	[2969	;	4387]
$\dot{V}O_{2max}$ (ml·min ⁻¹ ·kgBM ⁻¹)	55.2	±	6.7	[40.0	;	62.7]
RER	1.08	±	0.04	[1.02	;	1.13]
HR _{max} (bpm)	175.5	±	13.7	[147.2	;	194.9]
v _{max} (km·h ⁻¹)	17.8	±	1.6	[14.2	;	19.8]
CoT (mlO ₂ · kg ⁻¹ · m ⁻¹)	0.190	±	0.008	[0.182	;	0.197]
<i>Gas exchange threshold</i>								
$\dot{V}O_2$ (ml·min ⁻¹)	3251	±	488	[2741	;	4091]
$\dot{V}O_2$ (% $\dot{V}O_{2max}$)	86.6	±	6.5	[75.9	;	90.0]
RER	0.93	±	0.05	[0.83	;	1.02]
RER (% RER _{max})	86.4	±	4.0	[81.2	;	93.2]
HR (bpm)	154.1	±	11.9	[122.4	;	168.2]
HR (%HR _{max})	87.9	±	5.1	[81.1	;	92.2]
v (km·h ⁻¹)	14.1	±	1.7	[10.7	;	16.3]
v (% v _{max})	79.2	±	4.6	[71.2	;	85.3]

All values are mean ± standard deviation (SD). Range in square brackets. Pmax: maximal explosive muscle power of the one leg; $\dot{V}O_2$: oxygen uptake; RER: respiratory exchange ratio; HR: heart rate; v: velocity; CoT: metabolic cost of transport.

TABLE 2. Physiological characteristics of the triceps surae tendon (TST) and gastrocnemius medialis (GM) of subjects (n = 11) before the race.

TST- cross sectional area (mm ²)	92	±	14	[79	;	130]
TST- resting length (L ₀ , mm)	212	±	21	[190	;	250]
TST- strain ($\Delta L \cdot L_0^{-1}$, %)	7.9	±	0.8	[7.0	;	9.2]
TST- force (N)	4758	±	828	[3240	;	5421]
TST- stiffness (N·mm ⁻¹)	463	±	85	[357	;	612]
TST- Young module (GPa)	1.07	±	0.13	[0.90	;	1.30]
GM - fiber length (mm)	61.0	±	6.5	[49.0	;	68.9]
GM - pennation angle (°)	19.3	±	2.6	[15.0	;	23.0]
GM – thickness (mm)	18.2	±	2.9	[14.6	;	25.0]

All values are mean ± standard deviation (SD). Range in square brackets.

TABLE 3. Running time, mean velocity (v_{mean}) and mean heart rate (HR_{mean}) of the three stages ($n = 11$).

	Stage 1 (25 km)	Stage 2 (55 km)	Stage 3 (13 km)	Total
Running time (hh:mm:ss)	1:45:40 \pm 0:14:00 [1:29:12; 2:09:31]	5:30:43 \pm 1:12:15 [4:09:31; 7:44:33]	0:58:49 \pm 0:12:28 [0:48:29; 1:30:43]	8:15:08 \pm 1:36:49 [6:27:00; 11:24:41]
v_{mean} ($\text{km}\cdot\text{h}^{-1}$)	14.4 \pm 1.8 [11.6; 16.8]	10.4 \pm 2.1 [7.1; 13.2]	13.7 \pm 2.2 [8.6; 16.2]	12.8 \pm 2.0 [9.1; 15.4]
HR_{mean} (% of HR_{max})	90.6 \pm 3.7 [82.5; 96.0]	78.1 \pm 4.8 [69.0; 86.0]	86 \pm 4 [79.0; 92.0]	85.0 \pm 3.2 [81.3; 91.3]

All values are mean \pm standard deviation (SD). Range in square brackets.

TABLE 4. Body mass (BM), metabolic cost of transport (CoT), gas exchange ratio (RER) and biomechanical parameters determined before and immediately after each Stage.

	Stage 1 (25 km)		Stage 2 (55 km)		Stage 3 (13 km)		p		
	Before	After	Before	After	Before	After	Stage	Time	S x T
BM (kg)	68.8 ± 7.7	67.9 ± 7.9	68.8 ± 7.6	66.1 ± 7.7	68.1 ± 7.7	67.5 ± 8.1	0.124	0.001	0.087
CoT (mlO ₂ · kg ⁻¹ · m ⁻¹)	0.190 ± 0.008	0.197 ± 0.008	0.192 ± 0.006	0.205 ± 0.012	0.196 ± 0.009	0.203 ± 0.013	0.135	0.001	0.338
RER	0.83 ± 0.04	0.82 ± 0.12	0.80 ± 0.05	0.79 ± 0.07	0.79 ± 0.08	0.81 ± 0.11	0.092	0.276	0.096
Contact Time (sec)	0.131 ± 0.014	0.134 ± 0.016	0.135 ± 0.016	0.133 ± 0.013	0.135 ± 0.011	0.135 ± 0.009	0.582	0.898	0.491
Aerial time (sec)	0.221 ± 0.025	0.213 ± 0.018	0.217 ± 0.025	0.214 ± 0.014	0.209 ± 0.017	0.215 ± 0.015	0.328	0.469	0.046
Duty factor (%)	37.4 ± 4.5	38.5 ± 4.2	38.6 ± 5.1	38.1 ± 3.2	39.4 ± 3.1	38.7 ± 2.7	0.336	0.931	0.187
Step frequency (step·s ⁻¹)	2.85 ± 0.15	2.87 ± 0.12	2.86 ± 0.10	2.87 ± 0.10	2.89 ± 0.11	2.89 ± 0.12	0.191	0.549	0.692
Foot-print Index (cm ²)	13.64 ± 4.72	14.95 ± 4.61	13.38 ± 5.15	16.93 ± 5.28	13.90 ± 4.18	16.51 ± 3.99	0.497	0.001	0.061
CoM (m)	0.054 ± 0.016	0.052 ± 0.011	0.050 ± 0.013	0.050 ± 0.013	0.049 ± 0.012	0.051 ± 0.013	0.262	0.826	0.690
GRF (N)	1473 ± 181	1409 ± 138	1458 ± 163	1400 ± 159	1454 ± 150	1474 ± 139	0.154	0.029	0.075
W _{ext} (mlO ₂ · kg ⁻¹ · m ⁻¹)	0.087 ± 0.013	0.088 ± 0.014	0.082 ± 0.009	0.085 ± 0.015	0.078 ± 0.009	0.078 ± 0.016	0.093	0.588	0.733
k _{vert} (N· m ⁻¹)	28360 ± 5734	27315 ± 5001	29120 ± 5868	29644 ± 5492	30771 ± 6324	30848 ± 5836	0.083	0.726	0.517
Ext _{max} (°)	169 ± 5	169 ± 3	170 ± 4	170 ± 6	170 ± 4	171 ± 4	0.362	0.899	0.558
Load _{max} (°)	143 ± 5	143 ± 5	145 ± 5	146 ± 6	145 ± 5	145 ± 5	0.221	0.461	0.304
Flex _{max} (°)	89 ± 8	88 ± 7	93 ± 7	91 ± 8	94 ± 9	90 ± 7	0.073	0.142	0.884

All values are mean ± standard deviation (SD). Range in square brackets.

BM: body mass; CoT: cost of transport; RER: respiratory exchange ratio; CoM: centre of mass; GRF: maximal vertical ground reaction force;

W: external mechanical work; k_{vert}: vertical stiffness; Ext_{max}: maximal extension joint angle of the knee; Load_{max}: maximal load joint angle;

Flex_{max}: maximal flexion joint angle of the knee.

Significance by GLM Repeated Measures with two factors of the main effects of Stage (S), Time (T, before vs after) and Interaction (S x T).

1 **Effects of the Etna uphill ultra-marathon on energy cost and mechanics of running**

2

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1 **ABSTRACT**

2 **Purpose:** To investigate the effects of an extreme uphill marathon on the mechanical
3 parameters that are likely to affect the energy cost of running (Cr).

4 **Methods:** Eleven runners (27-59 years) participated in the “Etna SuperMarathon” (43 km, 0-
5 3063 m a.s.l.). Anthropometric characteristics, maximal explosive power of the lower limb
6 (P_{\max}) and $V'O_{2\max}$ were determined before the competition. In addition, before and
7 immediately after the race, Cr, contact (t_c) and aerial (t_a) times, step frequency (f) and running
8 velocity (v) were measured at constant self-selected speed. Then, peak vertical ground
9 reaction force (F_{\max}), vertical downward displacement of the centre of mass (Δz), leg length
10 change (ΔL), vertical (k_{vert}) and leg (k_{leg}) stiffness were calculated.

11 **Results:** Direct relationship between Cr, measured before de race, and race time was shown
12 ($r=0.61$; $p<0.001$). Cr increased significantly at the end of the race by 8.7%. Immediately
13 after the race, the subjects showed significantly lower t_a (-58.6%), f (-11.3%), F_{\max} (-17.6%),
14 k_{vert} (-45.6%) and k_{leg} (-42.3%) and higher t_c (+28.6%), Δz (+52.9%) and ΔL (+44.5%) than
15 before the race. The increase of Cr was associated with a decrement in F_{\max} ($r=-0.45$), k_{vert}
16 ($r=-0.44$) and k_{leg} ($r=-0.51$). Finally, an inverse relationship between P_{\max} measured before the
17 race and ΔCr during race was found ($r=-0.52$).

18 **Conclusions:** Lower Cr was related with better performance, and athletes characterized by the
19 greater P_{\max} showed lower increases in Cr during the race. This suggests that specific power
20 training of the lower limbs may lead to better performance in ultra-endurance running
21 competition.

22

23 **Key Words:** maximal oxygen uptake; cost of transport; trail; kinematics; stiffness.

24

1 INTRODUCTION

2 The energy cost of running (Cr), together with the maximal aerobic power ($V'O_2max$), its
3 fraction (F) sustained throughout the competition and the maximal capacity of the anaerobic
4 stores (AnS) represent the main factors determining running performances^[1]. Cr , defined as
5 the amount of energy spent above resting to transport 1 kg body mass over 1 m distance
6 (expressed in $J \cdot kg^{-1} \cdot m^{-1}$ or $mlO_2 \cdot kg^{-1} \cdot m^{-1}$), plays a relevant role in determining the
7 performance among middle and long distance runners with the same $V'O_2max$ and F ^[2]. Its
8 average value amounting to $0.182 \pm 0.014 mlO_2 \cdot kg^{-1} \cdot m^{-1}$ ($3.75 \pm 0.29 J \cdot kg^{-1} \cdot m^{-1}$)^[1], with an
9 inter-individual variability of about 10%, and with lower values in endurance runners than in
10 middle distance runners.

11 Cr is unaffected by the speed from about $2.2 m \cdot s^{-1}$ to $5 m \cdot s^{-1}$ ^[1], where the air resistance plays
12 a minor role, less than 5% of the total energy cost^[3]. In long distance runners, Cr increases
13 with the distance covered because of the fatigue effects. Brueckner et al.^[4] observed an
14 increment of Cr of about 0.142% per km of distance during a marathon, with a total increase
15 greater than 5%. Indeed, Gimenez et al.^[5], in subjects who ran 24h on a motorized treadmill,
16 observed a substantial increases in Cr after 8 hours; in addition, the subjects who maintained
17 the highest speed (expressed in percentage of the velocity attained at $V'O_2max$) were those
18 having the smallest Cr increase over the 24. Furthermore, several authors^[6,7] have shown
19 that, in mountain ultra-marathons, the changes of Cr are brought about by changes of the
20 mechanics of running. The principal aim of which is to minimize damage to lower limb
21 tissue, muscular fatigue, and symptoms associated with prolonged running over irregular
22 terrain with a large positive/negative elevation variation along their race^[8,9].

23 The mechanics of running in different conditions has been frequently investigated using the
24 spring mass model^[10], i.e., representing the leg in contact with the ground as a simple linear
25 spring. In this model, the parameters most frequently studied are the leg (k_{leg}) and vertical

1 (k_{vert}) stiffness coefficients, associated with leg spring deformation (ΔL) and with the vertical
2 displacement (Δz) of the centre of mass, respectively. Thus, whereas, k_{vert} is a measure of the
3 resistance of the body to vertical displacement after application of ground reaction forces, k_{leg}
4 is the resistance to change in leg length after application of internal or external forces.

5 The effects of long and ultra-long races on running mechanics have recently been
6 investigated. Morin et al.^[11], considering a mountain ultra-marathon race (166 km, total
7 positive and negative elevation of 9500 m) showed that athletes significantly reduced
8 ($P < 0.001$) aerial time (t_a), peak vertical ground reaction force (F_{max}), Δz , with an increment in
9 step frequency (f). On the other hand, the contact time (t_c) was not different as compared to
10 before the race. Furthermore, there was a nearly significant ($P = 0.053$) change in k_{vert} , which
11 increased by 6% after the race. This study supports previous findings^[12], where the same
12 behaviour of f , brought about by a shorter t_a with no changes in t_c was reported. Conversely,
13 after 24 hours of treadmill running on the level, Morin et al.^[13] observed a reduction in F_{max} ,
14 Δz , ΔL , and an increment in k_{vert} and f , but with lower t_c and constant t_a . This discrepancy in
15 changes of t_c and t_a compared to previous studies could be due to the different mechanics of
16 uphill and downhill mountain running, as compared to treadmill running. As evidenced by
17 Fourchet et al.^[14], a 5h long hilly run induces different effects on ankle muscles, as compared
18 to flat running; in particular only plantar flexor muscles are affected by neuromuscular
19 alterations, likely leading to a different running mechanics between mountain and flat runs.

20 Indeed, interventions to reduce C_r are constantly sought after by athletes, coaches and sport
21 scientists. Strength^[15] and plyometric^[16] training allow muscles and tendons to utilize more
22 elastic energy and to reduce the amount of energy wasted in braking forces thus reducing C_r .
23 Therefore, the purpose of the present study was to investigate the effects of an extreme uphill
24 marathon on several mechanical parameters that are likely to affect C_r .

25

1 **RESEARCH DESIGN AND METHODS**

2 **Participants**

3 Sixteen healthy Italian male runners (age range 27-59 years) were enrolled in this study as
4 participants in the uphill marathon named “Etna SuperMarathon”. The experimental protocol
5 was approved by the Ethics Committee of the University of Udine. Before the study began,
6 the purpose and objectives were carefully explained to each subject and written informed
7 consent was obtained from all of them. Subjects having overt metabolic and/or endocrine
8 diseases and those taking medications regularly or using drugs known to influence energy
9 metabolism were excluded. The participants were recruited among experienced ultra-
10 endurance runners who filled out questionnaires on physical exercise activity, demographics,
11 medical history and lifestyle ^[17]. All the participants of this study had run at least one ultra-
12 endurance race in their career. On average, subjects had 9.3 ± 5.4 and 5.8 ± 5.6 years of training
13 history and of ultra-endurance running race, respectively. They reported to run on average
14 69.2 ± 23.5 km every week. Sixteen athletes who were eligible for the study began the race,
15 and the 11 who completed the entire competition were taken into account for data analysis.

17 **Experimental protocol**

18 One week before the race, the subjects came to the exercise physiology laboratory, where
19 anthropometric characteristics, mechanical power of the lower limbs and a graded exercise
20 test to exhaustion on a treadmill were performed. The subjects were asked to refrain from any
21 vigorous physical activity during the day preceding the test and during the preliminary testing
22 session that they performed to familiarize with all the different equipment.

23 The “Etna SuperMarathon” took place in June 2012. The race started at 8:00 AM from the
24 beach of Marina di Cottone (Catania, Italy), at sea level, with temperature and relative
25 humidity of 29°C and 42%, respectively. Athletes covered about 30 km on the road to the

1 Etna volcano, while the last part of the race took place on a path of lava rock. After a total
2 distance of about 43 km, athletes reached the finish line covering an altitude difference of
3 3063 m with a mean slope of about 7% and with peak values reaching 14% (Garmin
4 Forerunner 305 GPS, Kansas City, USA). At the finish, temperature and relative humidity
5 were 21°C and 52%, respectively.

6 The day before the race and immediately after the end of the race (4 ± 2 min), body mass
7 (BM), Cr, respiratory exchange ratio (RER) and running mechanics were measured.

8

9 **Physiological measurements before the race**

10 BM was measured to the nearest 0.1 kg with a manual weighing scale (Seca 709, Hamburg,
11 Germany), stature was measured to the nearest 0.001 m on a standardized wall-mounted
12 height board. Body mass index (BMI) was calculated as $BM \text{ (kg)} \cdot \text{stature}^{-2} \text{ (m)}$.

13 Maximal power of lower limbs during a counter movement jump was assessed by means of
14 the Bosco et al.^[18] test (Ergo Jump, Boscosystem, Italy) .

15 Maximal oxygen uptake ($\dot{V}O_{2\max}$) and maximal heart rate (HR_{\max}) were determined during
16 a graded exercise test on a treadmill (Saturn, HP Cosmos, Germany) under medical
17 supervision. During the experiment, ventilatory and gas exchange responses were measured
18 continuously with a metabolic unit (Quark-b², Cosmed, Italy). The volume and gas analysers
19 were calibrated using a 3-L calibration syringe and calibration gas (16.00% O₂; 4.00% CO₂),
20 respectively. During the tests, electrocardiogram was continuously recorded and displayed on
21 line for visual monitoring, and HR was measured with a dedicated device (Polar, Finland).

22 Before the start of the study, subjects were thoroughly familiarized with treadmill running.

23 The tests were performed one week before the race and consisted in a 5-min rest period
24 followed by running at $10 \text{ km} \cdot \text{h}^{-1}$ for 5 min (treadmill slope: 1%); the speed was then
25 increased by $0.7 \text{ km} \cdot \text{h}^{-1}$ every minute until volitional exhaustion. A levelling off of oxygen

1 uptake (defined as an increase of no more than $1 \text{ ml}\cdot\text{kg}^{-1}\cdot\text{min}^{-1}$) was observed in all subjects
2 during the last one or two minutes of the exercise test, indicating that $\dot{V}'\text{O}_2\text{max}$ had been
3 attained. $\dot{V}'\text{O}_2\text{max}$ and HR_{max} were calculated as the average oxygen uptake and HR of the
4 last 20 s of the test.

5

6 **Energy cost of running and mechanical measurements during the race**

7 The day before and immediately after the race, the subjects ran for 6 min at a constant self-
8 selected speed on two oval compact rock paths situated near the start line (at sea level) and
9 near the finish line (at 3063 m above sea level), respectively. Both compact rock paths were
10 flat and 50 m long.

11 Cr and RER were measured continuously with a portable metabolic unit (k4, Cosmed, Italy).
12 The analyser, calibrated prior to each testing session, provided breath-by-breath data
13 recording. The last minute of sampling was used for further analysis. For all subjects, real-
14 time plots of $\dot{V}'\text{O}_2$ and RER indicated that metabolic steady state was achieved after 5
15 minutes. Net $\dot{V}'\text{O}_2$, obtained by subtracting pre-exercise standing $\dot{V}'\text{O}_2$ (measured for 6 min
16 in resting condition before the race) from gross $\dot{V}'\text{O}_2$, was converted to joules using an
17 energetic equivalent for O_2 based on the RER. This RER was always below 1.0 confirming
18 that aerobic metabolism was the main metabolic pathway. Cr was then obtained by dividing
19 net energy expenditure ($\text{J}\cdot\text{kg}^{-1}\cdot\text{s}^{-1}$) by running speed (v , $\text{m}\cdot\text{s}^{-1}$); the latter was measured by
20 means of two photocells placed immediately before and after the video recording zone (see
21 below), at a distance of 10 m between them. In addition, average lap speed was obtained
22 dividing the circuit length by the time needed to cover it. Average lap speed was not
23 significantly different than running speed measured in the video recording zone. All subjects
24 were also requested to maintain the same self-selected speed during the tests before and after
25 the race.

1 The running mechanics was studied using a digital camera with a sample frequency of 400 Hz
2 (Nikon J1, Japan). The camera was placed perpendicular to the running direction of athletes.
3 For each subject, video was recorded between the fourth and the sixth minute of running. Ten
4 subsequent representative steps were analysed, taking into account t_c (s) and t_a (s).

5 Step frequency ($\text{step}\cdot\text{s}^{-1}$) was calculated as:

$$7 \quad f = \frac{1}{(t_a + t_c)} \quad \text{eq. 1}$$

8
9 Given t_c (s), t_a (s), v ($\text{m}\cdot\text{s}^{-1}$), subject's BM (kg), and lower limb length (distance between great
10 trochanter and ground during standing, L in m), spring mass parameters were calculated using
11 the computation method proposed by Morin et al.^[19]. This method, based on modelling of the
12 ground reaction force signal during the contact phase by a sine function, allows the
13 computation of k_{vert} ($\text{kN}\cdot\text{m}^{-1}$) as the ratio of the F_{max} (N) to the Δz (m). K_{leg} ($\text{kN}\cdot\text{m}^{-1}$) was then
14 calculated as the ratio of F_{max} and the ΔL (m,) during contact of the foot on the ground.

16 **Statistical analyses**

17 Statistical analyses were performed using PASW Statistic 18 (SPSS Inc., IL, USA) with
18 significance set at $p < 0.05$. All results are expressed as means and standard deviation (SD).
19 Normal distribution of the data was tested using the Kolmogorov-Smirnov test.
20 Changes of BM, Cr, RER and mechanical parameters during the competition were studied
21 with Student's paired t-test.
22 The relationships between mechanical variables affecting Cr were investigated using
23 Pearson's product-moment correlation coefficient.

1

2 **RESULTS**

3 The physical characteristics before the race of the 11 subjects who completed the race are
4 reported in Table 1, together with their performance time. Their average $\dot{V}O_2\text{max}$, Cr and
5 P_{max} were $49.2\pm 8.8 \text{ mlO}_2\cdot\text{min}^{-1}\cdot\text{kgBM}^{-1}$, $0.190\pm 0.023 \text{ mlO}_2\cdot\text{m}^{-1}\cdot\text{kg}^{-1}$ and $1628\pm 212 \text{ W}$,
6 respectively.

7 As reported in Figure 1, a direct relationship between Cr and race time was observed before
8 ($r= 0.61$, $p<0.001$) as well as after ($r= 0.48$, $p<0.05$) the race.

9 Immediately after the race, Cr was 8.7% higher ($p<0.001$) than before the race; on the
10 contrary, BM and self-selected running speed were 5.7% and 7.3% lower ($p<0.05$) than
11 before the race (Table 2). In addition, subjects showed significantly lower t_a (-58.6%), f (-
12 11.3%), F_{max} (-17.6%), k_{vert} (-45.6%) and k_{leg} (-42.3%) and higher t_c (+28.6%), Δz (+52.9%)
13 and ΔL (+44.5%) than before the race (Table 2).

14 In order to identify the main factors affecting Cr during the race, the mechanical parameters
15 measured before and after the race were plotted for all subjects as a function of Cr. Pearson's
16 correlation coefficients were then used to analyse the association between variables entering
17 these equations. This analysis showed an inverse relationships between Cr and F_{max} ($r= -0.45$,
18 Figure 2C), Cr and k_{vert} ($r= -0.44$, Figure 2E) and Cr and k_{leg} ($r= -0.51$, Figure 2F). No
19 significant relationships between Cr and t_c , t_a , step frequency, ΔZ and ΔL were found.

20 Finally, an inverse relationship between mechanical power of the lower limbs measured
21 before the race and changes in Cr during the race was found (Figure 3; $r= -0.52$).

22

23 **DISCUSSION**

24 The main results of the present study showed that 1) Cr is directly related with the race time;
25 2) Cr increased significantly at the end of this extreme uphill race (~9%); 3) the increase in Cr

1 was associated with a decrease in F_{\max} , k_{vert} and k_{leg} ; and 4) the greater the mechanical power
2 of the lower limbs the lesser the changes in Cr due to the race.

3

4 Several authors have shown that Cr is an important part of the success in athletes with
5 comparable $V'O_2\text{max}$ and F even if conflicting results have also been reported^[2]. Millet et
6 al.^[20] observed, during a 24 hours treadmill run, that Cr was not directly related to
7 performance but may nevertheless be important to be able to maintain a high $\%V'O_2\text{max}$. In
8 addition, Gimenez et al.^[5] have shown that Cr measured before the 24 hours treadmill run
9 was negatively correlated with the speed expressed in $\%V'O_2\text{max}$. This finding suggests that
10 a low Cr could be important in determining the performance during “low-intensity” ultra-
11 endurance events and our results support this view, since Cr was strongly related with race
12 performance (Figure 1).

13

14 At the end of this extreme uphill race, Cr was increased by about 9% compared to before the
15 race, as observed in previous studies considering ultra-marathon events^[5,6]. This difference
16 was greater than the ones observed during classic flat marathons^[4], probably because of the
17 relevant slope and altitude difference covered by subjects and because of the type of road
18 surface. As observed previously^[21], the increase in Cr with the slope is related with the
19 increase in total work including internal work. Furthermore, in the last part of the race (~15
20 km), the subjects ran on a path of lava rock. This terrain can contribute to increasing Cr as
21 compared to compact terrain, and could be attributed to a reduced recovery of potential and
22 kinetic energy at each stride^[22]. Indeed, as suggested by Millet et al.^[6], during long distance
23 running events, greatly exceeding the marathon, maintaining a high F may help reducing
24 damage to lower limb tissue, muscular fatigue and symptoms associated with prolonged
25 running, even if such a strategy may lead to increased Cr values; thus, in the end “sacrificing

1 economy to improve running performance". **On the other hand, in agreement with our**
2 **results, some authors** ^[23,24] **are of the opinion that Cr in ultra-marathon runners has an**
3 **important role in setting performance, suggesting that the same phenotype and**
4 **physiological factors, including Cr, that determine success in marathon running** ^[25] **are**
5 **also likely to determine success in ultra-marathons and this should be even more evident**
6 **when the level of ultra-endurance athletes increases** ^[23].

7 **Moreover**, we do not think that the increasing altitude (from 0 to 3063 m above sea level) had
8 any effect on Cr, while obviously leading to a fall of about 10-15% on $V'O_{2max}$. We would
9 like to point out that at sea level, before the race, $V'O_2$ at the speed of $173 \text{ m}\cdot\text{min}^{-1}$ was on the
10 average $42.7 \text{ ml}\cdot\text{kg}^{-1}\cdot\text{min}^{-1}$, i.e. about 87% of the corresponding $V'O_{2max}$. At altitude,
11 immediately after the race, $V'O_2$ was reduced to $36 \text{ ml}\cdot\text{kg}^{-1}\cdot\text{min}^{-1}$ at the speed of $161 \text{ m}\cdot\text{min}^{-1}$,
12 i.e. about 80-85% of the corresponding $V'O_{2max}$ estimated at altitude. The O_2 consumption of
13 the respiratory muscles, as obtained from the expiration ventilation (BTPS), according to
14 Coast et al. ^[26], amounted to 188 and $170 \text{ ml}\cdot\text{min}^{-1}$ at sea level and at altitude, respectively.
15 Thus, the energy cost of running, when subtracting the O_2 consumption of the respiratory
16 muscles and the resting $V'O_2$ (4.4 and $4.6 \text{ ml}\cdot\text{kg}^{-1}\cdot\text{min}^{-1}$ at sea level and at altitude) amounted
17 to 0.171 and $0.183 \text{ ml}\cdot\text{kg}^{-1}\cdot\text{m}^{-1}$, respectively. The resultant increase of Cr, about 7%, is
18 therefore essentially equal to that reported above. Then, the observed increase of Cr is
19 independent of the effects of altitude on $V'O_{2max}$ and on ventilation. Which, as is well known,
20 are widely different in different subjects and lead to larger decreases in individual $V'O_{2max}$
21 ^[27], the larger its sea level value ^[28].

22 In addition, we would like to point out that the RER amounted to 0.88 and 0.82 at sea level
23 and at altitude, respectively, and that these values are close to that can be expected for the
24 metabolic respiratory quotient for these exercise intensities.

1 At the end of the race, the following changes of the running mechanics were observed: lower
2 t_a , f , F_{max} , k_{vert} and k_{leg} and higher t_c , Δz and ΔL (Table 2). Only the decreases of t_a and F_{max}
3 were in line with previous studies on ultra-endurance events^[11,13,29]. These differences could
4 be related to the fact that the subjects ran, before and after the race, at self-selected speed
5 which represented their real optimal running speed. At the end of the race, subjects decreased
6 their self-selected speed during the test by 7.3% on the average, this reduction was related
7 with their degree of fatigue and represents the real effort that subjects were able to sustain
8 after the race. However, the changes in self-selected running speed observed during the test
9 before and after the race had only a partial effect on changes in the mechanical parameters
10 considered in the present study. In fact, as observed previously^[30], k_{leg} showed no statistical
11 differences at speeds between 2.5 and 3.5 $m \cdot s^{-1}$; in addition, the speed has no effect on k_{leg} ^[19].
12 Indeed, if the speed was reduced from 2.9 to 2.7 $m \cdot s^{-1}$, k_{vert} decreased from 33 to 32 $kN \cdot m^{-1}$
13 (-4%)^[30], which was not statistically significant. Morin et al.^[19] did not measure k_{vert} at
14 speeds as low as 2.9 and 2.7 $m \cdot s^{-1}$, even so, we fitted the data points reported in their study
15 with a 2nd order polynomial, obtaining the following equation:

$$16 \quad k_{vert} = 1.512 \cdot s^2 - 6.906 \cdot s + 34.022 \quad \text{eq. 2}$$

17 where k_{vert} is expressed in $kN \cdot m^{-1}$ and the speed (s) in $m \cdot s^{-1}$ ($N=5$ data points, $r^2=0.997$).

18 According to equation 2, at 2.9 and 2.7 $m \cdot s^{-1}$, k_{vert} would be 27 and 26 $kN \cdot m^{-1}$, respectively (-
19 1%). In the present study k_{leg} decreased by 42.3% and k_{vert} by 45.6%, thus suggesting that the
20 changes in these mechanical parameters observed in the present study were largely affected
21 by fatigue and only marginally by speed.

22 In addition, at the end of the race t_c increased (by ~29%) and t_a decreased (by ~59%), leading
23 to a significant decrease in step frequency (by ~11%). In turn, the observed increase of t_c lead
24 to a significant increase in Δz (by ~53%) and ΔL (by ~45%). Furthermore, k_{vert} and k_{leg}

1 decreases were strongly related to a reduction in F_{\max} and to the increase in vertical
2 displacement (Δz) which can be interpreted as a safer running style, as discussed below.
3 The differences in the changes of the mechanical parameters between the present study and
4 the previous ones on ultra-marathon^[11,13,29] can be explained as follow.

5 1) We considered self-selected speed as representative of the fatigue level of the subjects,
6 which induced different mechanical adaptations, particularly increasing t_c and consequently
7 reducing t_a and f . Dutto and Smith^[31] reported decreases in f accompanied by a decrease of
8 k_{vert} in long running trials, suggesting that it is the inability of the system to maintain an
9 optimal stiffness that drives to exhaustion. Furthermore, the decrease in f observed at the end
10 of the race, was probably related to the fact that this ultra-marathon was characterised by a
11 continuous positive work. This condition implies mainly concentric muscle contractions,
12 which induce less muscle damage in knee-extensor and plantar-flexors muscles than the
13 eccentric contractions characterising downhill running generally included in ultra-marathon
14^[8,9]. This condition may lead to lesser changes in running mechanics (aiming at decreasing the
15 load on the muscles) than observed in previous extreme ultra-marathons^[11,13,29]. In addition,
16 the decrease in f observed in the present condition is likely associated with a decrease in
17 internal work performance and thus in the corresponding cardiorespiratory responses, which
18 in turn, may be particularly relevant when running uphill at 3000 m above sea level.

19 2) A greater continuous positive work performance than observed in previous studies^[11,29],
20 which did not allow any recovery periods for the athletes during the race.

21 3) The potential differences between ultra-long distance running on a treadmill and over
22 ground^[13,20], which may have induced different adaptations of t_c .

23 4) The post-race tests were done immediately after the subjects crossing the finishing line
24 which allowed us to examine the real effects of total fatigue on metabolic and mechanical
25 parameters.

1 In order to identify the main factors affecting Cr during the ultra-endurance running race, the
2 effects of changes on mechanical parameters before and after the race were plotted for all
3 subjects as a function of the corresponding changes on Cr (Figure 2).

4 In particular, the increases in t_c with decreases in t_a , implied a decreases in F_{max} , which was
5 related with the increase in Cr during the race (Figure 2 C). These changes in running
6 mechanics can be interpreted as a safer running style associated with an overall lower impact,
7 especially during the eccentric phase of each step, to the detriment of an increase of Cr^[6].

8 In particular, the decrease of k_{vert} and k_{leg} , brought about by fatigue, induced each runner to
9 sink further during contact, i.e. increasing t_c and Δz . Furthermore the decreased f likely led
10 runners to a less efficient elastic energy utilization^[32], and therefore lower velocity, at the end
11 of the stance phase, resulting in a decreased t_a . Finally, a shorter t_a implies that the runner
12 landed with less downward momentum, thus requiring less upward impulse during the
13 subsequent stance phase, therefore also F_{max} was lower. In addition, a decreased F_{max} can also
14 be due to a reduced force capacity of subjects because of fatigue during the race. Our results
15 are in accordance with Morin et al.^[13] and Degache et al.^[29] who evidenced a decreased
16 F_{max} at the end of long running trials; however, the question if this is a strategy intentionally
17 adopted by runners or the result of fatigue, it remains unsolved.

18 Indeed, the most powerful athletes showed the lower changes in Cr (Figure 3). These results
19 are in agreement with previous studies in athletes^[15,16] which emphasize the importance of
20 the muscle-tendon system and strength training to reduce Cr. In addition, force reduction
21 during the race can lead to ankle instability^[33], thus leading to a reduction of the capacity of
22 the foot to utilize all the mechanical energy transmitted by the muscle-tendon complex for
23 forward displacement.

24

25 **Practical Applications**

1 Cr represents one of the main factors determining performances in ultra-endurance runners
2 and its increase during the competition is related to mechanics of running deterioration and
3 lower P_{max} . These data show the importance of the lower limb muscle's characteristics
4 which maximize efficiency and reduce Cr during running. This suggests that coaches and
5 ultra-endurance runners need to strengthen the specific lower limb power training in their
6 preparation.

7

8 **Conclusion**

9 The increased Cr during the Etna uphill marathon was related to changes in the mechanics of
10 running such as increases in t_c , Δz and ΔL and decreases in t_a , f , F_{max} , k_{vert} and k_{leg} . In addition,
11 lower Cr was related with better performance, and athletes characterized by the greater P_{max}
12 showed lower increases in Cr during the race. This suggests that specific power training of the
13 lower limbs may lead to better performance in ultra-endurance running competition.

14

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22

23 **DISCLOSURES**

24 No conflicts of interest, financial or otherwise, are declared by the author(s).

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For Peer Review

FIGURE CAPTION

Figure 1: Race time (min) plotted for all subjects as a function of energy cost of running (C_r , $\text{mlO}_2 \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$) measured before (\bullet) and immediately after (\circ) the race.

Figure 2: Contact time (t_c , A), aerial time (t_a , B), maximal vertical ground reaction force (F_{max} , C), downward displacement of centre of mass during contact (Δz , D), vertical stiffness (k_{vert} , E) and leg stiffness (k_{leg} , F) measured before (\bullet) and immediately after the race (\circ) plotted for all subjects as a function of the measured energy cost of running (C_r , $\text{mlO}_2 \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$).

Figure 3: Maximal mechanical power of the lower limbs (P , W) measured before the race plotted for all subjects as a function of changes in energy cost of running caused by the race (ΔC_r , %).

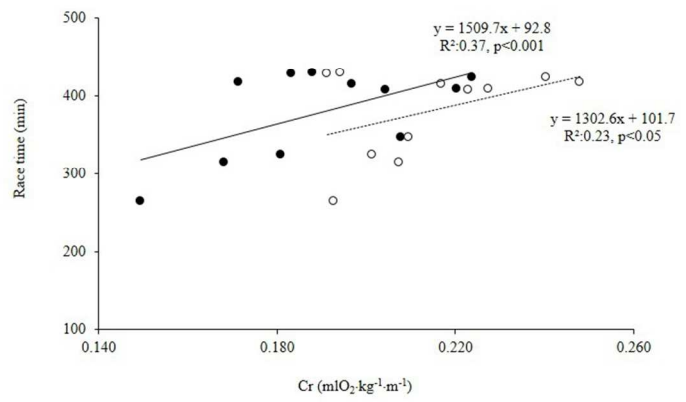
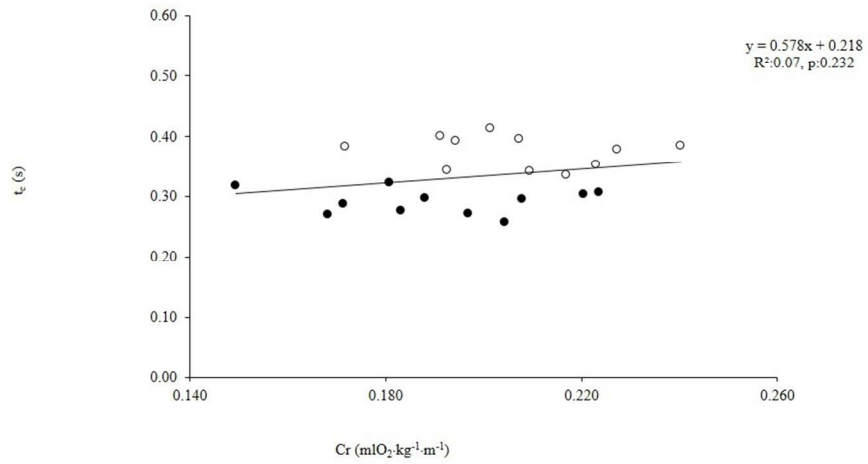


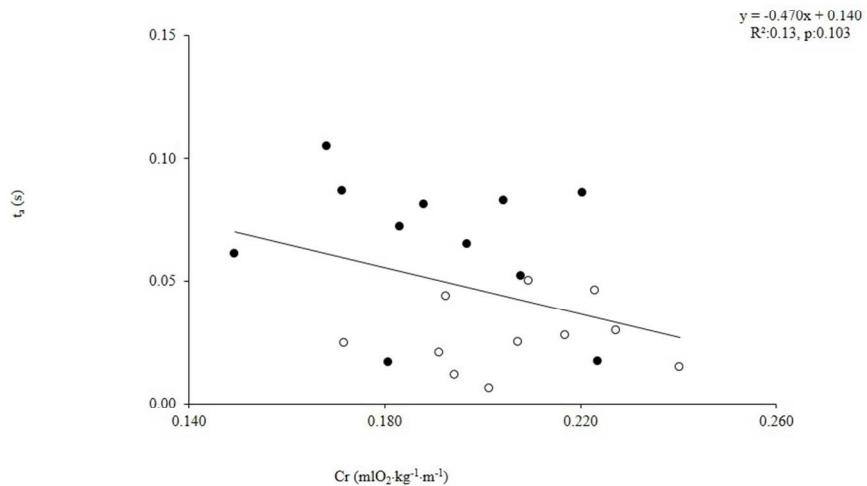
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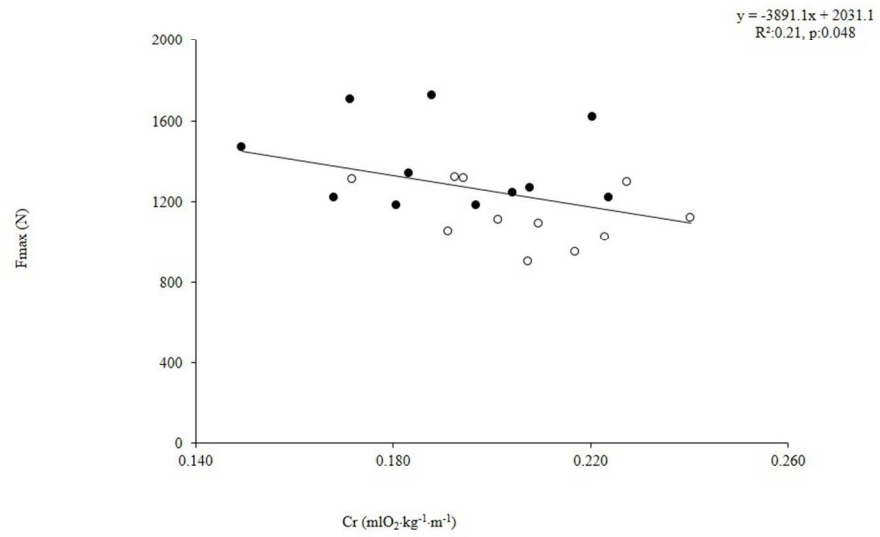
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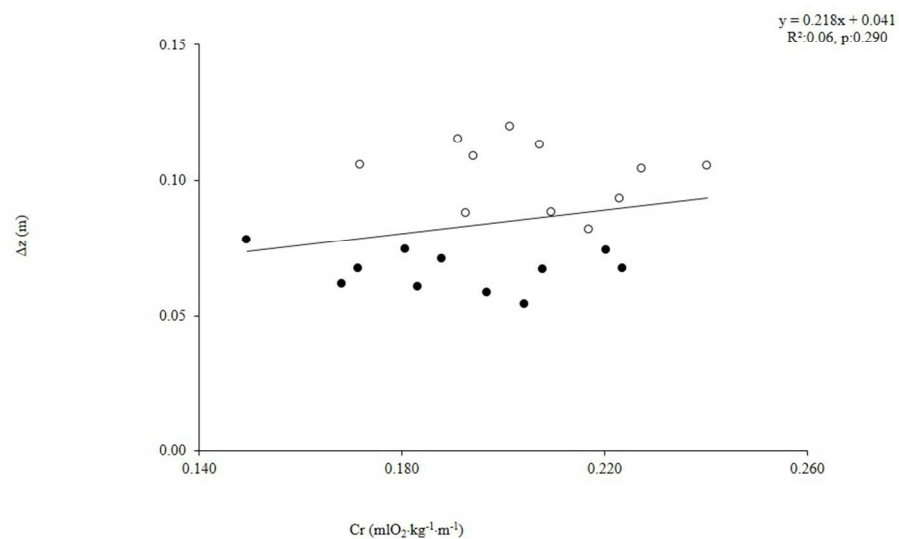
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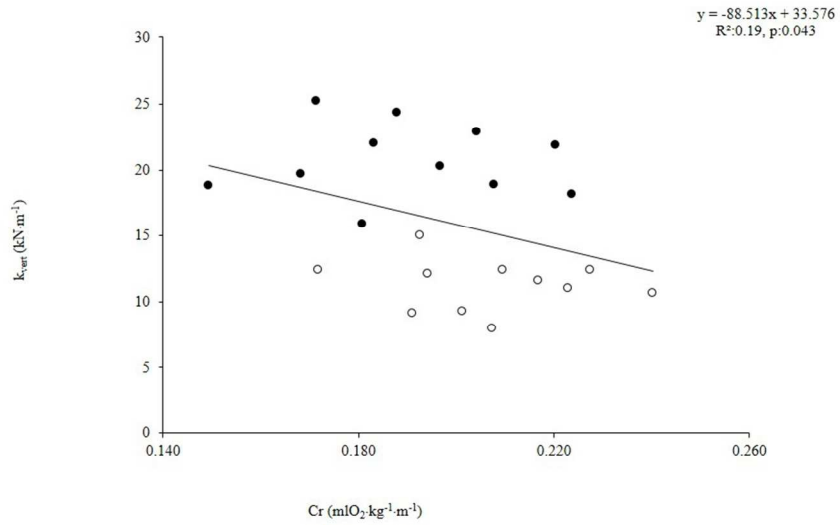
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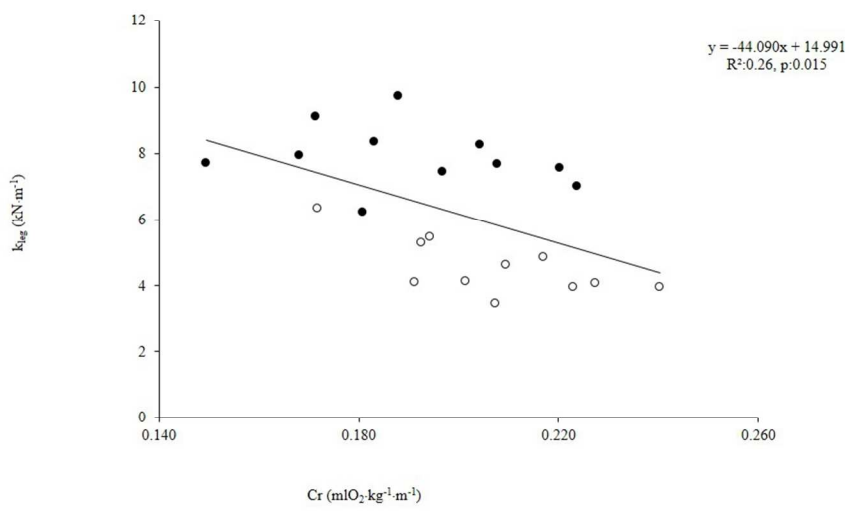
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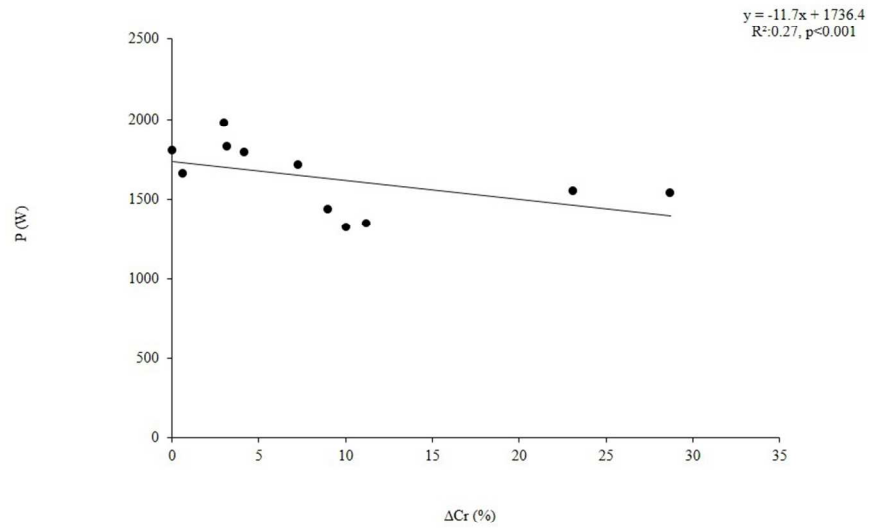
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TABLE 1. Physical characteristics of subjects (n:11) before the race.

Age (year)	43.2 ± 11.0	[27.0 – 59.0]
Body mass (kg)	72.9 ± 10.2	[57.0 – 88.0]
Stature (m)	1.77 ± 0.07	[1.63 – 1.85]
Body mass index (kg·m ⁻²)	23.1 ± 2.4	[20.2 – 27.4]
L (m)	0.89 ± 0.04	[0.81 – 0.94]
V'O ₂ max (ml·min ⁻¹ ·kg ⁻¹)	49.2 ± 8.8	[37.9 – 61.5]
HR _{max} (bpm)	176.8 ± 11.0	[161.0 – 193.0]
Cr (mlO ₂ ·m ⁻¹ ·kg ⁻¹)	0.190 ± 0.023	[0.149 – 0.224]
P _{max} (W)	1628 ± 212	[1319 – 1971]
Race time (hh:mm:ss)	6:14:01±1:04:29	[4:24:12 - 7:09:36]

All values are mean ± standard deviation (SD). Range in square brackets.

L: lower limb length; V'O₂max: maximal oxygen uptake; HR: heart rate; Cr: energy cost of running; P_{max}: maximal mechanical power of the lower limbs.

130 runners started the race, 109 completed it. Of the 11 runners of this study, 4 were classified within the 10th place, 2 between the 30th and 40th, 3 between the 50th and 60th and 2 between the 70th and 80th.

TABLE 2. Body mass, energy cost of running, respiratory exchange ratio and mechanical parameters determined before and immediately after the race.

	Before	After	Changes %	P
BM (kg)	72.9 ± 10.2	68.7 ± 9.8	-5.7	0.001
Cr (mlO ₂ ·m ⁻¹ ·kg ⁻¹)	0.190 ± 0.023	0.207 ± 0.019	+8.7	0.001
RER	0.88 ± 0.06	0.82 ± 0.08	-6.6	0.123
Self-selected running speed (m·s ⁻¹)	2.89 ± 0.17	2.68 ± 0.39	-7.3	0.024
Contact Time (s)	0.291 ± 0.021	0.375 ± 0.027	+28.6	0.001
Aerial time (s)	0.066 ± 0.028	0.027 ± 0.014	-58.6	0.001
Step frequency (step·s ⁻¹)	2.81 ± 0.18	2.49 ± 0.11	-11.3	0.001
F _{max} (N)	1380.0 ± 213.1	1136.4 ± 152.9	-17.6	0.001
Δz (m)	0.067 ± 0.007	0.102 ± 0.013	+52.9	0.001
ΔL (m)	0.175 ± 0.020	0.253 ± 0.034	+44.5	0.001
k _{vert} (kN·m ⁻¹)	20.72 ± 2.81	11.26 ± 1.97	-45.6	0.001
k _{leg} (kN·m ⁻¹)	7.90 ± 0.96	4.56 ± 0.85	-42.3	0.001

All values are mean ± standard deviation (SD).

BM: body mass; Cr: energy cost of running; RER: respiratory exchange ratio; F_{max}: maximal vertical ground reaction force; Δz: downward displacement of centre of mass during contact;

ΔL: displacement of the leg spring; k_{vert}: vertical stiffness; k_{leg}: leg stiffness.

P: Significance by Student paired t-test.

1 **EFFECTS OF AN UPHILL MARATHON ON RUNNING MECHANICS AND**
2 **LOWER LIMB MUSCLES FATIGUE**

3

4 **Submission type:** original investigation

5

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21 **Preferred running head:** Running mechanics and muscle fatigue

22 **Abstract word count:** 249

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24 **Number of figures:** 3

25 **Number of tables:** 4

26

27 **ABSTRACT**

28 **PURPOSE:** To investigate the effects of an uphill-marathon (43 km, 3063 m elevation gain)
29 on running mechanics and neuromuscular fatigue in lower limb muscles.

30 **METHODS:** Maximal mechanical power of lower limbs (MMP), temporal tensiomyography
31 (TMG) parameters and muscle belly displacement (Dm) were determined in the vastus
32 lateralis muscle before and after the competition in eighteen runners (age: 42.8±9.9 yr; body
33 mass: 70.1±7.3 kg; maximal oxygen uptake: 55.5±7.5 mL·kg⁻¹·min⁻¹). Contact (t_c) and aerial
34 (t_a) times, step frequency (f) and running velocity (v) were measured at 3,14,30 km and after
35 the finish line (POST). Peak vertical ground reaction force (F_{max}), vertical displacement of the
36 centre of mass (Δz), leg length change (ΔL), vertical (k_{vert}) and leg (k_{leg}) stiffness were
37 calculated.

38 **RESULTS:** MMP was inversely related with race time (r:-0.56,p:0.016), t_c (r:-0.61,p:0.008),
39 Δz (r:-0.57,p:0.012) and directly related with F_{max} (r:0.59,p:0.010), t_a (r:0.48,p:0.040), k_{vert}
40 (r:0.51,p:0.027). In the fastest sub-group (n:9) the following parameters were lower in POST
41 (p<0.05) than at km 3: t_a (-14.1±17.8%), F_{max} (-6.2±6.4%), k_{vert} (-17.5±17.2%), k_{leg} (-
42 11.4±10.9%). The slowest sub-group (n:9) showed changes (p<0.05) at km 30 and POST in
43 F_{max} (-5.5±4.9% and -5.3±4.1%), t_a (-20.5±16.2% and -21.5±14.4%), t_c (+5.5±7.5% and
44 +3.2±5.2%), k_{vert} (-14.0±12.8% and -11.8±10.0%), k_{leg} (-8.9±11.5 and -11.9±12%). TMG
45 temporal-parameters decreased in all runners (-27.35±18.0%,p<0.001), while Dm increased
46 (+24.0±35.0%,p:0.005), showing lower muscle stiffness and higher muscle sensibility to the
47 electrical stimulus.

48 **CONCLUSIONS:** Greater MMP was related with smaller changes in running biomechanics
49 induced by fatigue. Thus, lower limb power training could improve running performance in
50 uphill-marathons.

51 **Key Words:** kinematics; stiffness; tensiomyography; post-activation potentiation.

52 **INTRODUCTION**

53 The mechanics of running in different conditions^[1-3] have been frequently investigated using
54 the spring mass model (SMM)^[4]. This model consists of a point of mass supported by a single
55 mass-less linear spring, which allows to investigate the leg (k_{leg}) and vertical (k_{vert}) stiffness
56 coefficients associated with leg-spring compression (ΔL) and with the vertical displacement
57 (Δz) of the centre of mass (CoM) at the middle of the stance phase^[3]. In this model, k_{leg} is
58 defined as the ratio between peak vertical ground reaction force (F_{max}) and ΔL , while k_{vert} is
59 the ratio between F_{max} and Δz ^[5].

60 Previous studies^[2,5,6] showed a reduction in F_{max} , Δz , ΔL , and an increment in k_{vert} and step
61 frequency (f) after many hours of prolonged running (mountain ultra-marathon or MUM, 24-h
62 treadmill run, 5-h hilly running) with different behaviour of contact (t_c) and aerial (t_a) time.
63 Morin et al.^[5] hypothesized that these changes in the running pattern could lead to a smoother
64 and safer running style, likely preserving the body structures especially during the braking
65 phase of each step. Moreover, the different changes in t_c and t_a among these studies could be
66 due to the different running conditions (treadmill vs over-ground running; level vs
67 uphill/downhill running). Some authors suggested that treadmill and over-ground running can
68 be considered similar only when the sample size is sufficiently wide, because large individual
69 differences between the two running conditions were found^[7]. In addition, the inclination of
70 the running surface also influences running biomechanics^[8]. Indeed, in uphill running, the
71 peak forces recorded are smaller, f is greater, and the stride length is shorter as compared to
72 level and downhill running^[8]; similarly, the eccentric step phase is reduced. Also, the muscle
73 volume activated in the lower limbs is larger in uphill than in horizontal running. Besides,
74 uphill running requires considerably greater activation of the vastus and soleus and a lesser
75 activation of the rectus femoris, gracilis and semitendinosus compared to horizontal

76 running^[9]. It follows that, as showed by Lazzer et al.^[3], uphill running may lead to different
77 changes in running mechanics than those observed in previous MUM^[2,5,6].

78 Furthermore, neuromuscular fatigue (i.e. an exercise-related decrease in the maximal
79 voluntary force or power of a muscle group^[10]) has been shown to significantly impair the
80 performance of ultra-endurance athletes^[10,11]. This potentially involves processes at all levels
81 of the motor pathway from the brain to skeletal muscle.

82 Muscular fatigue was previously investigated by analysing electromyography together with
83 muscle mechanical output during dynamic and static muscle contractions^[11,12]. Recently, the
84 non-invasive technique of tensiomyography (TMG) has been used to examine the contractile
85 properties of skeletal muscle. Simunic et al.^[13] also suggested that this methodology could be
86 used to evaluate peripheral fatigue; however, few authors have used TMG to study this
87 phenomenon^[14-16].

88 To the best of our knowledge, no study has already analysed running biomechanics and
89 muscular fatigue during and after an uphill race. This type of event is peculiar because it is
90 characterized by lower impact and lower eccentric phase than a classic “flat” marathon or
91 MUM.

92 Therefore, the primary purpose of the present study was to investigate the effects of an
93 extreme uphill running marathon on running mechanics and on SMM. The secondary purpose
94 was to evaluate the effect of race-induced fatigue on muscle contractile properties by TMG.

95 The third aim of this study was to examine whether the changes in running mechanics and
96 TMG parameters due to the race-induced fatigue were different between faster and slower
97 runners.

98 We hypothesized that the changes in SMM induced by the investigated uphill running were
99 different than those brought about by level running or classical MUM; in particular, we
100 expected a decrease in k_{vert} and k_{leg} . Also, we hypothesized that the fastest runners showed

101 smaller changes in running mechanics as compared to the slowest athletes. Finally, we
102 expected different muscle stiffness and sensibility to the electrical stimulus between the two
103 groups.

104

105 **METHODS**

106 **Subjects**

107 Twenty-five healthy Italian male runners were enrolled in this study as participants in the
108 “Supermaratona dell’Etna” (SME), and the 18 athletes who completed the race were
109 considered for data analysis (mean±SD: age= 42.8 ± 9.9 yr, body mass=70.1±7.3 kg, height=
110 1.71±0.05 m, V’O₂max=55.5±7.5 mL·kg⁻¹·min⁻¹, maximal mechanical power (MMP) of the
111 lower limbs=27.6±7.7 W·kg⁻¹, (Table 1)).

112 The experimental protocol was approved by the Ethics Committee of the University of Udine.
113 Before the study began, the purpose and objectives were carefully explained to each subject
114 and written informed consent was obtained from all of them. The participants were recruited
115 among experienced ultra-endurance runners (12.4±8.5 years of training history in running;
116 6.5±3.5 years of ultra-endurance running race experience and 88.4±39.5 km/week of running
117 training) and were asked to fill out a questionnaire on physical exercise activity,
118 demographics, medical history and lifestyle. Subjects who reported any muscular or
119 metabolic diseases or recent physical injury were excluded from the study.

120

121 **Experimental protocol**

122 The race took place in June 2013; the starting time was set at 8:00 AM in Marina di Cottone
123 (Catania, Italy), at sea level, the temperature and relative humidity were 27°C and 22%
124 respectively. The first 30-km of the race to Etna North (1810 AMSL), were on paved road,
125 whereas its final part led to the finish line at 3000 AMSL over an all-trail course. The overall
126 distance was 43km with 3063m of elevation gain, a mean slope of about 7% and with peak

127 values reaching 14% (Figure 1). At the finish line, temperature and relative humidity were
128 16°C and 45% respectively.

129 During the week before the race, participants were asked to come to the laboratory to perform
130 a graded exercise test on a treadmill to evaluate their maximal oxygen uptake ($V'O_2\text{max}$).
131 Athletes were also asked to refrain from any vigorous physical activity during the day
132 preceding the test and during the preliminary testing session that they performed to
133 familiarize with all the equipment. Moreover, the day before the race and immediately after
134 the end of the race, the jumping test^[17] and TMG assessment were performed, and
135 anthropometric characteristics measurements were carried out. Furthermore, running
136 mechanics were evaluated during the race at km 3, 14, 30 and immediately after the athletes
137 reached the finish line (POST). In addition, GPS coordinates were continuously recorded
138 throughout the competition (Garmin Forerunner 305 GPS, Kansas City, USA).

139

140 **Physiological measurements before and after the race**

141 Body mass (BM) and $V'O_2\text{max}$ were assessed the week before the race as described by
142 Lazzer et al.^[18]. The day before and immediately after the race, MMP was assessed during a
143 counter movement jump by means of the Bosco test^[17] (Ergo Jump, Boscosystem, Italy).
144 In addition, the subjects underwent TMG before the race and immediately after (2-4 min)
145 crossing the finish line, using a protocol previously described by Simunic et al.^[13]. From
146 every twitch response, the displacement of muscle belly (Dm), delay time (Td), contraction
147 time ($T_{\text{contraction}}$), sustained contraction time (Ts) and relaxation time (Tr) were calculated. Dm
148 was defined as the peak amplitude in the displacement–time curve of the tensiomyographical
149 twitch response. Td was defined as the time between the electrical stimulus and displacement
150 of the sensor to 10% of Dm, $T_{\text{contraction}}$ was the time from 10% to 90% of Dm reached, Ts was

151 the time period in which muscle response remains greater than 50%, and T_r was the time from
152 90% D_m to decline to one-half of the D_m in the relaxation phase^[13,15].

153

154 **Mechanical measurements during the race**

155 Running mechanics were studied using four digital cameras with a sample frequency of 400
156 Hz (Nikon J1, Japan). The cameras were placed perpendicular to the running direction of
157 athletes at km 3, 14, 30 and immediately after the finish line of the race (POST). The
158 recording zone during the race (km 3, 14 and 30) was selected in order to include at least 15m
159 of flat road (inclination $<1\%$, as measured by means of GPS devices the day before the race).

160 Then, immediately after the race, the athletes were asked to run at a constant self-selected
161 speed, as close as possible to the race speed, for 50 m on a flat compact rock path situated
162 near the finish line. Three attempts were performed, and the one with the running speed
163 closest to that recorded during the race (at the three checkpoints) was used for video analysis.

164 Running speed was measured by means of two photocells placed immediately before and
165 after each video recording zone. Because of the limited space available for placing the
166 camera, only five subsequent steps were analysed in order to measure t_c (s) and t_a (s). Step
167 frequency (f , $\text{step}\cdot\text{s}^{-1}$) was calculated as: $1/(t_a+t_c)$.

168 Given t_c (s), t_a (s), v ($\text{m}\cdot\text{s}^{-1}$), subject's BM (kg), and lower limb length (distance between great
169 trochanter and ground during standing, L in m), spring mass parameters were calculated using
170 the computation method proposed by Morin et al.^[1]. This method, based on modelling of the
171 ground reaction force during the contact phase by a sine function, allows the computation of
172 k_{vert} ($\text{kN}\cdot\text{m}^{-1}$) as the ratio of the F_{max} (N) to the Δz (m) and of k_{leg} ($\text{kN}\cdot\text{m}^{-1}$) as the ratio of F_{max}
173 and the ΔL (m). Moreover, in order to identify the effect of MMP on biomechanical
174 parameters during the race, MMP measured before and after the race was plotted as a function
175 of the biomechanical parameters for all athletes.

176

177 **Statistical analyses**

178 Statistical analyses were performed using PASW Statistic 18 (SPSS Inc., IL, USA) with
179 significance set at $p < 0.05$. All results are expressed as means and standard deviation (SD).
180 Normal distribution of the data was tested using the Kolmogorov-Smirnov test.
181 Median value of the subjects' final ranking was considered to split all subjects into two sub-
182 groups of 9 subjects (the 9 fastest runners and the 9 slowest runners). Changes of speed and
183 mechanical parameters during the race were studied with General Linear Model repeated
184 measures with two factors considering groups (called "G": the 9 fastest runners vs the 9
185 slowest runners) and distance (called "D": 3 km vs 14 km vs 30 km vs POST). As well,
186 changes of BM, maximal mechanical power of the lower limbs and TMG parameters before
187 and after the race were studied with General Linear Model repeated measures with two factors
188 considering groups (called "G": 9 fastest runners vs 9 slowest runners) and Time (called "T":
189 pre vs post). When significant differences were found, a Bonferroni post-hoc test was run to
190 determine the exact location of the difference.

191 The relationships between $\dot{V}O_2\text{max}$ and performance time, MMP and mechanical variables
192 were investigated using Pearson's product-moment correlation coefficient.

193

194 **RESULTS**

195 Race time and physical characteristics of the athletes measured before the race (PRE) are
196 reported in Table 1. Race time of the winner of the SME was 3:50:38, while the average time
197 of the subjects was 5:29:10 \pm 1:01:12 (ranking 1st-101st).

198 An inverse relationship between $\dot{V}O_2\text{max}$ and race time ($r: -0.85$, $p < 0.001$) as well as
199 between MMP-PRE and race time ($r: -0.56$, $p: 0.016$) were observed.

200 When MMP measured before and after the race was plotted as a function of mechanical
201 parameters, inverse relationships between MMP and t_c (Figure 2A) as well as Δz (Figure 2D)
202 were observed. However, direct relationships between MMP and t_a (Figure 2B), F_{max} (Figure
203 2C) as well as k_{vert} (Figure 2E) were observed. No significant relationships between MMP
204 and f , ΔL and k_{leg} were found.

205 A further analysis was focused on the comparison between two sub-groups of athletes ($n=9$),
206 who were divided according to the final ranking. The 9 fastest runners were younger (-21.5%
207 in age, $p:0.024$), with lower BM (-12.2%, $p:0.004$) and BMI (-11.7%, $p:0.002$) and higher
208 $V'O_2max$ (+17.5%, $p:0.007$) and MMP (+29.5%, $p:0.047$) as compared to the 9 slowest
209 runners (Table 1).

211 *Mechanical parameters*

212 When the results recorded from all 18 athletes were averaged (Table 2), there was a
213 decrement at km 14 and 30 in speed ($-2.4\pm 3.4\%$ and $-4.8\pm 7.2\%$; $p<0.01$), at km 30 and POST
214 in t_a ($-14.6\pm 18.2\%$ and $-18.0\pm 16.4\%$ respectively, $p<0.01$), F_{max} ($-4.2\pm 6.4\%$ and $-5.6\pm 5.2\%$
215 respectively, $p<0.001$) and k_{vert} ($-12.1\pm 15.0\%$ and $-15.0\pm 14.0\%$ respectively, $p<0.01$).
216 Moreover, k_{leg} decreased only POST ($-11.7\pm 11.2\%$, $p<0.001$). Conversely, at km 30 and
217 POST, an increment in Δz ($+7.5\pm 11.8\%$ and $7.5\pm 17.6\%$ respectively, $p<0.05$) and in t_c
218 ($+4.8\pm 7.8\%$ and $+5.2\pm 9.6\%$ respectively, $p<0.05$) was observed.

219 When the two sub-groups were analysed separately, the fastest runners did not show any
220 significant change in v and mechanical parameters throughout the race (Table 3). On the
221 contrary, immediately after the race (POST), they showed lower t_a ($-14.1\pm 17.8\%$, $p<0.05$),
222 F_{max} ($-6.2\pm 6.4\%$, $p<0.05$), k_{vert} ($-17.5\pm 17.2\%$, $p<0.05$), k_{leg} ($-11.4\pm 10.9\%$, $p<0.05$) and MMP
223 ($-23.6\pm 26.2\%$, $p<0.05$, Table 4). The slowest runners showed a decrease in F_{max} at km 30 and
224 POST ($-5.5\pm 4.9\%$ and $-5.3\pm 4.1\%$; $p<0.05$), a t_a decrease at km 30 and POST ($-20.5\pm 16.2\%$

225 and $-21.5 \pm 14.4\%$, respectively, $p < 0.005$) and t_c increase at km 30 and POST ($+5.5 \pm 7.5\%$ and
226 $+3.2 \pm 5.2\%$, respectively, $p < 0.05$). Consequently, k_{vert} and k_{leg} decreased at km 30 and POST
227 ($-14.0 \pm 12.8\%$ and $-11.8 \pm 10.0\%$; -8.9 ± 11.5 and $-11.9 \pm 12\%$, respectively; $p < 0.05$) (Table 3).
228 In this group, MMP decreased by $-23.2 \pm 15.3\%$ after the race ($p < 0.005$, Table 4). Moreover,
229 MMP was higher in the fastest runners before and after the race as compared to the slowest
230 ones ($+28.9 \pm 0.4\%$, $p < 0.05$, Table 4). The gait parameters were not compared between fastest
231 and slowest athletes because of the significant difference in speed at every checkpoint
232 ($29.9 \pm 5.3\%$, $p < 0.001$).

233

234 *TMG parameters*

235 Figure 3 shows the TMG responses averaged among all runners that were carried out before
236 (solid line) and immediately after (dashed line) the race. After the race, a significant decrease
237 ($p < 0.001$) in $T_{\text{contraction}}$ ($-12.8 \pm 9.7\%$), T_s ($-39.3 \pm 31.6\%$), T_r ($-46.2 \pm 33.5\%$) and T_d ($-$
238 $11.1 \pm 9.5\%$) was observed, together with an increase of D_m ($+24.0 \pm 35.0\%$, $p = 0.005$). When
239 these parameters were compared between the fastest and slowest group, no significant
240 differences were found (Table 4).

241

242 **DISCUSSION**

243 The main results of the present study showed that 1) race time was inversely related with
244 $\dot{V}O_2\text{max}$ and MMP, 2) running mechanics did not change throughout the race in the fastest
245 runners, while it changed from the 30th km onward in the slowest runners. However, in both
246 groups running mechanics before the race (PRE) was significantly different than immediately
247 after the race (POST). 3) TMG time-parameters ($T_{\text{contraction}}$, T_s , T_r , and T_d) decreased and D_m
248 increased after the race in both groups.

249

250 As previously observed by several authors, strong correlations have been shown between
251 $\dot{V}O_2\text{max}$ and running performance in subjects with different running levels^[18]. However,
252 when groups of athletes with a relatively narrow range of $\dot{V}O_2\text{max}$ are studied, $\dot{V}O_2\text{max}$
253 becomes a less sensitive predictor of performance, while its fraction that can be sustained
254 throughout the race and the energy cost of running (Cr) become more and more important for
255 predicting performance in distance running^[18]. Particularly, some authors^[18], showed that
256 lower values of Cr in trained runners were related with higher values of MMP, k_{vert} and low
257 foot-print index (i.e. the medio-lateral displacement of the foot during the whole stance
258 phase), supporting previous studies that underlined the role of muscle-tendon complex
259 stiffness in storing and releasing elastic energy^[19].

260 Indeed, in the present study, the athletes with higher values of MMP presented lower t_c and
261 Δz and higher t_a , F_{max} and k_{vert} : these are all factors that could promote higher running
262 velocity^[20] and lower energy expenditure because of the lower oscillation of the centre of
263 mass^[18,19].

264 In contrast to previous studies^[2,6], no changes in f and an increase in Δz have been observed.
265 This suggests that the lower eccentric phase that is involved in uphill races like SME
266 promoted peculiar adaptations so that the characteristics of the spring mass system rather than
267 the running speed were modulated throughout the race. Indeed, during an uphill running race
268 it may not be necessary to adopt a safer running style because of the peculiarity of the course
269 profile. Furthermore, the increase in Δz observed in the present study could be a consequence
270 of the decrease in k_{vert} and F_{max} as observed previously in exhaustive but much shorter running
271 efforts^[20-23], in which spring mass characteristics changed toward a longer contact time^[22-24],
272 higher Δz and lower k_{vert} ^[21].

273 Furthermore, the fastest runners changed their running pattern only at the last checkpoint,
274 immediately after they crossed the finish line. We can speculate that these athletes changed

275 their running pattern between km 30 and km 43, in the non-paved leg of the race. This part of
276 the race, where the surface stiffness was different compared to the first part, could affect the
277 running mechanics even in the fastest and most trained runners, although previous studies
278 have shown that runners adjust their stiffness to maintain consistent support mechanics across
279 different surfaces^[25]. Conversely, the slowest runners changed their spring mass parameters
280 between km 14 and km 30. Interestingly, the transit at km 30 for the slowest athletes occurred
281 after about 4 hours from the race start, while the fastest athletes reached this checkpoint in
282 about 3 hours. Our hypothesis, in accordance with the study of Morin et al.^[2], is that the
283 spring mass parameters change after a certain time of exercise performed rather than after a
284 certain amount of distance covered.

285 Neuromuscular alterations due to fatigue^[2] and muscle damage which occur during an ultra-
286 endurance event could affect running mechanics^[5]. Millet et al.^[12] demonstrated that central
287 fatigue plays the main role in decreasing force after an ultra-marathon. As well, alterations of
288 neuromuscular propagation, excitation-contraction (E-C) coupling failure and modifications
289 of the contractile apparatus may be involved in decreasing force^[26]. Hunter et al.^[16] used the
290 TMG to assess peripheral fatigue 24 hours after exercise-induced muscle damage and they
291 observed a decrease in Dm and an increase in $T_{\text{contraction}}$, by -31% and +21% respectively.
292 However, a different behaviour of TMG-parameters during various fatigue protocols has been
293 shown by other authors^[14,15] even if, to our knowledge, the TMG has been used only once to
294 evaluate muscular fatigue during an ultra-endurance event. After an Ironman triathlon,
295 authors found muscle specific decreased Td in *rectus femoris* and increased $T_{\text{contraction}}$, Tr and
296 Dm in *biceps femoris*^[14]. In contrast with our hypothesis, in the present study, no differences
297 in TMG parameters between the two sub-groups of athletes before and after the race were
298 found. When all 18 athletes were analysed together, Dm increased by 24% while the other
299 investigated parameters decreased, suggesting that the vastus lateralis muscle was less stiff

300 and reacted faster to the electrical stimulus. Our results are in agreement with Millet et al.^[12]
301 who stimulated electrically the femoral nerve before and after a 65-km ultramarathon race,
302 showing greater peak twitch tension and shorter contraction time after the race. The authors
303 hypothesized that these changes could be due to the potentiation of the twitch force after
304 fatigue^[12]. In fact, a shift to the left of both torque^[27] curve and TMG curve, similar to that
305 observed in the present study after the race (Figure 3), is analogous to the shift usually
306 observed in post-activation potentiation (PAP). PAP is commonly detected after short burst of
307 strength or power exercise^[28] and it was also seen in endurance athletes after a maximal
308 isometric contractions^[27]. Therefore, we suggest that enhanced PAP may counteract fatigue
309 during endurance exercise which affect the behaviour of the muscle fibres.

310

311 *Limits of the study*

312 In this study, one issue was related to the running speed, which was self-selected both
313 throughout the race and after its conclusion. However, the difference in speed was -2.4%
314 between the second and the first checkpoint, -4.9% between the third and the first checkpoint
315 and -4.1% between the last and the first checkpoint. As previously observed^[5], these
316 differences can be considered acceptable when comparing gait parameters by video analysis.
317 In order to minimize this issue for the POST time point, athletes performed three running
318 attempts, and the one with the speed closest to the average speed value recorded during the
319 race (at km 3, 14 and 30) was taken into account for further analysis. Also in this case, the
320 speed difference was negligible (-4.1%).

321 A second limit of this study was related to the number of subsequent steps that were analysed
322 in order to calculate the SMM parameters. We considered 5 subsequent steps, the maximum
323 allowed by the camera placement with respect to the environment characteristics. However,

324 other studies analysed running mechanics taking into consideration a similar number of
325 consecutive steps (either 5-8^[5] or 10 steps^[3,18]), thus supporting our approach.
326 Finally, muscle contractile properties can be affected by muscle temperature ^[29]. In order to
327 minimize this issue, in the present study, prior the beginning of the race, athletes underwent
328 TMG measurements after a 10-minute warm-up. This countermeasure conceivably increased
329 intramuscular temperature to values similar to the ones present after the end of the race, seen
330 as this physiological variable shows steep increments in the first 10 minutes, reaching its
331 plateau or values comparable to the ones recorded after prolonged exercise ^[30].

332

333 PRACTICAL APPLICATIONS

334 The present study shows that greater values of MMP are related to smaller changes in running
335 biomechanics induced by fatigue. Thus, lower limb power training could be important for
336 long-distance uphill running performance. This suggests that coaches and athletes should
337 consider the integration of specific lower limb power training to their training programs in
338 order to enhance long-distance uphill running performance.

339

340 CONCLUSIONS

341 An inverse relationship between race time and $\dot{V}O_2\text{max}$ as well as MMP was found. Higher
342 MMP was related with higher F_{max} , t_a and k_{vert} as well as lower t_c and Δz : all these factors
343 could conceivably promote higher running velocity. These findings suggest that lower limbs'
344 muscle power plays an important role in determining the performance of uphill long-distance
345 runners. Future interventional studies are required to investigate whether lower limb power
346 training can improve running performance in uphill long-distance competitions. TMG
347 analysis showed a decrement in muscle stiffness and higher sensibility of the muscle to the
348 electrical stimulus, suggesting that the potentiation of fast twitch fibres and the fatigue of
349 slow twitch fibres are two parallel mechanisms involved in this type of race.

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357

358 **DISCLOSURES**

359 No conflicts of interest, financial or otherwise, are declared by the author(s).

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FIGURE CAPTIONS

Figure 1: Race profile of SME obtained from the GPS device. Black arrows indicate where the videos were taken (km 3-14-30 and POST).

Figure 2: Maximal mechanical power (MMP) plotted for all subjects as a function of contact time (t_c , A), aerial time (t_a , B), maximal vertical ground reaction force (F_{max} , C), downward displacement of centre of mass during contact (Δz , D) and vertical stiffness (k_{vert} , E) measured before (\bullet) and immediately after the race (\circ).

Figure 3. Muscle response averaged among all runners to an electric stimulus obtained using tensiomyography on the vastus lateralis muscle, measured before (solid line) and immediately after the race (dashed line).

TABLE 1. Physical characteristics of subjects measured before the race in all athletes and in the first and last nine runners of the group.

	All runners		9 fastest runners	9 slowest runners	P
Age (years)	42.8 ± 9.9	[24.0 - 60.0]	37.7 ± 8.4	48.0 ± 8.8	0.024
Body mass (kg)	70.1 ± 7.3	[60.0 - 83.0]	65.5 ± 5.7	74.6 ± 5.8	0.004
Stature (m)	1.72 ± 0.05	[1.65 - 1.84]	1.72 ± 0.05	1.73 ± 0.04	0.720
Body mass index (kg·m ⁻²)	23.5 ± 2.2	[20.1 - 28.3]	22.0 ± 1.2	24.9 ± 2.1	0.002
L (m)	0.91 ± 0.05	[0.82 - 1.00]	0.89 ± 0.04	0.93 ± 0.05	0.064
V'O ₂ max (mL·kg ⁻¹ ·min ⁻¹)	55.5 ± 7.5	[40.4 - 71.8]	59.9 ± 7.3	51.0 ± 4.6	0.007
MMP (W·kg ⁻¹)	27.6 ± 7.7	[15.8 - 45.8]	31.2 ± 8.2	24.1 ± 5.5	0.047
Race time (hh:mm:ss)	05:29:10 ± 01:01:12	[03:50:38 - 07:16:28]	04:38:13 ± 00:35:21	06:20:07 ± 00:29:30	0.001

All values are mean ± standard deviation (SD). Range in square brackets.

L: lower limb length; V'O₂max: maximal oxygen uptake; MMP: maximal mechanical power of the lower limbs;

p: Significance by ANOVA test (fastest 9 runners vs slowest 9 runners).

TABLE 2. Mechanical parameters determined at km 3, 14, 30 and immediately after the race (POST) in all subjects (N:18)

	All subjects											
	3km			14km			30km			POST		
v (m/s)	3.69	±	0.62	3.60*	±	0.61	3.51*	±	0.68	3.54	±	0.72
tc (s)	0.251	±	0.030	0.252	±	0.031	0.263*	±	0.034	0.265*	±	0.030
ta (s)	0.089	±	0.023	0.086	±	0.021	0.076*	±	0.027	0.073*	±	0.025
f (Hz)	2.96	±	0.15	2.96	±	0.16	2.96	±	0.16	2.97	±	0.24
Fmax (BM)	2.14	±	0.21	2.13	±	0.20	2.05*	±	0.22	2.02*	±	0.19
Δz (m)	0.053	±	0.010	0.053	±	0.010	0.057*	±	0.011	0.057*	±	0.010
ΔL (m)	0.178	±	0.029	0.173	±	0.027	0.181	±	0.033	0.187	±	0.037
k_{vert} (kN·m ⁻¹)	28.85	±	6.77	28.13	±	6.87	25.37*	±	6.85	24.45*	±	6.34
k_{leg} (kN·m ⁻¹)	8.48	±	1.73	8.53	±	1.55	7.86	±	1.93	7.46*	±	1.87

All values are mean \pm standard deviation (SD).

v: speed; tc: contact time; ta: aerial time; f: step frequency; F_{max} : maximal vertical ground reaction force; BM: body mass; Δz : downward displacement of center of mass during contact; ΔL : displacement of the leg spring; k_{vert} : vertical stiffness; k_{leg} : leg stiffness.

*p<0.05 compared to the first checkpoint

TABLE 3. Mechanical parameters determined at km 3, 14, 30 and immediately after the race (POST) in the 9 fastest and 9 slowest runners.

(Continue)

	9 fastest runners											
	3km			14km			30km			POST		
v ($\text{m}\cdot\text{s}^{-1}$)	4.19	\pm	0.40	4.08	\pm	0.43	4.01	\pm	0.56	3.90	\pm	0.77
tc (s)	0.229	\pm	0.026	0.230	\pm	0.028	0.240	\pm	0.031	0.248	\pm	0.034
ta (s)	0.099	\pm	0.025	0.100	\pm	0.019	0.091	\pm	0.026	0.085	\pm	0.026
f (Hz)	3.04	\pm	0.09	3.03	\pm	0.12	3.03	\pm	0.08	3.02	\pm	0.27
Fmax (BM)	2.27	\pm	0.22	2.27	\pm	0.19	2.19	\pm	0.23	2.13	\pm	0.21
Δz (m)	0.046	\pm	0.007	0.046	\pm	0.009	0.049	\pm	0.009	0.052	\pm	0.012
ΔL (m)	0.186	\pm	0.022	0.179	\pm	0.017	0.192	\pm	0.037	0.190	\pm	0.020
k_{vert} ($\text{kN}\cdot\text{m}^{-1}$)	32.71	\pm	7.19	32.27	\pm	7.37	29.25	\pm	7.56	26.98	\pm	8.15
k_{leg} ($\text{kN}\cdot\text{m}^{-1}$)	7.97	\pm	1.65	8.16	\pm	1.38	7.53	\pm	2.37	7.05	\pm	1.52

(Continue)

	9 slowest runners										P				
	3km			14km			30km			POST		Group	Distance	G x D	
	3.20	\pm	0.32	3.11	\pm	0.29	2.99	\pm	0.25	3.18	\pm	0.48	0.001	0.121	0.844
	0.272	\pm	0.017	0.275	\pm	0.012	0.287	\pm	0.015	0.281	\pm	0.010	0.001	0.001	0.653
	0.078	\pm	0.015	0.073	\pm	0.014	0.062	\pm	0.018	0.061	\pm	0.018	0.011	0.005	0.596
	2.87	\pm	0.15	2.89	\pm	0.18	2.88	\pm	0.18	2.93	\pm	0.19	0.098	0.970	0.782
	2.02	\pm	0.10	1.99	\pm	0.07	1.91	\pm	0.10	1.91	\pm	0.10	0.003	0.048	0.369
	0.060	\pm	0.006	0.060	\pm	0.005	0.064	\pm	0.006	0.062	\pm	0.005	0.002	0.004	0.405
	0.170	\pm	0.034	0.167	\pm	0.035	0.171	\pm	0.027	0.182	\pm	0.049	0.271	0.323	0.441
	24.99	\pm	3.50	23.99	\pm	2.72	21.48	\pm	2.92	22.05	\pm	2.31	0.007	0.003	0.740
	8.98	\pm	1.74	8.89	\pm	1.70	8.19	\pm	1.42	7.92	\pm	2.17	0.182	0.008	0.916

All values are mean \pm standard deviation (SD). v : speed; tc: contact time; ta: aerial time; f : step frequency; F_{max} : maximal vertical ground reaction force; BM: body mass; Δz : downward displacement of centre of mass during contact; ΔL : displacement of the leg spring; k_{vert} : vertical stiffness; k_{leg} : leg stiffness.

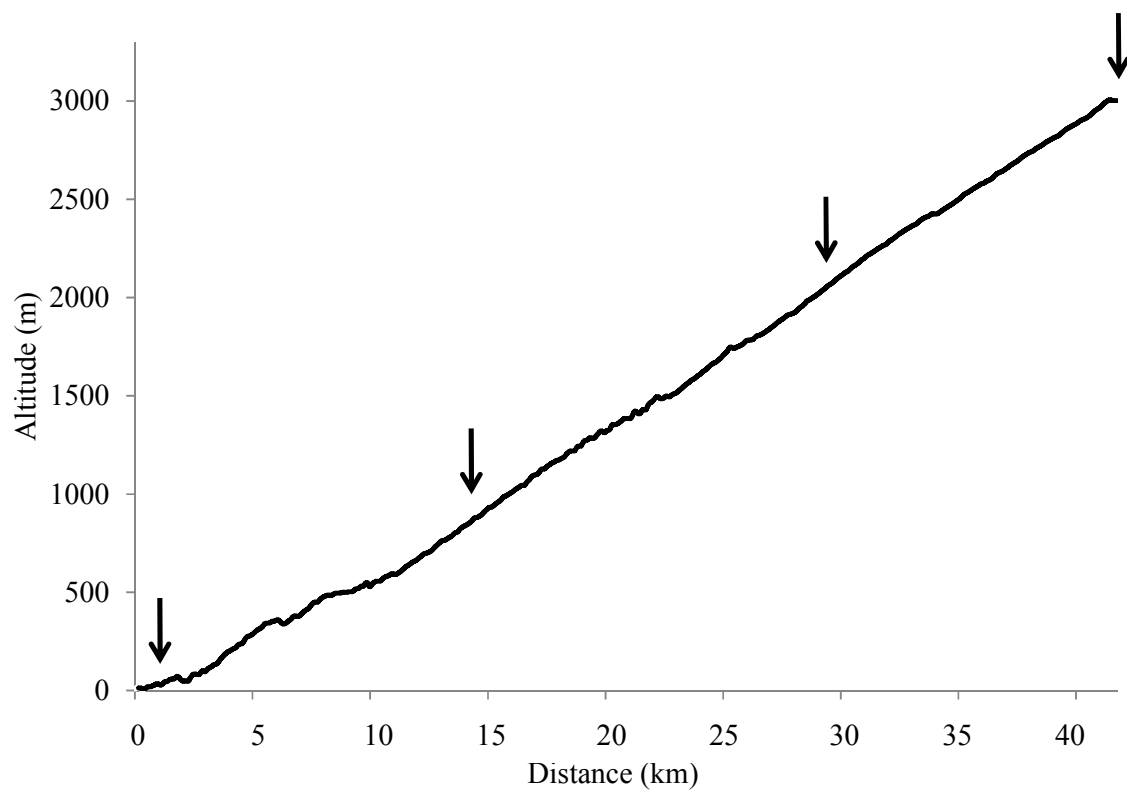
P: significance by GLM Repeated Measures with two factors of the main effects of Group (G), Distance (D) and Interaction (G x D).

TABLE 4. Body mass, maximal mechanical power (MMP) of the lower limbs and tensiomyographic parameters in the *vastus lateralis* muscle, measured before and immediately after the race in the 9 fastest and 9 slowest runners of the group.

	9 fastest runners						9 slowest runners						p		
	Before			After			Before			After			Group	Time	GxT
Body mass (kg)	65.6	±	5.7	63.2	±	6.1	74.8	±	5.8	72.3	±	5.8	0.004	0.001	0.001
MMP ($W \cdot kg^{-1}$)	31.2	±	8.2	23.8	±	9.3	24.1	±	5.5	18.5	±	4.2	0.048	0.008	0.379
$T_{\text{contraction}}$ (ms)	25.8	±	5.4	22.0	±	3.5	25.3	±	4.1	22.6	±	2.4	0.972	0.004	0.382
Ts (ms)	139.8	±	60.0	93.8	±	69.1	134.2	±	63.2	72.6	±	47.9	0.611	0.012	0.447
Tr (ms)	92.3	±	45.4	50.2	±	45.8	89.6	±	45.6	47.6	±	46.5	0.883	0.007	0.995
Td (ms)	23.9	±	1.9	21.4	±	2.1	25.3	±	3.9	22.3	±	1.9	0.172	0.003	0.697
Dm (mm)	6.6	±	1.7	8.1	±	3.0	6.2	±	2.3	7.9	±	2.8	0.785	0.010	0.874

All values are mean \pm standard deviation (SD). $T_{\text{contraction}}$: contraction time; Ts: sustain time; Tr: relaxation time; Td: delay time; Dm: maximal radial displacement; p: Significance by GLM Repeated Measures with two factors of the main effects of Group (G), Time (T) and Interaction (G x T).

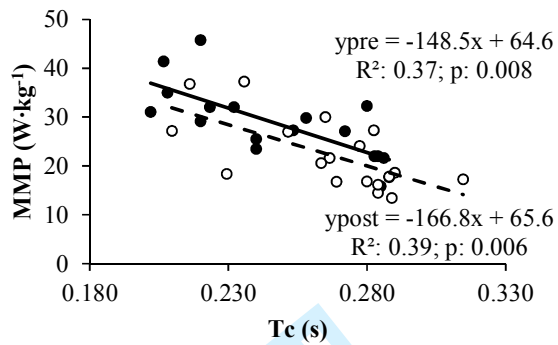
FIGURE 1



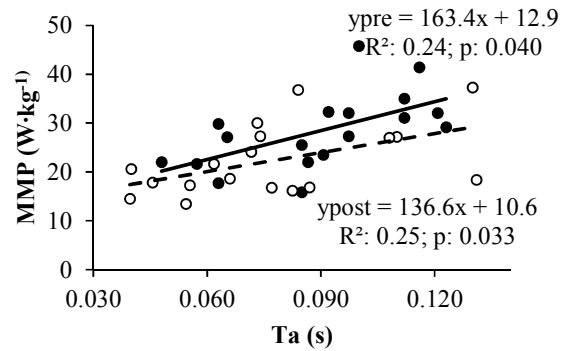
Review

FIGURE 2

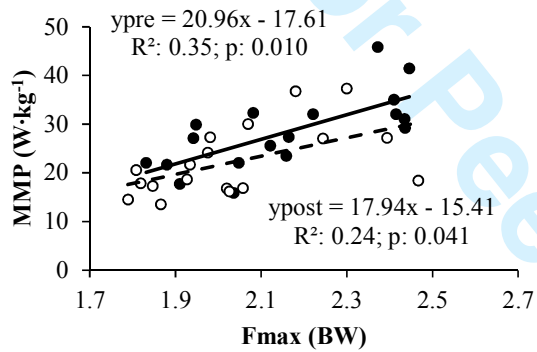
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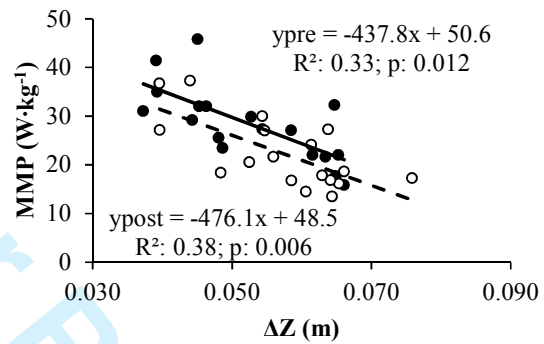
B.



C.



D.



E.

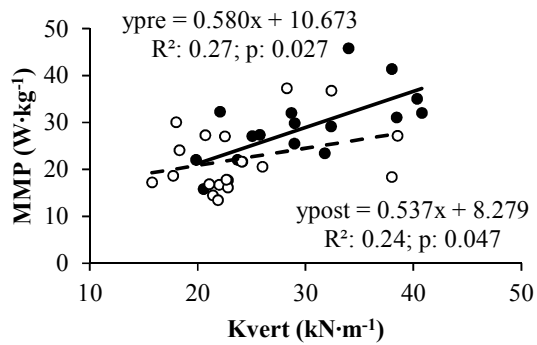
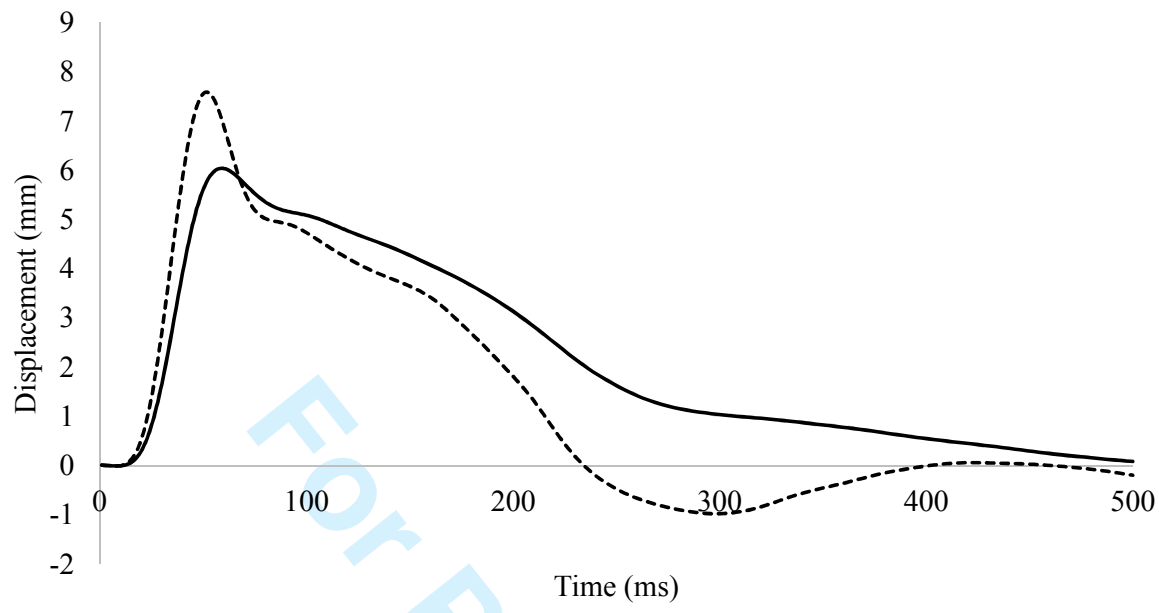


FIGURE 3



For Peer Review

1 Energetics of vertical kilometer foot races; is steeper cheaper?

2

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4

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13 RUNNING HEAD: energetics of uphill running

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28 A.L.R.O. and R.K. interpreted the results. N.G. and A.L.R.O. prepared the figures and

29 drafted the manuscript. N.G., A.L.R.O., K.H. and R.K. all edited and revised the

30 manuscript. N.G., A.L.R.O., K.H. and R.K. all approved the final version of the manuscript.

31 ABSTRACT

32 Vertical kilometer foot races consist of a 1,000 m elevation gain in less than 5,000 m of
33 overall distance and the inclines of the fastest courses are $\sim 30^\circ$. Previous uphill
34 locomotion studies have focused on much shallower angles. We aimed to quantify the
35 metabolic costs of walking and running on very steep angles and to biomechanically
36 distinguish walking from running. Fifteen runners (10 M, 5 F, 32.9 ± 7.5 years, 1.75 ± 0.09 m,
37 64.3 ± 9.1 kg) walked and ran for 5 minutes at 7 different angles (9.4° , 15.8° , 20.4° , 24.8° ,
38 30.0° , 35.0° and 39.2°) all at a fixed vertical velocity (0.35 m/s). We measured the
39 metabolic rates and calculated the vertical costs of walking ($C_{w_{\text{vert}}}$) and running ($C_{r_{\text{vert}}}$).
40 Using video analysis, we determined stride frequency, stride length and duty factor
41 (fraction of stride that each foot is in ground contact). At all angles other than 9.4° , $C_{w_{\text{vert}}}$
42 was cheaper than $C_{r_{\text{vert}}}$ (average $-8.45\% \pm 1.05\%$; $p < 0.001$). Further, broad minima for both
43 $C_{w_{\text{vert}}}$ and $C_{r_{\text{vert}}}$ existed between 20.4° and 35° (average $C_{w_{\text{vert}}}$ 44.17 ± 0.41 $\text{J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$ and
44 average $C_{r_{\text{vert}}}$ 48.46 ± 0.35 $\text{J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$). At all angles and speeds tested, both walking and
45 running involved having at least one foot on the ground at all times. But, in walking, stride
46 frequency and stride length were $\sim 28\%$ slower and longer, respectively than in running. In
47 conclusion, we found that there is a range of angles for which energy expenditure is
48 minimized. At the vertical velocity tested, on inclines steeper than 15.8° , athletes can
49 reduce their energy expenditure by walking rather than running.

50

51 **Keywords:** walking, running, uphill, cost of transport

52 INTRODUCTION

53 In vertical kilometer foot races (VK), athletes complete a course with 1,000 m vertical
54 elevation increase in less than 5,000 m of total race length (International Skyrunning
55 Federation rules <http://www.skyrunning.com>). Terrain, slope and length vary between
56 racecourses. To date, the world record for men in the VK is 29 minutes and 42 seconds,
57 set on a course with a length of 1,920 m, an average inclination of 27.5° (Km vertical de
58 Fully, Switzerland). That equates to an average vertical velocity of ~0.56 m/s and an
59 average velocity parallel to the ground of 1.21 m/s. A VK course with only a slight incline
60 would require an unreasonably fast parallel velocity. For instance, a racecourse with an
61 incline of only 1° would require the impossible running speed of 31.84 m/s to rise 1,000 m
62 in 30 minutes. Conversely, a course with a gradient of 40° would require a speed of only
63 1.03 m/s to gain 1,000 m in 30 minutes. But, if the course is too steep, the rock-climbing
64 techniques required would likely be slower than walking/running at more moderate slopes.
65 Analysis of the best performances in different VK races suggests that there may be an
66 optimal angle for achieving the best time (Figure 1). Since there are no VK races with an
67 average incline steeper than 28.9° (La Verticale du Grand Serre, France), it is unknown if
68 the optimal gradient is actually steeper.

69

70 Another factor to consider is that in VK races, some athletes walk, some run and some
71 alternate gaits. It is not clear which gait or combination is optimal. On level ground or
72 treadmills, at matched speeds slower than ~2.0 m/s, walking requires less metabolic
73 energy than running (3, 15, 17, 25). This is generally attributed to the more effective
74 inverted pendulum-like exchange of mechanical energy at slower walking speeds and the
75 superior elastic energy storage and recovery of running at faster speeds (6). However, on
76 uphill grades both of those mechanisms are disabled (8, 24). On the level (17) as well as
77 moderate inclines and declines (18, 19) the preferred walk-run transition speed occurs
78 near but not exactly at the metabolically optimal transition speed. As speed is increased,
79 people typically first adopt a running gait at a speed slightly slower than the metabolic
80 crossover point.

81

82 The metabolic cost of uphill walking and running has long been of interest to exercise
83 physiologists (3, 14, 15, 18) but almost all studies have examined uphill walking or running
84 on angles less than 9°. One highly relevant exception is the innovative study by Minetti et
85 al. (21). They measured the metabolic cost ($\text{J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$) of walking (C_w) and running (C_r)

86 on a range of slopes up to 24.2°. Note, for C_w and C_r , the calculated distance is parallel to
87 the surface or treadmill. They concluded that at a given treadmill belt speed, C_w and C_r
88 are directly proportional to the slope above +15% (8.5°) and that C_w and C_r converge at
89 steeper angles. Minetti et al. (21) also defined the vertical costs of walking ($C_{w_{vert}}$) and
90 running ($C_{r_{vert}}$), as the energy expended to ascend one meter vertically. $C_{w_{vert}}$ and $C_{r_{vert}}$
91 both decreased at steeper angles reaching minimum values at slopes ranging from 20%
92 (11.3°) to 40% (21.8°). However, we are reluctant to extrapolate from the data of Minetti et
93 al. to the steeper slopes at which VK races are often contested. Further, VK competitors
94 often alternate between walking and running at the same speed and Minetti et al. did not
95 directly compare the energetics of the two gaits at matched speeds. Finally, it is not clear if
96 the traditional biomechanical distinction between walking and running on level ground (i.e.
97 in running, the center of mass trajectory reaches its lowest point at mid-stance and there is
98 an aerial phase when no feet are in contact with the ground) applies on very steep slopes.
99 Previous investigators have used the terms “Groucho running” (16) and “grounded
100 running” (23) to describe a bouncing gait that does not involve an aerial phase.

101

102 To the best of our knowledge, there are no prior scientific studies of human walking or
103 running at the steep angles that are encountered in the fastest VK races. Minetti et al. (20)
104 analyzed stair running races but such “skyscraper races” are much shorter duration than
105 VK (from 50 s to about 14 min compared with ~30 min) and they did not measure the
106 metabolic cost. Intriguingly, Kay’s mathematical analysis of uphill mountain running races
107 (12) concluded that if an optimum gradient for ascent exists, it is steeper than the range of
108 gradients studied so far.

109

110 The primary purpose of this study was to quantify the metabolic costs of walking and
111 running across a wide range of inclines up to and beyond those used in VK races. We
112 aimed to determine if walking or running is more economical and if there are energetically
113 optimal angles for the two gaits. Specifically, we compared walking and running at a fixed
114 vertical velocity (0.35 m/s) at angles ranging from ~10 to ~40°. Based on the findings of
115 Minetti et al. (21), and because the treadmill belt speeds we studied are < 2.0 m/s, we
116 hypothesized that: 1. walking would require less metabolic energy than running. We further
117 hypothesized that: 2. for both walking and running, there would be distinct intermediate
118 angles (~30°) that minimize the energetic cost of ascending at a fixed vertical velocity.

119

120 Our secondary purpose was to distinguish the biomechanics of walking vs. running on
121 steep inclines. We hypothesized that: 3. at steep angles and slow treadmill belt speeds,
122 running would not involve an aerial phase. However, a greater stride frequency during
123 running would distinguish it from walking.

124

125 **MATERIALS AND METHODS**

126 *Subjects.* Fifteen healthy, competitive mountain runners (10 males, 5 females, 32.9 ± 7.5
127 years, 1.75 ± 0.09 m, 64.3 ± 9.1 kg) volunteered and provided informed consent as per the
128 University of Colorado Institutional Review Board.

129

130 *Experimental design.*

131 We modified a custom treadmill so that it was inclinable from 0 to 45° (Figure 2). To
132 provide adequate traction, we adhered a wide swath of skateboard grip tape (i.e.
133 sandpaper) to the treadmill belt (Vicious Tape, Vancouver, BC Canada). To protect the
134 electronic motor controller, we mounted three v-belt pulleys on the treadmill drive roller,
135 hung ropes over the pulleys and attached moderate weights to the ropes (~8 kg). We
136 chose the minimum amount of weight such that when the subject stood on the belt with the
137 motor turned off, the belt did not move. Providing a mechanical resistance to the motor
138 allowed it to produce power and maintain a nearly constant treadmill belt speed.

139

140 The study consisted of three sessions. During the first session (familiarization), each
141 athlete walked and ran for 2 to 3 minutes on the treadmill at 4 angles (9.4, 30.0, 35.0 and
142 39.2°). During the second and third visits, subjects either walked (e.g. Day 2) or ran (e.g.
143 Day 3) for 5 minutes at 7 different angles (9.4°, 15.8°, 20.4°, 24.8°, 30.0°, 35.0° and 39.2°)
144 and corresponding treadmill belt speeds (2.14, 1.29, 1.00, 0.83, 0.70, 0.61, 0.51 m/s).
145 Subjects had five minutes rest between trials. Half of the subjects walked on Day 2 and
146 ran on Day 3; the other half did the opposite. These angle and speed combinations fixed
147 the vertical velocity at 0.35 m/s. We chose this vertical velocity knowing the VK records for
148 men (29:42 = 0.56 m/s vertical velocity) and women (36:04 = 0.46 m/s vertical velocity)
149 and recognizing the need for submaximal intensities so that we could record steady-state
150 metabolic rates. Pilot testing indicated that faster vertical velocities would elicit non-
151 oxidative metabolism. For each subject, we randomized the order of the angles used on
152 both Days 2 and 3.

153

154 *Metabolic data.* To determine the metabolic rates during walking and running, we used an
155 open-circuit expired gas analysis system (TrueOne 2400, ParvoMedic, Sandy, UT, USA).
156 Subjects wore a mouthpiece and a nose clip allowing us to collect the expired air
157 determine measure the rates of oxygen consumption ($\dot{V}O_2$) and carbon dioxide production
158 ($\dot{V}CO_2$). We averaged the data of the last 2 minutes of each trial. We then calculated
159 metabolic rate in W/kg using the Brockway equation (2). We only included trials with
160 respiratory exchange ratios (RER) less than 1.0. We calculated the vertical costs ($J \cdot kg^{-1} \cdot$
161 m^{-1}) of walking ($C_{w_{vert}}$) and running ($C_{r_{vert}}$) by dividing the gross metabolic power by the
162 vertical velocity.

163

164 *Biomechanical parameters.* To measure stride parameters, we recorded each trial using a
165 high-speed video camera (Casio EX-FH20) at 210 fps. We extracted contact and stride
166 times for 10 strides using Kinovea 0.8.15 software (www.kinovea.org) and then calculated
167 stride frequency ($=1/\text{stride time}$) and stride length ($=\text{velocity}/\text{stride frequency}$). To
168 determine duty factor, we divided contact time for one foot by the total stride period.

169

170 *Statistical analysis*

171 We analyzed the data using SPSS with significance set at $p \leq 0.05$. We analyzed the
172 vertical cost of walking ($C_{w_{vert}}$), vertical cost of running ($C_{r_{vert}}$) and biomechanical
173 parameters with a general linear model repeated measures considering two factors (slope
174 and gait: walking versus running). We followed up with a Bonferroni post-hoc test when
175 significant differences were detected. At 9.4° the treadmill belt speed was faster than the
176 walk-run transition speed, thus only 9 subjects were able to complete the entire 5-minute
177 trial using a walking gait. Therefore, when making statistical comparisons of the 9.4° trials,
178 we calculated the variables for just those 9 subjects.

179

180 **RESULTS**

181 *Vertical cost of walking vs. running.* At 9.4° , the vertical cost of walking ($C_{w_{vert}}$) was
182 numerically slightly greater than vertical cost of running ($C_{r_{vert}}$) but they were not
183 statistically different ($n=9$; $+1.54\%$; $p=0.545$). However, $C_{w_{vert}}$ was significantly less than
184 $C_{r_{vert}}$ at 15.8° (-6.35% ; $p=0.001$), 20.4° (-8.45% ; $p=0.001$), 24.8° (-8.73% ; $p=0.001$), 30.0°
185 (-9.23% ; $p=0.001$), 35.0° (-8.99% ; $p=0.001$) and 39.2° (-8.93% ; $p=0.001$) (Table 1).

186

187 $C_{w_{\text{vert}}}$ was numerically least at 30° ($43.86 \pm 2.02 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$), but was not statistically
188 distinguishable from 20.4° ($44.23 \pm 1.69 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$), 24.8° ($44.10 \pm 2.10 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$) or 35.0°
189 ($44.57 \pm 2.14 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$) (Table 1, Figure 3). $C_{w_{\text{vert}}}$ at 15.8° was less than $C_{w_{\text{vert}}}$ at 9.4°
190 ($n=9$; -18.2% ; $p=0.001$). Further, $C_{w_{\text{vert}}}$ at 20.4°, 24.8°, 30.0° and 35.0° was less than
191 $C_{w_{\text{vert}}}$ at 15.8° (average -5.47% ; $p<0.001$). Additionally, $C_{w_{\text{vert}}}$ at 39.2° was significantly
192 greater than $C_{w_{\text{vert}}}$ at 20.4°, 24.8°, 30.0° and 35.0° (average $+4.31\%$; $p<0.001$).

193

194 $C_{r_{\text{vert}}}$ was numerically least at 24.8° ($48.22 \pm 2.57 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$), but was not statistically
195 distinguishable from at 20.4° ($48.31 \pm 2.54 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$), 30.0° ($48.32 \pm 3.07 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$) or
196 35.0° ($48.97 \pm 3.01 \text{ J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$) (Table 1, Figure 3). $C_{r_{\text{vert}}}$ at 15.8° was less than $C_{r_{\text{vert}}}$ at 9.4°
197 (-7.88% ; $p=0.001$). As was true for walking, $C_{r_{\text{vert}}}$ at 20.4°, 24.8°, 30.0° and 35.0° was less
198 than $C_{r_{\text{vert}}}$ at 15.8° (average -2.90% ; $p<0.001$). Finally, $C_{r_{\text{vert}}}$ at 39.2° was greater than
199 $C_{r_{\text{vert}}}$ at 20.4°, 24.8°, 30.0° and 35.0° (average $+4.42\%$; $p<0.001$).

200

201 *Biomechanical parameters.* Walking stride frequency was slower than running stride
202 frequency at every incline (average $-27.99\% \pm 7.75\%$; $p<0.001$) (Figure 4A). Thus, walking
203 stride length was longer than running stride length at every incline (Figure 4B). In both
204 walking and running, stride frequency and stride length decreased on steeper inclines at
205 the correspondingly slower treadmill belt speeds (Figure 4A and 4B). Duty factor was
206 greater than 50% for both walking and running conditions at all speed/incline combinations
207 tested, indicating non-aerial gaits. Walking duty factor was greater than the running duty
208 factor at every incline (average $10.29 \pm 5.92\%$; $p<0.001$) except at 40°.

209

210 **DISCUSSION**

211 Our major findings are: 1) across the range of angles and speeds tested, which fixed the
212 vertical velocity, walking is less expensive than running, 2) there is a broad range of
213 angles for which the vertical costs of walking and running are minimized, 3) at the
214 angle/speed combinations we studied, in both walking and running, at least one foot is
215 always in contact with the ground.

216

217 Our results support the hypothesis that at a fixed vertical velocity of 0.35 m/s, walking
218 would be less expensive than running at steep inclines, though at 9.4° there was not a
219 significant difference between gaits. Explaining the energetic difference between walking
220 and running is not straightforward. We know that the inverted pendulum and spring

221 mechanisms that conserve mechanical energy during level walking and running
222 respectively are disabled during uphill locomotion (8, 24), but it is not yet possible to
223 quantify those effects. Minetti et al. (18) showed that during uphill locomotion the “internal
224 work” for reciprocating the limbs is actually greater in walking than in running despite the
225 slower stride frequencies in walking. Kram and Taylor (13) established that metabolic rate
226 is inversely proportional to contact time during level running. At the inclines and speeds in
227 the present study, the contact times for running averaged $34.4 \pm 3.2\%$ less than for walking
228 and that may at least partially explain the metabolic cost difference between the two gaits.
229 Further, because of how the legs are positioned differently in the two gaits, the mechanical
230 advantages of the extensor muscles at the knee are larger in level walking vs. running (1).
231 Smaller muscle forces require a smaller active muscle volume which is energetically
232 cheaper. However, we are not aware of any mechanical advantage measurements for
233 steep uphill locomotion.

234

235 At 9.4° , the treadmill belt speed (2.14 m/s) was much faster than during the other trials,
236 and is equal to the spontaneous walk-run transition speed on level ground, ~ 2 m/s (3, 11,
237 15). Previous studies (4, 10, 11) have demonstrated that the preferred transition speed is
238 slower on moderate inclines and that humans generally choose the gait that minimizes
239 their metabolic cost (17). In the present study, at 9.4° and 2.14 m/s, all of the subjects
240 informally expressed that they would prefer to run. At 15.8° and 1.29 m/s, walking was
241 significantly cheaper but most of the subjects expressed that they would prefer to run.
242 Between 20.4° and 1.00 m/s and 30.0° and 0.70 m/s subjects mentioned that walking felt
243 better. But, if there were no constraints, they thought that they would prefer to alternate
244 between the two gaits every one or two minutes. At 35.0° and 0.61 m/s and 39.2° and only
245 0.51 m/s, gait preference was ambiguous. Subjects expressed that they did not strongly
246 prefer walking (the less expensive gait) because they felt running involved less
247 musculoskeletal “stress” and also balance was more challenging when walking. A future
248 study focused on gait preference, metabolic cost and perceived effort during both walking
249 and running on steep inclines is needed to better understand this topic.

250

251 We reject our second hypothesis. Rather than there being a distinct optimum, we found
252 that there is a range of angles for which $C_{w_{\text{vert}}}$ and $C_{r_{\text{vert}}}$ are minimized. For both walking
253 and running, the minimum values were reached between 20.4° and 35° . A second order
254 polynomial regression suggests that the minimum values for $C_{w_{\text{vert}}}$ and $C_{r_{\text{vert}}}$ would be

255 attained at 28.4° ($R^2=0.64$) and 27.0° ($R^2=0.33$), respectively. At angles shallower than
256 20° , both $C_{w_{\text{vert}}}$ and $C_{r_{\text{vert}}}$ are significantly greater. This could be due in part to the greater
257 metabolic power required to support body weight at faster treadmill belt speeds (9).
258 Further, at our extreme angle, 39.2° there was an increase in $C_{w_{\text{vert}}}$ and $C_{r_{\text{vert}}}$ which we
259 believe is caused by the difficulty of maintaining balance at such steep angles. Part of the
260 balance challenge was due to the fact that at 39.2° , the treadmill belt speed was only 0.55
261 m/s and involved exaggerated contact times (0.924 ± 0.09 s for walking and 0.588 ± 0.11 s
262 for running). In a pilot study, two subjects tried to walk and run with the treadmill inclined to
263 45° and the $C_{w_{\text{vert}}}$ and $C_{r_{\text{vert}}}$ both increased dramatically compared to $\sim 40^\circ$. Balance was
264 quite difficult for those pilot subjects and they frequently grabbed the handrails. Moreover,
265 at that extreme slope, both subjects reported discomfort in their calves and feet because of
266 excessive stretch. For that reason, we “only” studied up to 39.2° in the actual experiment.
267 For C_w and C_r at angles between 10° and 24.8° , our results are congruent with the 5th
268 order polynomial regression formula given by Minetti et al. (21). However, extrapolating
269 beyond 24.8° , that formula leads to large overestimates of the C_w and C_r (Figure 5).

270

271 A recent paper from our lab, Hoogkamer et al. (9), proposed a new explanation for the
272 metabolic cost of running up relatively shallow inclines $< 9^\circ$. In that model, the cost of
273 running (C_r) is determined by three factors: the cost of perpendicular bouncing, the cost of
274 parallel braking and propulsion and the cost of lifting the center of mass. They assumed a
275 constant efficiency for performing the center of mass lifting work, their results supported
276 that assumption and they derived a value of $\sim 29\%$ efficiency. In the present study, the
277 vertical work rate was held constant between the different inclines and thus with the same
278 efficiency the vertical cost would be the same between running conditions. In the
279 Hoogkamer et al. study, as the incline approached 9° , the cost of parallel braking and
280 propulsion approached zero. At the even steeper angles used in the present study, the
281 cost of parallel braking and propulsion (the “wasted impulse”) presumably is nil. Finally,
282 Hoogkamer et al. reasoned that the cost of perpendicular bouncing would not change over
283 the moderate inclines they studied. At the steeper inclines used in the present study, just
284 based on trigonometry, the perpendicular forces would be less than during level running
285 (e.g. $\sim 13\%$ reduced on a 30° incline, cosine = 0.866). However, the running speeds on
286 the inclines studied here were much slower than typical level running speeds and involved
287 prolonged contact times. Prolonged contact times presumably would allow recruitment of
288 slower (and more economical) muscle fibers to generate the perpendicular forces, but long

289 contact times impair the spring-like bouncing motion and therefore might be less
290 economical (5). Overall, from the Hoogkamer et al. perspective, the broad plateau of
291 $C_{r_{vert}}$ observed for running at angles from 20.4° to 35° probably results from counteracting
292 savings vs. costs for perpendicular bouncing at the different speed and angle
293 combinations. A similar model for uphill walking has not yet been put forth.

294

295 As we hypothesized, there was no aerial phase in steep uphill running, i.e. the duty factor
296 (average $62.7 \pm 0.80\%$) was greater than 50% at every incline tested. This suggests that
297 other parameters should be considered to distinguish between walking and running uphill.
298 McMahon et al. (16) defined “Groucho running” as a non-aerial gait that still involved a
299 bouncing center of mass trajectory, i.e. the center of mass was lowest at mid-stance.
300 Rubenson et al. (23) used the term “grounded running” for the same phenomenon in
301 running birds. Because our subjects were running uphill, the center of mass-based
302 definition probably does not apply (8). Nonetheless, when we asked our subjects to either
303 “walk” or “run”, they all subjects immediately and intuitively distinguished the two gaits.
304 Previous studies reported that when treadmill speed is fixed, on steeper inclines, stride
305 length and aerial time decrease and stride frequency increases (7, 22). We observed
306 decreases in both stride frequency and stride length at steeper angles (figure 4 and 5)
307 because treadmill speed was slower at the steeper angles we tested. Thus, with our
308 experimental design, we could not determine how speed and incline independently affect
309 stride frequency and stride length.

310

311 *Limitations and future research*

312 One limitation of our study is that it was conducted on a treadmill whereas VK races are
313 performed on uneven terrain (ski slopes, trails) with the presence of stones, stairs, gravel
314 etc. Voloshina and Ferris report that the energy expenditure of running on an uneven
315 terrain treadmill was only 5% higher than on a smooth treadmill (26). But, Zamparo et al.
316 showed that running on a sandy terrain requires 20% more energy than on firm terrain
317 (27). Thus, the cost of transport during a real VK race is surely somewhat greater than
318 what we measured on our treadmill. Another limitation was that our treadmill did not permit
319 the use of poles. The VK world record as well as most of the fastest performances
320 outdoors were achieved using poles.

321

322 Future studies should compare uphill walking and running with and without poles in order
323 to determine if using poles is advantageous. Further studies involving different
324 combinations of vertical velocity, treadmill speed and angle are also needed. Finally, a
325 more thorough biomechanical comparison of walking vs. running is in order since on steep
326 inclines the defining characteristic(s) of these two gaits are not yet clear.

327

328 In conclusion, we studied the cost of walking and running at angles substantially steeper
329 than any previous study. We found that for both walking and running there is a range of
330 angles (20.4 degrees to 35.0 degrees) for which energy expenditure is minimized. Our
331 data suggest that, to achieve the best results, VK races should be contested within this
332 range of angles. Although other factors may be important, on very steep slopes, athletes
333 can reduce their energy expenditure by walking rather than running.

334

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338

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- 407

408 **FIGURE AND TABLE CAPTIONS**

409 Figure 1. The average of the five best performances for ten different VK races in the year
410 that the each course record was set. 1: The Rut VK (USA); 2: Val Resia VK (I); 3: Mont
411 Blanc VK (F); 4: Limone Vertical Extreme (I); 5: Latemar VK (I); 6: VK Lagunc (I); 7: VK
412 face de Bellevarde (F); 8: Dolomites VK (I); 9: VK Col de Lana (I); 10: VK de Fouilly (CH);
413 11: La Verticale du Grand Serre (F); USA: United State of America; I: Italy; F: France; CH:
414 Switzerland.

415

416 Figure 2. Customized treadmill mounted at 30°.

417

418 Figure 3. Metabolic power (W/kg) and vertical cost of transport (CoT_{vert} , J/kg·m) of walking
419 (black circles) and running (white circles) plotted as a function of angle (degrees) and
420 treadmill speed (m/s) for 15 subjects. At 9.4° only 9 subjects were able to walk at the
421 required speed (2.14 m/s). Except for 9.4°, walking was less metabolically expensive than
422 running. See text for more details.

423

424 Figure 4. Stride frequency (strides/s, 4A) and stride length (m, 4B) for walking (black
425 circles) and running (white circles) as a function of angle (degrees) and treadmill speed
426 (m/s) for 15 subjects. At 9.4° only 9 subjects were able to walk at the required speed (2.14
427 m/s).

428

429 Figure 5. Mean cost of running (Cr , in J/kg·m) measured in the present study (white
430 circles) and computed with the formula of Minetti et al. (21) (black line). The dashed line
431 extrapolates to angles steeper than 24.2° (45%). The relationship between Cr and the
432 slope for our data is described by the formula $Cr = 1.3614 + 0.7686$ (angle in degrees)
433 ($R^2=0.97$).

434

435 TABLE 1. Vertical cost of walking and running (mean±SD, in J/kg·m) as a function of the
436 slope angle (°) and treadmill belt speed (m/s). Vertical velocity was fixed at 0.35 m/s. At
437 9.4° only 9 subjects were able to walk at the required speed (2.14 m/s). For all other
438 angles n=15.

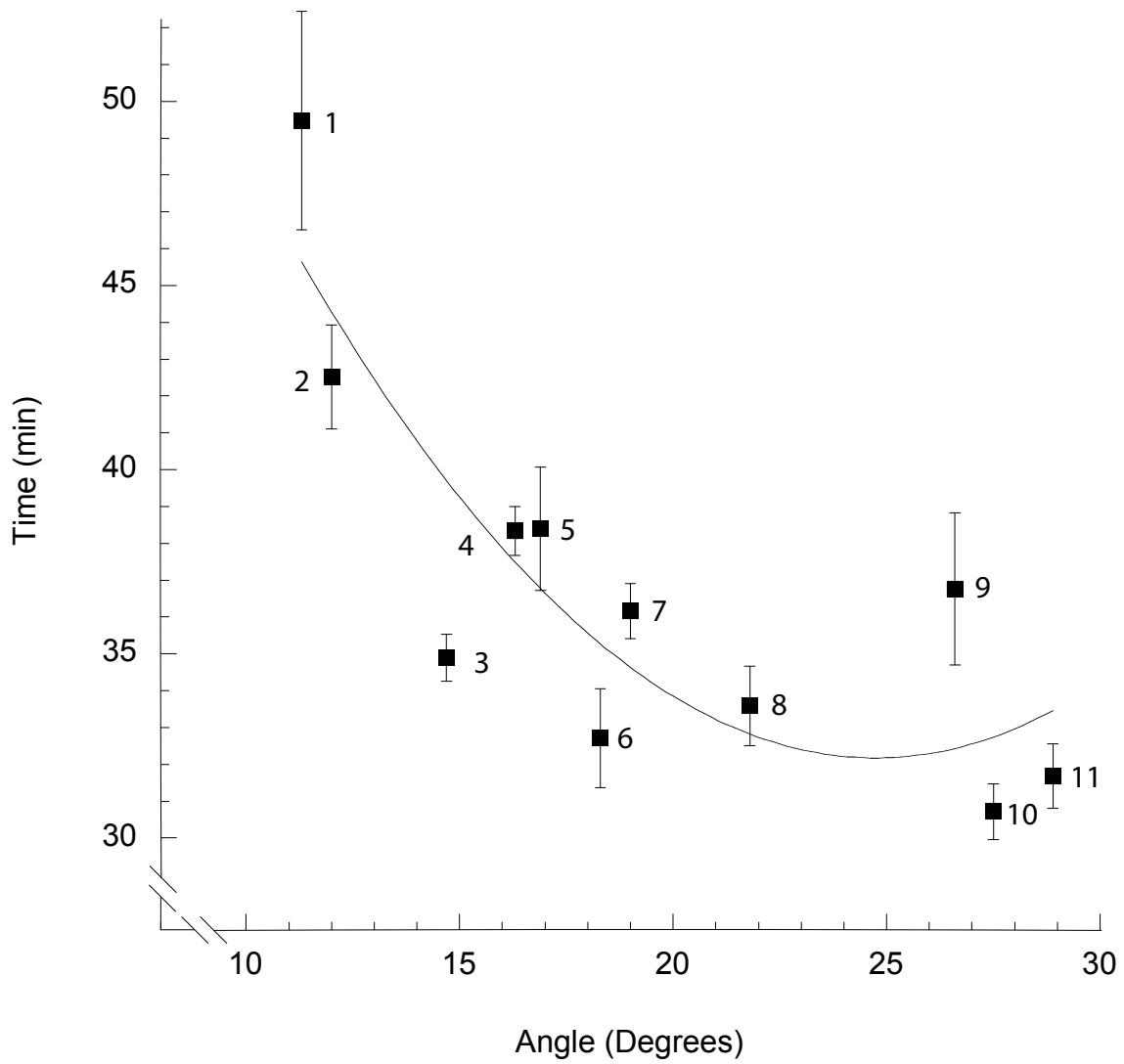


Figure 2

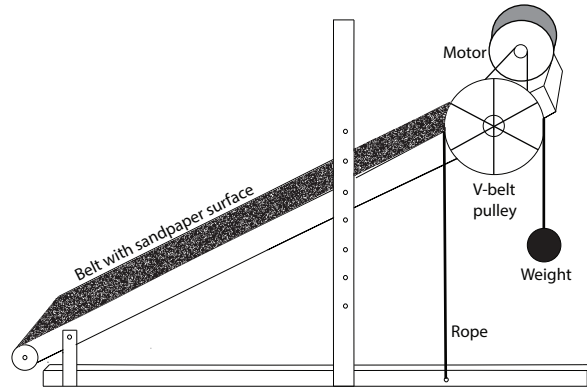


Figure 3

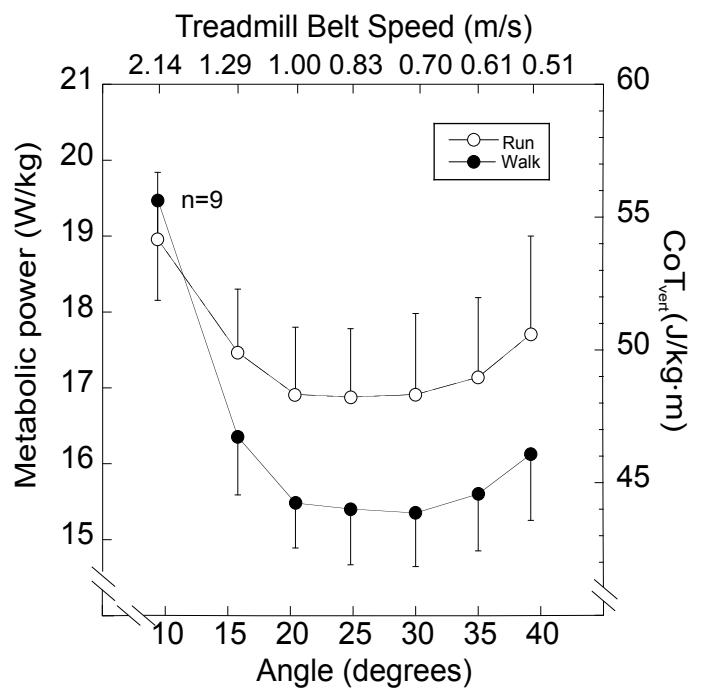


Figure 4

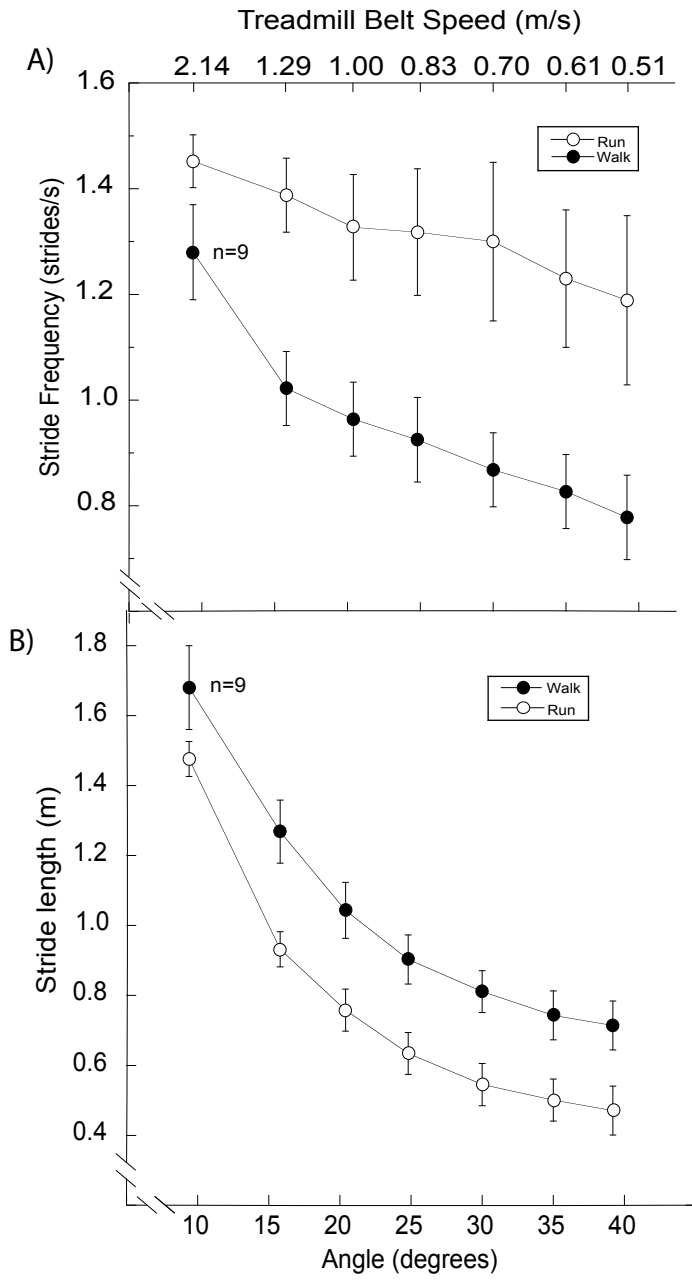


Figure 5

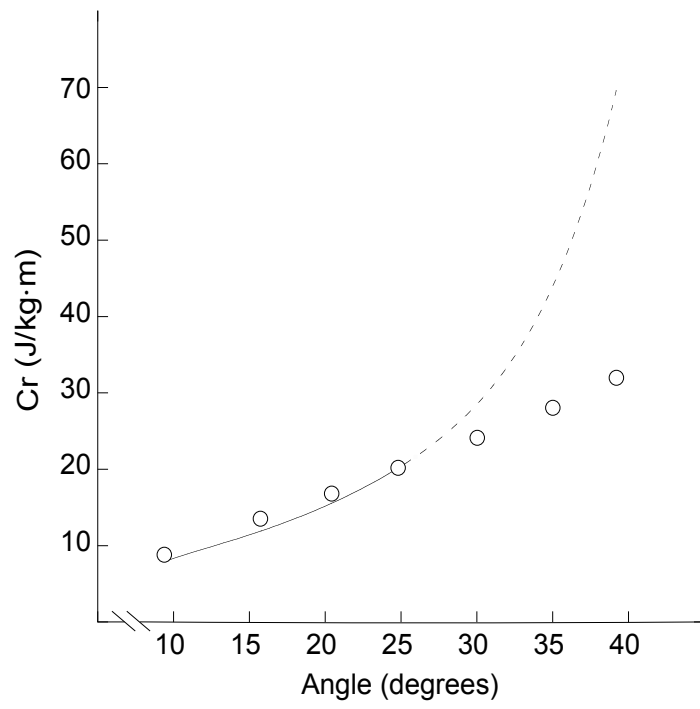


Table 1. The vertical cost of walking and running as function of the slope angle.

Angle (degrees)	Treadmill belt speed (m/s)	Walk ($\text{J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$)	Run ($\text{J} \cdot \text{kg}^{-1} \cdot \text{m}^{-1}$)	Difference (%)	p
9.4	2.14	55.67 ± 3.80	54.83 ± 2.29	1.53	0.545
15.8	1.29	46.73 ± 2.19	49.90 ± 2.37	-6.35	0.001
20.4	1.00	44.23 ± 1.69	48.31 ± 2.54	-8.45	0.001
24.8	0.83	44.01 ± 2.10	48.22 ± 2.57	-8.73	0.001
30.0	0.70	43.86 ± 2.02	48.32 ± 3.07	-9.23	0.001
35.0	0.61	44.57 ± 2.14	48.97 ± 3.01	-8.99	0.001
39.2	0.51	46.07 ± 2.49	50.59 ± 3.70	-8.93	0.001

A Mechatronic System Mounted on Insole for Analyzing Human Gait

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Abstract—In this paper, designing and fabricating a mechatronic system for analyzing exerted forces by human gait has been described. Force sensitive resistors (FSRs) sensors as well as Arduino Due (Microcontroller) have been utilized in the system which is mounted on a shoe insole. Furthermore, the applied Interrupt Service Routine (ISR) programming technique in microcontroller and signal conditioning circuit design has been explained. The mechatronic system has been tuned and calibrated through the experimental tests and some of the important results have been presented and discussed.

Keywords— Force sensitive resistors (FSRs), Arduino Due, insole, force platform, gait

I. INTRODUCTION

It might be indeed true to say that human body motion has been under investigation since about fifty years ago. Several researchers focused on analyzing human body motion from different points of view; in fact, there are some motivating reasons for them. From scientific perspective, realizing and comprehending details of human motion is an important problem. Walking and running efficiently; that is, moving with minimum energy consumption is an interesting issue for the sportive researchers. From the medical point of view, diagnosing and preventing some injuries and diseases such as diabetes can be done by analyzing body motion. Ankle moment has a remarkable effect on trunk acceleration propulsion, and balance while walking [1].

Some types of systems are using air coils in the shoes for measuring the pressure in order to monitor human gait, as in the work by Kyoungchul in [4]. Furthermore, different kind of instruments have been presented so far for gait event detections or fault diagnostician [5]–[9]. Generally speaking, recognition and analysis of the human gait can be subdivided in three different approaches: image processing, floor sensors and sensors placed on the body [10].

Precise result from motion Kinect requires analyzing the steps during walking on a surface of the force plates; otherwise, may lead to inaccuracies. Many methods have been developed in order to analyze human walking. Infrared cameras and force plates have been used in some laboratories because of their accurate measurement and also availability of standards for them. The high price is the main disadvantage of

these type of instruments. Some other types of instruments such as treadmills are available but walking in a normal way is different from walking on the treadmills. Moreover other types of instruments are commercially available in market but they are expensive products so they are not easily available for general usage [2], [3].

A simple cheap footswitch system has been presented in [11] in order to measure accurately the initial and end foot contact time. The idea of this footswitch not only has been widely used in the systems for mobile gait analysis, but also is used in our work for the purpose of building an accurate and inexpensive mechatronic system mounted on a shoe insole with use of force sensitive resistors (FSRs). Applying FSRs sensors result in high nonlinear-response which leads to difficulty in parameters calculating that is a challenging problem for designing a measurement system for gait analysis [12].

In this paper, the design and the test of a mechatronic system mounted on insole platform in order to measure and analyze force reaction during walking is discussed and presented. The mechatronic system is based on two main parts: the sensorial insole and the data acquisition device. The shoe insole includes five force sensitive resistors (FSRs) with separated signal channels. The main part of data acquisition block is a microcontroller (Arduino) for ADC conversion and data logging on a SD card. For calibrating the system and finding the most optimized coefficient of conversions (volt-newton) and also reducing the value of RMS of error signals, a force platform has been used.

Although a number of works and products has been done in this area and some of them are similar to our work such as newest one in [13], there are some remarkable difference



(a)



(b)

Fig. 1. a) Front view of Arduino Due, b) FSR sensor (Flexiforce A401)

between our work and the others. Using low-cost instruments, average error of 5% and the minimum invasiveness at the end of the athletic gesture are the main advantages and differences between our work and the others.

This paper is organized as follows: Section II briefly explains the data acquisition technique. The description of the sensors is give in Section III. Section IV provides a description on the system realization. In Section V the methodology of calibration and tuning has been discussed.

II. DATA ACQUISITION

Data acquisition and logging is performed by a custom microcontroller system that has the ability of recording the measured data on a SD memory card. In our system the Arduino Due (Fig. 1.a) which is a microcontroller board based on the Atmel SAM3X8E ARM Cortex-M3 CPU [14] has been used for force data logging on a SD card. In our system the Arduino Due (Fig. 1.a) which is a microcontroller board based on the Atmel SAM3X8E ARM Cortex-M3 CPU [14] has been used for force data logging on a SD card.

First, the available data values will be copied in the first cell of the circular buffer, then they will be transferred from the

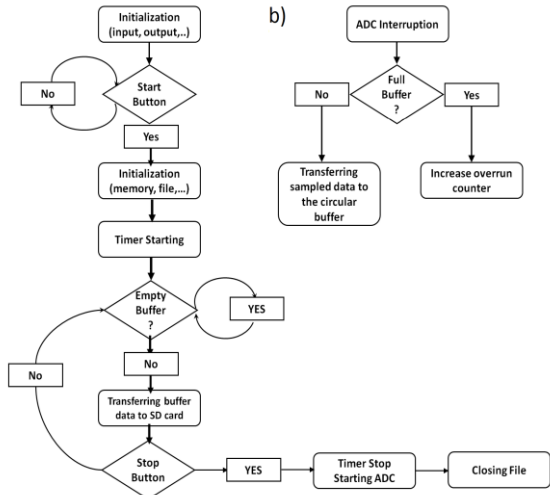


Fig. 2. Flowchart of Arduino program, a) the flowchart of the main () program, b) the flowchart of the interruption service routine (ISR) program for data sampling

TABLE I

TYPICAL PERFORMANNCE OF SENSOR FLEXIFORCE A401

Typical Performance	Evaluation Condition
Linearity (Error) $< \pm 3\%$	Line drawn from 0 to 50% load
Repeatability $< +2.5\%$ of full scale	Conditioned sensor, 80% of full force applied
Hysteresis $< 4.5\%$ of full scale	Conditioned sensor, 80% of full force applied
Drift $< 5\%$ per logarithmic time scale	Constant load of 25 lb (111N)
Response Time $< 5 \mu\text{sec}$	Impact load, output recorded on oscilloscope

buffer to the memory card. The last step will be done during the pause time between two sequence acquisition times. Fig. 2 illustrates the flowchart of the main program of microcontroller (Arduino Due). The Fig. 2.a shows the main program flowchart for data acquisition of the received signals and saving data on a memory card. The flowchart of the program for Interrupt Service Routine (ISR) of data sampling is illustrated in Fig. 2.b.

According to Fig. 2, once the sampling ISR has been

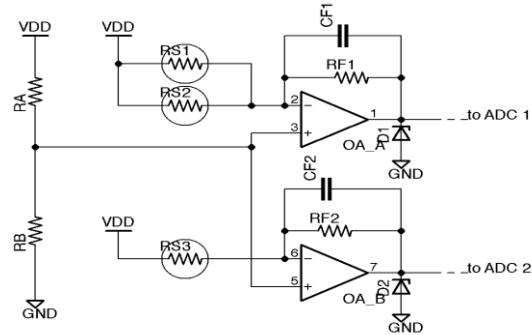


Fig. 3. Signal Conditioning Circuit (In the figure, only two channels of six channels have been demonstrated)

completed, the microcontroller goes back to the main () loop, in which the acquired samples are transferred to the SD card. When the timer generates another interrupts (so the sampling Routine is started again), the transfer is stopped and can be restricted once the ISR is completed.

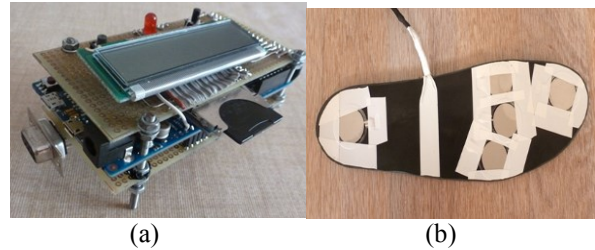


Fig. 4. a) The mounted boards of the acquisition system. In order from the bottom: Signal conditioning circuit (on the left side, the arrived signals connector from the sensors is visible), the board of Arduino Due, the control board with the SD slot for memory and the display, b) Sensorial insole, the five Flexiforce A401 sensors are visible

III. SENSORS

A. FSR Sensors

The measurement of the ground reaction force (GRF) is done by force sensing resistors (FSR). This kind of the sensors are frequently used in similar works [13], [15], [16]. Teksan Flexiforce A401 (Fig.1.b) is the type of the sensor that has been chosen in our system. The typical performance of this sensor is reported in Table I.

B. Signal Conditioning Circuit

Signal conditioning circuit which is a conductance-voltage convertor, has been used to convert the received signals from

sensors in readable mode for ADC (Analog Digital Converter). Fig. 3 shows the signal conditioning circuit; R_{S1} , R_{S2} and R_{S3} are the resistive sensors. The DC gain of the first channel can be calculated by considering the superposition effect as follows:

$$V_{out2} = -V_{DD} \frac{R_F}{R_{S1}} - V_{DD} \frac{R_F}{R_{S2}} + V + \left(1 + \frac{R_F}{R_{S1} || R_{S2}}\right) \quad (1)$$

By reorganizing the equation 1, the following equation can be obtained:

$$V_{out2} = -\Delta V \frac{R_F}{R_{S1}} - \Delta V \frac{R_F}{R_{S2}} + V_+ \quad (2)$$

Where $\Delta V = V_{DD} - V_+$ and $V_+ = 3.2 \text{ Volt}$ for Arduino Due.

As it can be seen in Fig. 3, two 3.6 Volt Zener diodes (D_1 and D_2) are mounted in parallel to the output. These diodes act as a voltage protection for the inputs of the ADC channels. In fact if the voltage of one of the input pins surpass the breakdown voltage of the Zener diode, the diode acts and prevents the probable damages on microcontroller.

The values of R_A and R_B resistors are chosen 1.8 k Ω and 3.3 k Ω respectively. The value of the feedback resistor has been chosen to fully exploit the ADC range. Knowing that during running the reaction of vertical forces to the ground reaches up to twice the body weight [17] and estimating the maximum weight of a person on the test is 100 kg so the scale measuring system is based on 200 kg (less than 2000 N). Regarding the information on the data sheet of the Tekscan Flexiforce A401 sensor, it is possible to estimate about the conductance of the sensor under 200 kg (440 lb) pressure.

The conductance / weight ratio can be calculates as:

$$m = \frac{G_s(120lb) - G_s(20lb)}{120lb - 20lb} = 1.6 \times 10^{-7} \left[\frac{S}{lb} \right] \quad (3)$$

With knowing the value of slope of the conductance/weight, the conductance can be evaluated as:

$$G_s(440lb) = m \cdot f = m \cdot 440 \text{ lb} = 70.4 \mu S \quad (4)$$

And the resistance of the sensor can be obtained as:

$$R_s(440lb) = \frac{1}{G_s(440lb)} = 14.2 \text{ k}\Omega \quad (5)$$

Now by considering the equation 2, the value of R_F (neglecting the second sensor) is:

$$R_{F2} = \frac{V_+ - V_{out}}{\Delta V} R_s = \frac{3.2V - 0.2V}{1.8V} \times 14.2 \text{ k}\Omega = 23.5 \text{ k}\Omega \quad (6)$$

The nearest commercial resistor to R_{F_DUE} is 22k Ω . The capacitor is also used in signal conditioning circuit in order to have a cutoff filter for the frequency about $F_C=250 \text{ Hz}$ and can be obtained as follows:

$$C_{F_DUE} = \frac{1}{2\pi F_C R_{F_DUE}} = 29 \text{ nF} \quad (7)$$

The nearest commercial capacitor to C_{F2} is 27nF. A filter capacitor has been used to reduce filter noise at high frequencies.

IV. SYSTEM REALIZATION

The final version of our system includes two main blocks: Data Acquisition Block and Sensorial Insole. The data acquisition block is mounted on a mounting box that is kept trough a belt on the person's body during the running; while, the sensorial insole is located in the shoe. The two blocks are connected with heavy duty multipolar cables.

A. Data Acquisition Block

The data acquisition block is based on three boards: The Arduino Due microcontroller board, an expansion board that mounts the slot for the memory card and some circuits for the control of the acquisition and the signal conditioning circuit for six separated channels of data acquisition.

These boards are positioned one above another and interconnected with the connector (header) so they can easily be disassembled for any changes or tune-ups. The final structure of data acquisition block is shown in Fig. 4.a.

B. Sensorial Insole

Fig. 4.b illustrates the last version of the sensorial insole that was placed in a shoe. As it can be seen, the sensors are located on a nominally flat surface. Several arrangements of force sensors have been investigated to experimentally determine the optimal placement, as shown in Fig. 5. The main advantages of this type of sensor location is that sensors can work in an optimal condition. The wiring was done with the normal copper wires at the bottom of the slab, cables and connectors are protected by sheaths shrink and held in place by adhesive tape.

V. TUNING AND CALIBRATION

Similar to other measuring systems also our system needs to be calibrated. In fact, our mechatronic system records and registers the behavior of the output voltage of the op-amp.

The gain of the signal conditioning circuit depends on the resistance of the circuit and can change the coefficient of the conversion.

By neglecting the fixed-terms, following equation turns up:

$$V_{out} = -\Delta V R_F G_s \quad (8)$$

Where the value of the conductance G_s is chosen approximately from the sensor data sheet. Regarding the presented material in section III:

$$G_s = m \cdot F_{lb} \quad (9)$$

Where F_{lb} is the applied force on the sensor measured in pound. By substitution the equation 9 in 8 and rearranging the expression for explication the fore, we can obtain:

$$F_{lb} = -\frac{V_{out}}{m \Delta V R_F} \quad (10)$$

For converting the force in pound to newton, multiplication to 4.45 is needed:

$$F_N = -\frac{V_{out}}{m \Delta V R_F} \times 4.45 \quad (11)$$

The value of ΔV is 1.8 V for signal the conditioning circuit of Arduino Due. Therefore, a conversion constant can be obtained:

$$k_{v \rightarrow N} = -\frac{1}{m \Delta V R_F} \times 4.45 = 702 \left[\frac{N}{V} \right] \quad (12)$$

Noting that multiplication of this value by assuming the output swing of the op-amp causes in $702 \times 3 = 2180[N]$ which is the maximum force that the system measures.

In fact the reading carried out from the acquisition is not measuring of voltage but is direct reading of the digital conversion of the signal. Consequently, a range number from 0 to 4095 will present the voltage between 0 and full scale

voltage of ADC ($V_{FS_ADC} = 3.3 \text{ Volt}$). Thus, it is possible to find directly the conversion between the numerical value converted by the ADC and the force:

$$k_{ADC \rightarrow N} = -\frac{1}{m\Delta V R_F} \times 4.45 \times \frac{V_{FS_ADC}}{2^N} = 5.66 \times 10^{-3} \left[\frac{N}{LSB} \right] \quad (13)$$

A. Characteristic Limitation of the System

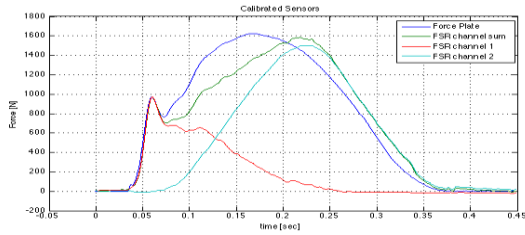


Fig. 6. Initial calibration of the sensors for comparison with the force platform

The technical limitations imposed by the choice of sensors and the variability of each individual body structure require the use of a proper calibration procedure. Also the insole mounted on the shoe can be in different forms that results in different force distributions during the walking. Moreover, the quality of the sensors, their positions and also conditions of their performance (humidity and temperature) can affect the performance of the system.

B. Calibration Methodology

We started from a configuration with 3 sensors on 2 separated channels and then a configuration with 5 sensors on 5 separated channels, as it can be seen in Fig. 5. The methodology used is based on linear regression, the method has been used in similar works where it seems to give good results, leading to an error close to 5% [13]. We can choose among two different strategies for calibration: 1) minimizing the RMS value of the error signal between the readings of the force platform and those of the sensors: this leads to have a behavior of the force which should approximate the overall performance of the platform with some margin of errors. 2) Minimizing the RMS error on the features: this should lead to a trace of the force that deviates the most from the force platform, but it will be less uncertainty about the value of the extracted features.

C. First Configuration

The first sensor configuration of the insole with three sensors and two separated channels is shown in Fig. 5.a. The position of the sensors are chosen in order to consider maximum pressure during the motion [18]. Some tests have been done in the laboratory with the force platform, in Fig. 6 the behavior of the acquired signals of sensors and the force platform has been used. The coefficient for the calibration have been found in a different way for the two channels. For the first channel (where the sensor is located under the heel) a multiplicative constant (K_1) has been found in order to match the amplitude of the first peak recorded by the sensors and the amplitude recorded from the platform. For the second channel the term (K_2) is to minimize the RMS value of the error signal given by:

$$e = f_{ForcePlate} - k_1 \cdot S_{channel_1} - k_2 \cdot S_{channel_2} \quad (14)$$

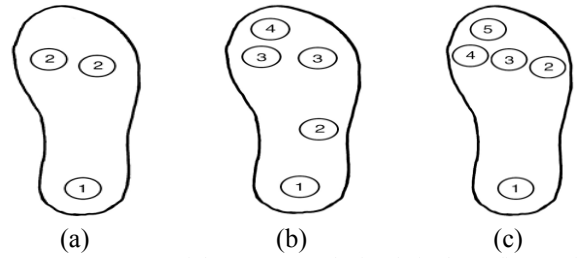


Fig. 5. Arrangement of the sensors on the insole in the a) first version

In which e is the error signal between the acquisition of the force platform and the sensors, $f_{ForcePlate}$ is the signal acquired from the force platform of strength and used as a reference, $K_{1,channel}$ represents the first channel signal acquisition (k_1 is found by comparison of peaks), k_2 is the factor that multiplies the signal of the second channel and $S_{channel_2}$ minimizes the RMS value of e .

Accurate force estimation, correct recording contact time and superimposed of initial part of curves could be concluded from Fig. 6.

D. Second Configuration

The aim of the second configuration is to achieve the greater accuracy of the curve and to obtain this goal, two additional sensors are mounted (four channels and five sensors in total). This arrangement of the sensors is shown in Fig. 5.b. The additional central sensor has the purpose of providing the missing information in the central phase of the step while the

TABLE I II

CALIBRATION COEFFICIENT K WHICH IS CALCULATED WITH USE OF MATLAB. THE VALUES OF EVERY ROW REPRESENTS THE MULTIPLICATIVE COEFFICIENT FOR ACQUIRED DATA BY THE SENSORS AND THEY ARE EXPRESSED IN $\left[\frac{N}{LSB} \right]$

CHANNEL	TEST 1	TEST 2	TEST 3	TEST 4
1	3.37	1.65	2.66	4.49
2	4.45	3.13	6.42	2.90
3	0.79	0	0	0
4	0	1.25	1.22	0.86
5	5.40	0.84	0	3.34

TABLE I III

RMS ERROR IN THE VALUE OF FORCE PEAKS REACHED AT THE MOMENT OF CONTACT WITH THE GROUND (PEAK RELATIVE TO THE HEEL) AND IN THE MOMENT OF MAXIMUM THRUST UPWARDS (PEAK RELATIVE TO THE METATARSALS). THE VALUES WERE NORMALIZED TO THE MAXIMUM VALUE OF THE PEAKS RECORDED FOR EACH TEST.

PEAK	TEST 1	TEST 2	TEST 3	TEST 4
Heel	6.60%	10.7%	15.5%	11.6%
Metatarsal	2.79%	8.84%	7.78%	4.31%

sensor located on the tip is used to obtain the information on the toe force.

Adding channels definitely increases the availability of the information; however, it increases both system complexity and calibration procedure. The results of two experimental tests are shown in Fig 7. As it can be seen, the acquired signal by channel 2 is different (green curve in Fig 7.a and 7.b). This is

because of force platform position, runner style and the higher travel speed achieved during the second test. Another observation made always on the channel 2 is that the signal shape is irregular and noisy by increasing the speed. The results are more accurate in comparison to Fig. 6 (first configuration) due to the more accurate positioning of the sensors.

E. Third Configuration

For the third force sensors configuration, which is depicted in Fig. 5.c, it was decided to follow the approach used in [16], and to remove the central sensor in order to have a better coverage forefoot. The aim is to detect more accurately the impulsive force peaks.

The applied changes in the third configuration are modification of the position of sensor 2 (see the Fig. 5.c) and placement of all the sensors on the independent channels (totally 5 channels).

F. Procedure

The tests for data acquisition have been done based on third configuration in this way: force platform was placed in a running track (in a proper position compared to the level of the ground) and the reaction force exerted by four different tests (subjects) have been recorded and registered. Every test has

exerted force of metatarsals the channels 2, 3, 4 and 5 is taken into account.

This procedure is performed independently for each test. Fig. 7 shows some test results. In particular, the figure refers to the obtained performance with the coefficient that minimize the RMS value of them error signal between the registered force by the force platform and the sensors (this set of coefficient will be K_{graph}).

G. Results

Although these results seems be worse respect to the second configuration it should be taken into account that these results are extracted from 15 steps and not the two first steps of the tests. The calculated coefficient are given in Table II. From these data. We can definitely say that the coefficient vary greatly among each singular test.

Another important observation is that some coefficients are zero, this means that the corresponding channel does not bring any additional information with referring to other channels.

The results are obtained using the second set of coefficient (K_{peaks}), those that minimize the error relating only to the peaks of the curve, are summarized in the Fig. 8 and 9.

The graphs represent the force peaks (on the heel and metatarsals) recorded by the FSR sensors and each point is related to a test. In all cases, we see the trend monotonically increasing (as was expected) showing a certain linearity between the measured force and the exerted force, however, we see that the dispersion of the points is very wide between the tests. The RMS value of the error of these measurement was normalized to the maximum force peak recorded and registered by the force platform from the heel and metatarsals for every test. The results for every test are reported in Table III.

The average value of the RMS error (considering both peaks) is about 8.5%, which is a result not far from the 5% accuracy which was the target of the system. The set of coefficient calculated on the basis of the force peaks are reported in Table IV.

VI. CONCLUSION

In this work an economic mechatronic system mounted on insole in order to measure accurately the vertical forces for the human gait analysis has been realized and presented. While almost the similar systems has dealt with analysis of the walk, in the presented system race forces which conclude higher and more impulsive nature, are also involved.

Laminar FSR sensors have been placed on the insole of the shoe, it was seen that the sensor positions is an important factor in final results. Moreover, it was concluded that high number of sensors will not necessarily increase the accuracy of the system.

The main aspects that have characterized in this work are: Choices of the sensors, physical realization of the prototype in a reliable compact, arrangement of the sensors on the insole in order to obtain the maximum amount of information as possible and Sensor calibration.

TABLE I V

COEFFICIENT CALCULATED TO MINIMIZE THE RMS VALUE OF THE ERROR BETWEEN THE FORCE PEAKS REGISTERED AND RECORDED WITH FSR SENSORS AND THE FORCE PLATFORM K_{PEAKS} . THE MEASUREMENT UNIT IS $\left[\frac{N}{LSB}\right]$.

CHANNEL (Heel)	TEST 1	TEST 2	TEST 3	TEST 4
1	2.85	0	0.4	2
2	7.88	44.1	54.5	11.7
CHANNEL (Metatarsal)	TEST 1	TEST 2	TEST 3	TEST 4
2	1.60	0	1.08	0.35
3	3.18	2.26	1.06	1.90
4	2.39	0.24	2.17	0
5	4.47	0	1.49	7.45

registered totally fifteen steps, this is to understand how the coefficient may be varied depending on the work condition.

Two types of coefficients were calculated with the linear regression. The first set of coefficients is chosen in order to minimize the error between the extracted curves from the force platform and the sensors, and have been calculated by appending the various tests carried out by the same person and also by applying linear regression to the whole performance of all the steps. The second set of coefficients is targeted instead of minimizing the error on the two characteristics peaks of GRF in a way similar to what was done for the first set of coefficients.

For the first peak, which shows the pressure at the moment of heel contact with the ground, channels 1 and 2 (see Fig. 5.c) is considered and for the second peak, which realizes the

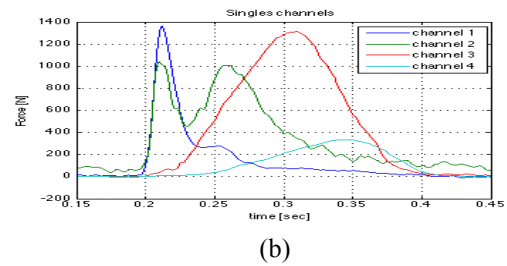
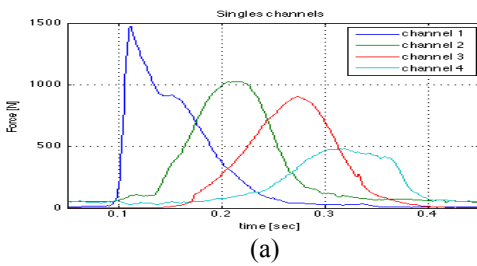


Fig. 7. Data acquisition with the second configuration of two different tests. Total number of channels weighted to reduce the RMS value of the error between two curves. (a-b) performance of individual channels

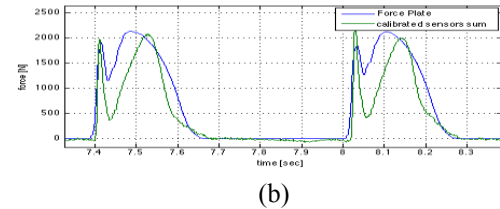
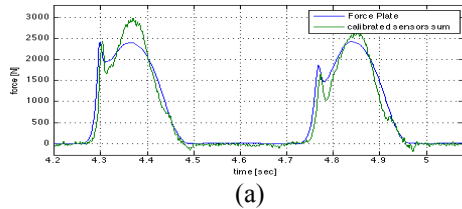


Fig. 8. Acquired signals from two tests. Recorded track process by the force platform (in blue) and that of the calibrated sensors for reducing the RMS value of the error signal between two curves. Here only two steps are shown but totally 15 steps exists for every test.

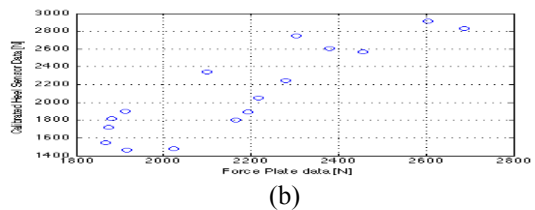
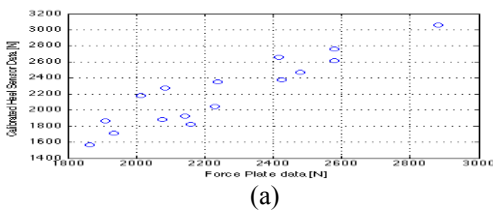


Fig. 9. Peak forces on the heel which are measured by the FSR sensors and actual measured with the force platform. Monotonically trend increasing is clear.

Particularly, the most important features of our system are the parameterization of the force curves and possibility of reconstructing the overall trend described by the parameterized curve.

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