



# High-bandwidth beam balance for vacuum-weight experiment and Newtonian noise subtraction

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**Abstract** We report the experimental results of a prototype balance for the Archimedes experiment, devoted to measure the interaction between quantum vacuum energy and gravity. The prototype is a *beam balance* working at room temperature which shares with the final balance several mechanical and optical components. The balance sensitivity has been tested at the site of the Virgo gravitational wave detector in order to benefit from its quiet environment and control facilities. This allowed also the test of the coherence of the balance data with the Virgo interferometer signal and with the environmental data. In the low-frequency regime, the balance has shown a sensitivity of about  $8 \times 10^{-12} \text{Nm}/\sqrt{\text{Hz}}$ , which is among the best in the world, and it is very promising toward the final Archimedes measurement. In the high-frequency region, above a few Hz, relying on the behavior of the balance as a rotational sensor, the ground tilt has been measured in view of the next work devoted to Newtonian noise subtraction (NNS) in Virgo. The measured ground tilt reaches a minimum of about  $8 \times 10^{-11} \text{rad}/\sqrt{\text{Hz}}$  in the few Hz region and ranges from  $10^{-10}$  to  $10^{-9} \text{rad}/\sqrt{\text{Hz}}$  in the 10–20 Hz region, where a very interesting coherence, at some frequencies, with the Virgo interferometer signal is shown.

## 1 Introduction

In recent years, the measurement of small forces with macroscopic detectors has experienced an enormous development, driven by the interferometers for gravitational wave detection [1–7] and by the improvement of instruments like torsion pendulums and beam-balance rotational sensors [8–11]. Remarkably, torsion balances and rotational sensors, typically working in the mHz region, have shown a considerable overlap of interests both with space-based interferometers and with the ground-based gravitational wave detectors. In this latter case, the control loops, which keep the interferometers on their working point, can benefit, in the sub-Hz region, from a ground tilt signal provided by the rotational sensors [11, 12]. Furthermore, the sensitivity in the low-frequency range (around 10 Hz) of the ground-based detectors is expected to be limited by the so-called Newtonian noise in the next scientific runs [13, 14]. Rotational sensors will provide ground-motion signals useful to reconstruct the

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variation of the gravitational field and hence contribute to the subtraction of Newtonian noise from the gravitational wave signal [15].

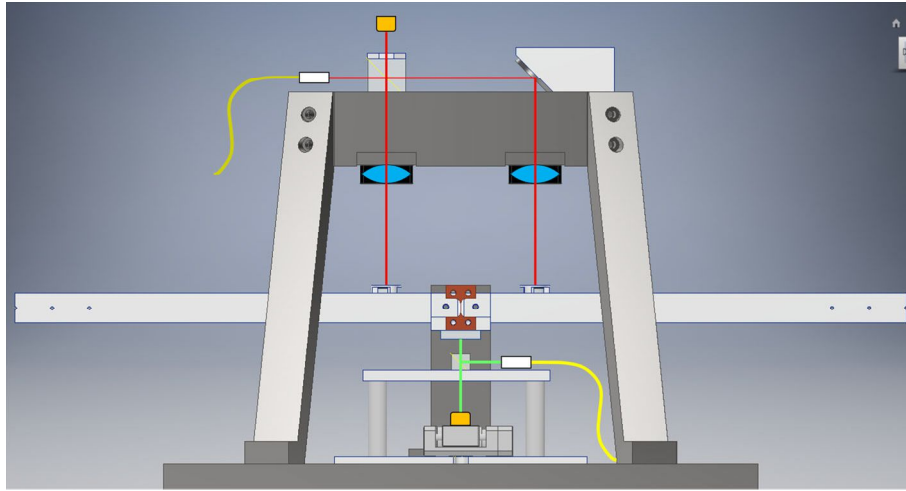
Within the framework of macroscopic detectors of small forces, Archimedes collaboration recently proposed a beam balance to measure the force exerted by the gravitational field on a rigid Casimir cavity. The force to be measured is called the *Archimedes force of vacuum*, as it corresponds to the weight of the vacuum fluctuation modes that are expelled by the Casimir cavity [16, 17]. The measurement consists in detecting the weight variation of a layered type II superconductive sample around its transition [17]. The core of the apparatus will be a cryogenic balance whose design torque sensitivity is about  $\tilde{\tau} = 6 \times 10^{-13} \text{ Nm}/\sqrt{\text{Hz}}$  in the frequency range of tens of mHz or lower [18].

As described in this paper, the apparatus is a rotational sensor. Its characteristic features are low moment of inertia, low restoring force and low resonant frequency in order to maximize the sensitivity to the applied force [18]. To study the feasibility of such an extremely sensitive balance, a prototype working at room temperature has been built. To warrant high sensitivity, the balance readout is an interferometric system. Moreover, the final apparatus will work in a cryogenic environment that implies a long recovery time for each intervention on the balance. For this reason, the readout of the prototype balance has already been designed to be particularly robust and to have a high dynamic range, in order to pledge its capability in recovering the correct interferometer signal even in case of high deviations from the working point. The balance has been initially assembled and tested in the Naples laboratory; then, it has been installed at the Virgo site, which is seismically more quiet, specifically in the North-end building. In this setup, the balance has been tested for the torque sensitivity in the low-frequency regime, while at high frequencies it has been operated as a tiltmeter (rotational sensor). The results of these tests suggest that the balance is presently limited at low frequencies by actuator and sensing noises, while at high frequencies the balance is enough sensitive to measure the ground tilts and can be used for Newtonian noise subtraction. Interestingly, the balance signal is coherent, at some frequencies, with the output of the Virgo interferometer. Although this coherence is not due to Newtonian noise coupling of the ground tilt, it would help in identifying particular noise sources like, for example, diffused light from vibrating elements excited by ground motion.

The paper is organized as follows: In Sect. 2, the mechanical and optical schemes of the prototype balance are described. In Sect. 3, its low-frequency behavior is shown, and a discussion on the reached sensitivity and its possible increase is presented. In Sect. 4, the high-frequency behavior is illustrated, in particular, the use of the balance as a tiltmeter. Finally, the next steps toward further improvements for the balance performance is outlined in Sect. 5.

## 2 The balance prototype

The working prototype of Archimedes is a short-arm version of the final balance, with no samples suspended from its ends. Its core consists of a 50-cm-long arm, attached at its center through two thin wirelike suspensions (Fig. 1), in a configuration similar to LIGO rotation sensor [11]. Unlike this latter, however, the balance requires a high torque-to-tilt transfer function, which implies that momentum of inertia as well as suspension restoring force has to be as low as possible. To fulfill these specifications, the suspended arm is hollow and made of aluminum, leading to a momentum  $0.013 \text{ kg m}^2$  in the case of the prototype. In the final design of the balance, instead, the momentum is  $0.72 \text{ kg m}^2$ , since the arm length is 1.4 m and superconducting samples are suspended from its ends. The restoring force is kept low



**Fig. 1** Scheme of the balance prototype including the optical readout. Notice the two lenses (in light blue), with focal length equal to their distance from the arm. The displacement and relative tilts of the two beams recombining at the beam splitter are of the second order with respect to the arm tilt

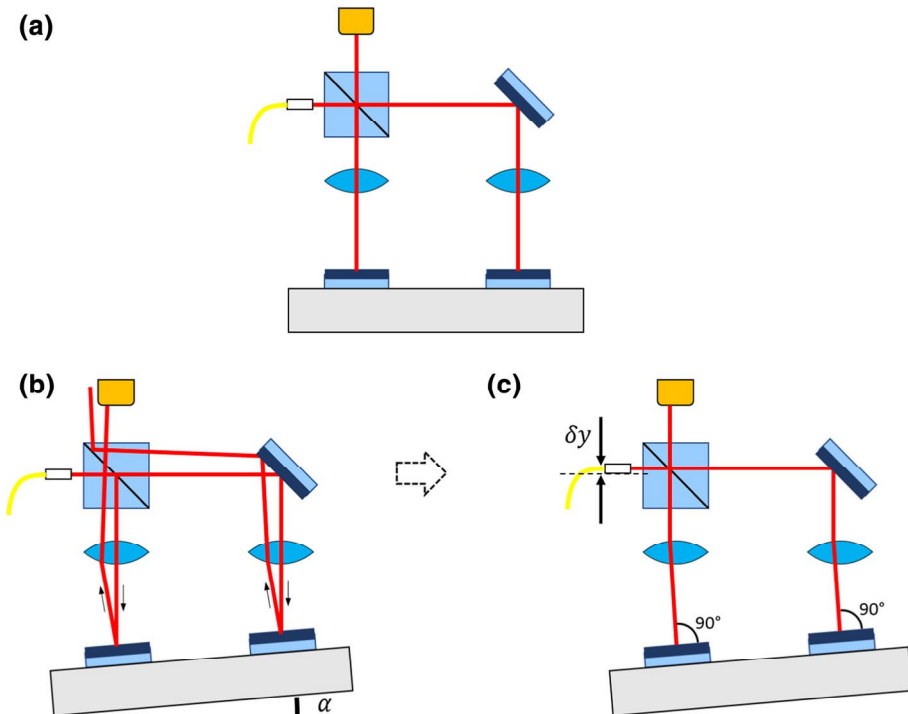
by using thin suspensions with a  $0.5\text{ mm} \times 0.1\text{ mm}$  section. This force, together with the distance between the arm center of mass and its center of rotation, determines the resonance frequency of the balance. The center of mass of the prototype has been tuned to be within  $10\text{ }\mu\text{m}$  from the center of rotation, giving a resonance frequency of  $25\text{ mHz}$ .

### 2.1 Optical readout: interferometer and optical lever

The balance angular motion can be monitored by two different optical readouts: a Michelson interferometer, with higher sensitivity, and an auxiliary optical lever, with wider dynamic range. Both the optical systems are physically bolted to the ground; hence, the arm angular motion is measured with respect to it. The interferometer has been designed with the following requirements: (1) minimize coupling with undesired degrees of freedom; (2) maintain good contrast even for relatively high tilts; and (3) allow realignment by moving optical elements not lying on the reference nor on the measurement arm.

The first condition has been obtained with the beams impinging on the mirrors perpendicularly. To keep a simple optical scheme, a Michelson interferometer with unequal arm lengths has been chosen, for a path length difference of  $10\text{ cm}$ . In the present version of the prototype, the length difference is not compensated and the laser frequency is not yet stabilized. However, the frequency noise is not a limiting source in the present condition. Optical path compensation and laser frequency stabilization are planned for the next improvement of the balance.

The second condition has been fulfilled by designing the interferometer in such a way that the angular and translation separations of the two interfering beams are of the second order with respect to the arm tilts. This has been obtained by adding in both the beam paths a lens with focal length  $L_f$  equal to the distance between the lens itself and the mirror, so that the beam is focused on the arm mirror (see Fig. 1). This scheme allows also the fulfillment of the third specification. Indeed, if the arm tilt  $\alpha$  is higher than a few mrad, the interferometer can be realigned by translating the input beam vertically by the quantity  $\delta y = L_f \alpha$ . In this



**Fig. 2** Optical scheme of the interferometric readout. In figure (a), the interferometer is aligned, while the balance arm is horizontal. An arm tilt  $\alpha$  would misalign the interferometer (b), but the presence of lenses in both arms permits the realignment by moving vertically the input laser beam by an amount  $\delta y$  (c)

condition, the beams impinge again orthogonally on the arm mirrors; then, they are reflected on the incoming path and recombine correctly at the beam splitter, as sketched in Fig. 2.

As mentioned above, the readout is completed by an auxiliary optical lever, powered by a superluminescent diode (SLED) and read by a quadrant photodiode. The lever is designed to have the beam impinging perpendicularly on a mirror placed on the lower face of the balance arm, and it is used as an initial reference position for the arm tilt.

## 2.2 Center of mass positioning

Beam balances and tiltmeter signals should not be induced by translation ground motion, but only by weight variations or ground rotations, respectively. It is known [19,20] that, if the tiltmeter center of mass does not lie on its rotation axis, a ground acceleration along the arm direction  $\ddot{z}$  generates a torque on the arm  $\tau = m\delta\ddot{z}$ , where  $m$  is the arm mass and  $\delta$  is the distance from the center of mass to the rotation axis. This means that, in order to minimize the coupling between  $\ddot{z}$  and the arm tilt, the distance  $\delta$  needs to be tuned as close as possible to zero.

Several tests have been performed to ascertain the difficulties in setting this distance within the limits of about  $10\mu\text{m}$ , as required by the Archimedes experiment [17]. The tuning of the center of mass position is done by regulating a set of screws placed on the arm. With the finest screw rotation, the center of mass can be moved by about  $1\mu\text{m}$ . Tuning operations are performed in air, and tiny mechanical displacements can occur while going into vacuum.

This implies that the tuning accuracy in vacuum is at best around  $10\mu\text{m}$ , which is still compliant with the requirements. However, in the design of the final balance, the center of mass positioning will be performed by acting remotely on the screws while the system is already in vacuum.

During operation at the Virgo site, the decoupling from translation ground noise has been tested with two methods. The first coarse one was to compare the balance signal with those of nearby seismometers during a far earthquake. In this case, the arrival times of various seismic waves are well separated: The first to occur are the primary waves (P-waves), which are essentially translation pressure waves, hence the secondary waves (S-waves), which are shear waves that can have tilt components depending on their polarization, and finally the surface waves, which have tilt components. While seismometers sense the ground motion, an ideal tiltmeter is expected to be sensitive to surface waves but not to P-waves. The behavior of our tiltmeter during a far earthquake is shown in Fig. 3. As expected, P-waves did not produce a signal above the noise level, while the effect of surface waves has been clearly observed.

A second, more refined method to test the decoupling from  $\ddot{z}$  was based on the comparison between tiltmeter and seismometer signals at a frequency where there is mainly translation seismic noise, that is, 0.4 Hz, around the microseismic peak frequency. At this frequency, a seismometer, which is more sensitive to translations than to tilts, would give a signal in which the component due to the ground tilt is negligible, unlike a tiltmeter, which is more sensitive to tilts than to translations. It follows that at 0.4 Hz the coherence between two such signals would be much less than 1, and this is what has been actually observed in our case, where  $Coh \approx 0.25$ , as shown in Fig. 4. The residual coherence is the consequence of a non-null distance  $\delta$ . Indeed, if the tiltmeter center of mass does not lie on its rotation axis ( $\delta \neq 0$ ), ground translations give rise to a signal, which is read as a tilt. The *shift-to-tilt* coupling allows an estimate of  $\delta$ . The coupling, measured as:

$$C = \sqrt{Coh} \frac{\theta}{\ddot{z}/g}$$

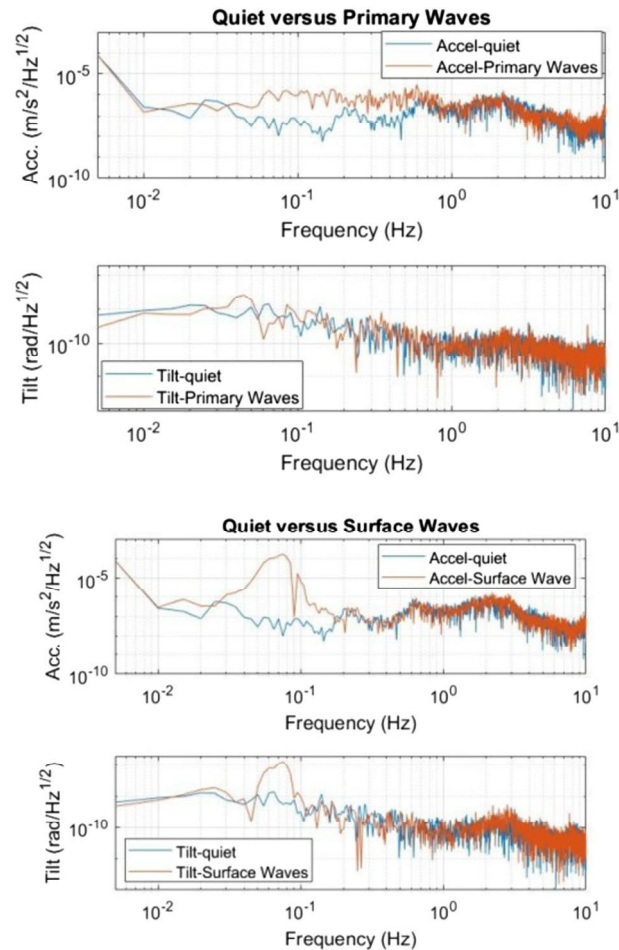
results  $C \approx 1.2 \times 10^{-3}$ , where  $\theta$  is the balance signal at 0.4 Hz and  $g$  is the gravitational acceleration. At first order, the coupling is given by

$$C = \frac{mg \cdot \delta}{I\omega^2}$$

where  $I$  and  $m$  are the momentum of inertia and the mass of the arm, respectively, and  $f = \omega/2\pi$  is the measurement frequency [19]. In the hypothesis that a microseism does not produce ground tilts, the value of the coupling  $C = 1.2 \times 10^{-3}$  corresponds to the upper limit  $\delta = 15 \times 10^{-6} \text{ m}$ , consistent with expectations.

### 2.3 Actuators and control loop

The beam balance is kept at the desired working point through a feedback control system. The loop is closed with electrostatic actuators, as typically used for the control of torsion pendulums [9, 10]. In our case, they are four metallic plates placed along the two sides of the balance arm. This latter is grounded, while the actuators are powered by a DC voltage supplier that can reach the maximum voltage of 2000 V. The actuator torque  $\tau = \beta \cdot V^2$  is quadratic in the applied voltage  $V$ , with  $\beta = 2.5 \times 10^{-11} \text{ Nm/V}^2$ . The maximum torque is  $\tau_{\text{max}} = 10^{-4} \text{ Nm}$ . The control signal is linearized by performing the square root of the correction signal before sending it to the actuators. The error signal is provided by the optical

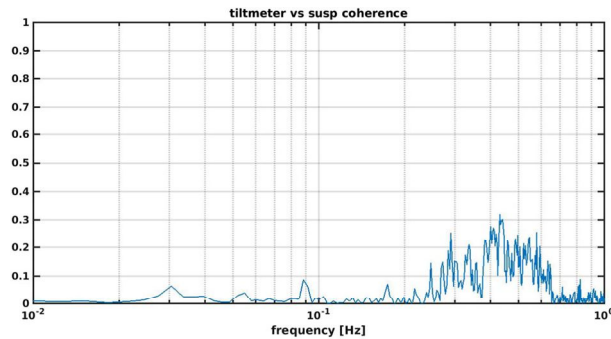


**Fig. 3** Earthquake as read by a seismometer and by the tiltmeter. Top figure, upper plots: seismometer signal before (blue) and during (red) the P-waves; Top figure, lower plots: balance signal during the same period. It can be noticed that, during the earthquake, the seismometer senses the higher ground motion while the balance does not, as expected. Bottom figure: the same signals as in Top figure but referring to quiet period (blue) and surface waves. It can be noticed that, as expected, both the seismometer and the tiltmeter sense the higher ground motion

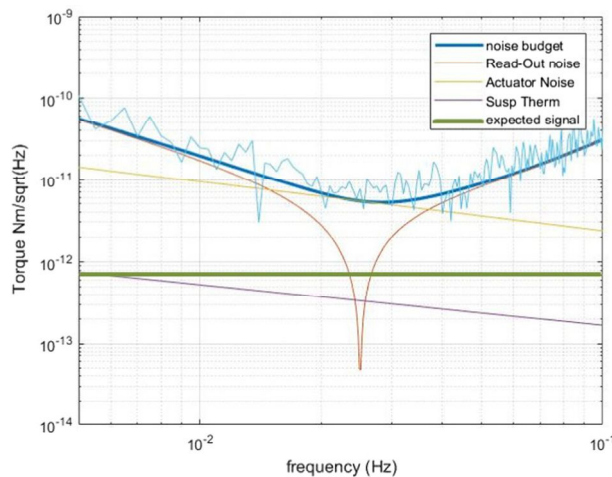
readout, as described in Sect. 2.1. After obtaining a coarse positioning with the optical lever signal, the error signal is switched to the interferometric signal, which provides a finer reference. During the operations at the Virgo site, the error and control signals are acquired and computed by the Virgo processing system [3]. The control loop has unity gain at 0.2 Hz.

### 3 Results at low frequencies

In the region of tens of mHz, the torque sensitivity reaches the value  $\tilde{\tau} \simeq 8 \times 10^{-12} \text{Nm}/\sqrt{\text{Hz}}$ . To our knowledge, this result is comparable with or even better than the currently best torque



**Fig. 4** Coherence of the tiltmeter with a combination of accelerometers at the upper stage of the Virgo superattenuator



**Fig. 5** Sensitivity and noise budget of the balance prototype compared with the expected signal (green line)

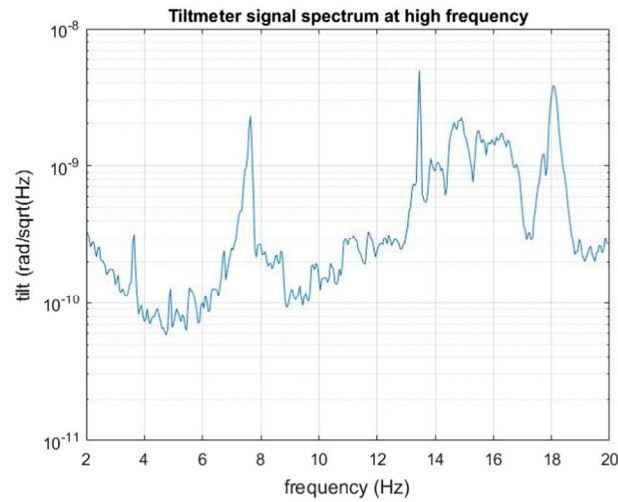
sensitivities in the world for balance systems [11]. Actuation and sensing noise are the main limiting noise sources, as reported in Fig. 5. At frequencies below 10 mHz and above 100 mHz, the interferometer signal is indeed coherent with the laser power fluctuations read at the input of the interferometer by an auxiliary photodiode.

In the intermediate region, the major contribution is given by the actuator noise. This can be evaluated considering that presently the actuation is obtained by applying a DC voltage control signal (i.e., not modulated). This implies that the actuation noise  $\tilde{A}_n$ , at first order, is proportional to  $V_{\text{RMS}}$ , the RMS of the control signal:  $\tilde{A}_n = \beta \cdot V_{\text{RMS}} \tilde{V}_n$ , where  $\tilde{V}_n$  is the voltage output noise of the amplifier. In the best condition, the balance was operated with tens of volts of static correction, corresponding to the noise reported in Fig. 5.

#### 4 Sensitivity to tilts at high frequencies

Beam balances can be used as rotational sensors. In our case, in the low-frequency region, the sensitivity is not yet sufficiently good to use the balance as tiltmeter to control the Virgo





**Fig. 6** Spectral density of the tilt amplitude in a quiet night at the Virgo site

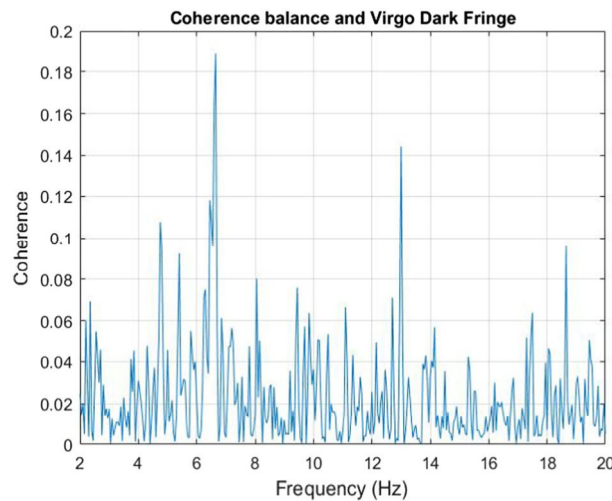
interferometer. This is due to the choice of a very light arm, which helps in reaching a very good sensitivity in torque, but makes more difficult its use as a tilt reference. On the contrary, at higher frequencies, far above the resonance frequency, a light arm is not a limitation. Above a few Hz, rotation sensors are expected to be used in future detectors as ground tilt sensors for Newtonian noise subtraction.

The balance has been positioned at the North-end building, on the same floor where other auxiliary systems, like seismometers and other sensors, are located. The balance has been installed just before the start of the Virgo observation run O3 and remained on site for several months. The data taking allowed us to measure the ground tilts and test the coherence with seismometers and with the Virgo interferometer signal.

The results of the tilt measurement are shown in Fig. 6 for the frequency region from 2 to 20 Hz. This interval is particularly interesting for both Virgo and the future Einstein Telescope, whose observation band will extend down to 2 Hz. At a few Hz, the measured tilt reaches  $\tilde{\theta} \approx 8 \times 10^{-11} \text{ rad}/\sqrt{\text{Hz}}$ . Above 10 Hz, it shows a plateau of a few times  $10^{-10} \text{ rad}/\sqrt{\text{Hz}}$  and a series of resonances larger than  $10^{-9} \text{ rad}/\sqrt{\text{Hz}}$ . The tilt measurement at lower frequencies, around a few Hz, highlights the property of the Virgo site to be quiet in this range.

In the 10–20 Hz interval, the measured tilt is similar to that at the LIGO site [13]. In particular, in the outer ranges (10–13 Hz and 18–20 Hz) the plateau is comparable, whereas in the middle range (between 13 and 18 Hz) the noise is higher. This result is still under investigation. Several resonances are coherent with seismometer signals, corroborating the hypothesis that they are structural resonances of the building. Figure 7 shows the correlation between the tiltmeter and the Virgo interferometer (i.e., gravitational wave) signals. At several frequencies, the tiltmeter is partially coherent with the Virgo interferometer and with seismometers placed in the building. On the other hand, at some frequencies, like 18.65 Hz, the balance signal is coherent with the Virgo interferometer, but not with the seismometers. However, in both cases, estimates of the Newtonian noise coupling is not compatible with a direct Newtonian coupling of ground motion with tilt masses, but rather with, for instance, a coupling mechanism through diffused light.





**Fig. 7** Coherence of the balance signal with the Virgo interferometer signal

## 5 Conclusions and next steps

The measurement campaign with the beam balance performed at the Virgo site provided very encouraging results toward the definitive measurement of the weight of electromagnetic vacuum. Indeed, the torque sensitivity at low frequencies reaches the value  $8 \times 10^{-12} \text{ Nm}/\sqrt{\text{Hz}}$ , which is only a factor  $\approx 10$  higher than the torque expected in the measurement of vacuum weight.

At present, the sensitivity is limited by the laser amplitude and actuators noises. These can be reduced by stabilizing the laser and using voltage amplifiers with a lower noise. The latter improvement will be possible once the balance will be moved to a more quiet site, such as the SAR-GRAV laboratory, in Sardinia. In these seismic conditions, the force needed to maintain the interferometer locked is expected to be at least an order of magnitude lower; therefore, we could use amplifiers with a lower voltage and hence with a lower noise.

At high frequencies, the balance has shown a very good sensitivity to tilts, allowing us to measure the ground tilt at the Virgo site and to show that at some frequencies the Virgo dark-fringe signal is correlated with the tiltmeter signal. Moving the balance to the SAR-GRAV laboratory will permit a better study of the sensitivity to lower tilts, which will allow a new version of the balance to be used to measure ground tilts in the next Virgo run.

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**Data Availability Statement** This manuscript has associated data in a data repository. [Authors' comment: This manuscript has associated data in the Virgo Gravitational-Wave detector Data Repository. All data included in this manuscript are available upon request by contacting with the corresponding author.]

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## Appendix: The Archimedes and Virgo Collaboration

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